

Seismicity-Permeability Coupling in the Breaching and Sealing of Reservoirs and Caprocks

Derek Elsworth (Penn State), Yi Fang (PSU), Chaoyi Wang (PSU), Takuya Ishibashi (AIST/PSU), Yves Guglielmi (LBNL/Aix-Marseille), Kyunjae Im (PSU), Yunzhong Jia (PSU/NTU), Brandon Schwartz (PSU), Ziyang Li (PSU), Elif Yildirim (PSU), Andre Niemeijer (UU), Thibault Candela (TNO), Ben Madara (PSU), Mengke An (Tongji), Fengshou Zhang (Tongji), Jacques Riviere (Grenoble/PSU), Parisa Shokouhi (PSU), Chris Marone (PSU)

Some Key Issues in Energy Supply

Needs

Constraints and Solutions

CO₂ Sequestration - Linking Induced Seismicity to Permeability Evolution

Controls on seismicity - the aseismic-seismic transition

Controls on maximum magnitude event

RSF - for permeability evolution

Controls on stability and permeability

Mineralogical & textural

Structural

Healing and sealing and the seismic cycle

Energy From Hot Rocks - EGS and SGRs

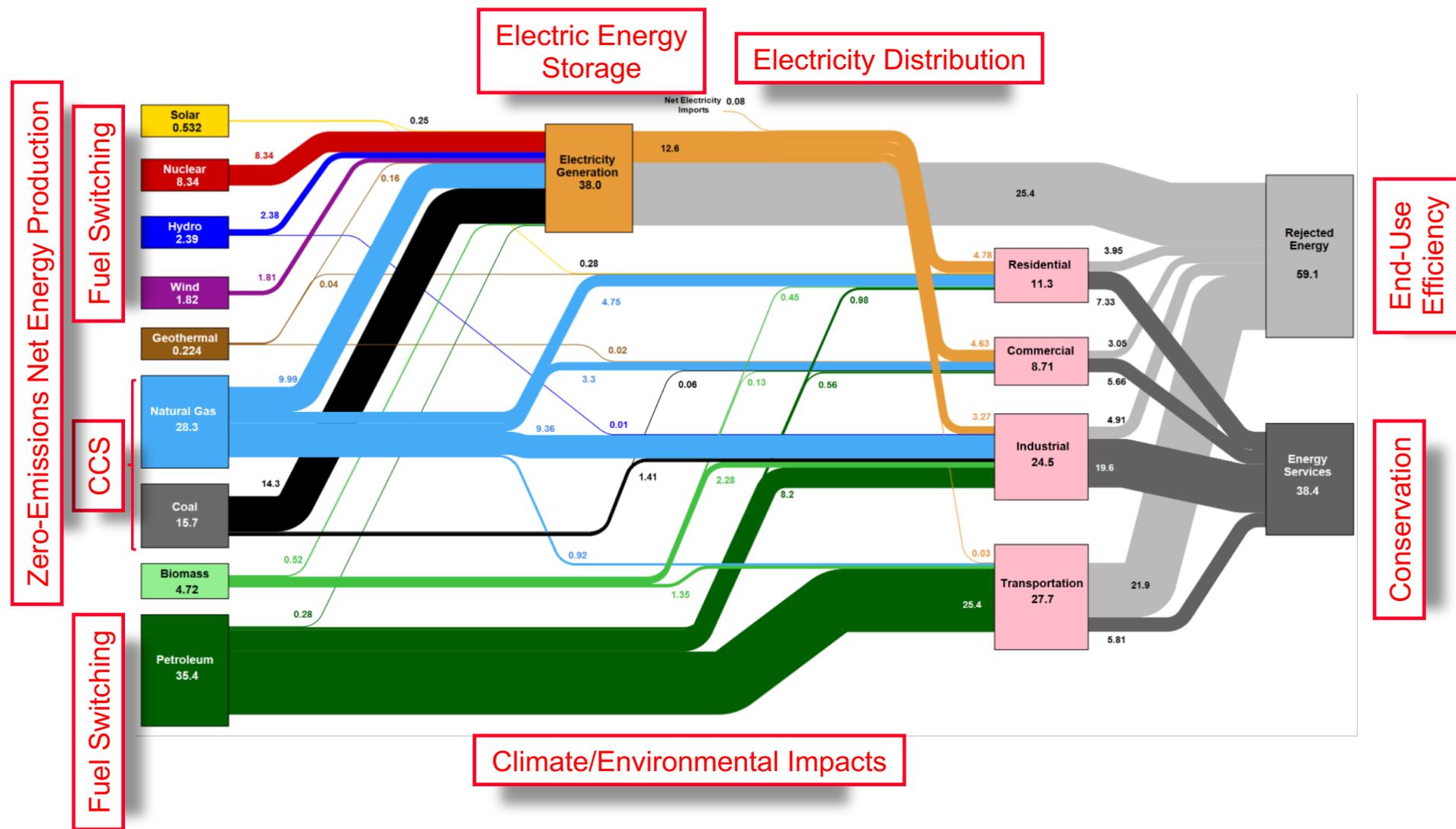
Anomalous seismicity - Newberry Demonstration Project

Permeability scaling - Newberry Demonstration Project

Summary

US Energy Consumption 2015 - Key R&D Strategies

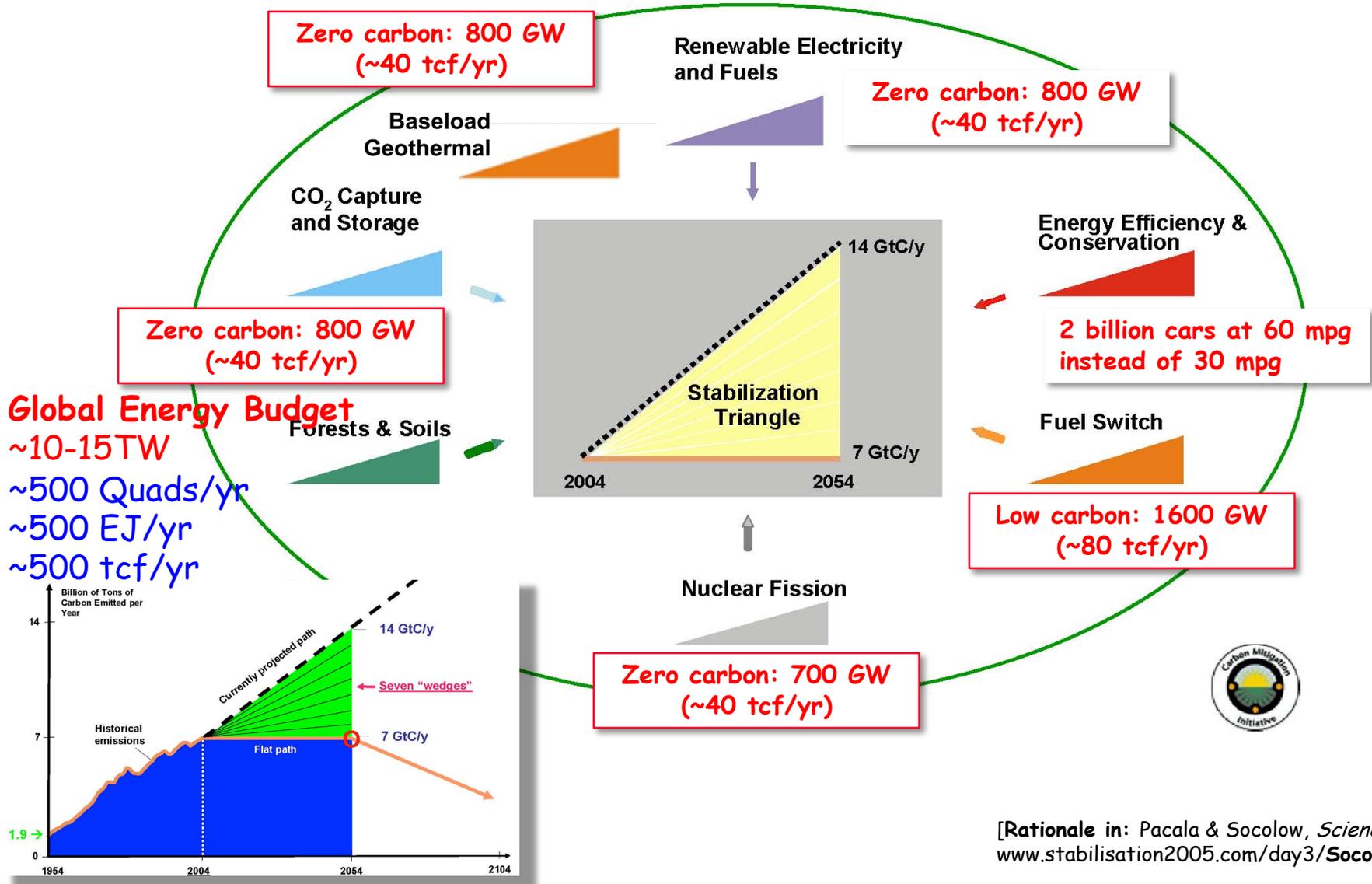
~100 Quads = 100 EJ = 100 tcf CH₄ (~20% of World)



[After Pat Dehmer, US DOE, Office of Science, 2009; Sankey Diagram from LLNL]

Capacity Needs - Stabilization Wedges

Fill the Stabilization Triangle with Seven Wedges

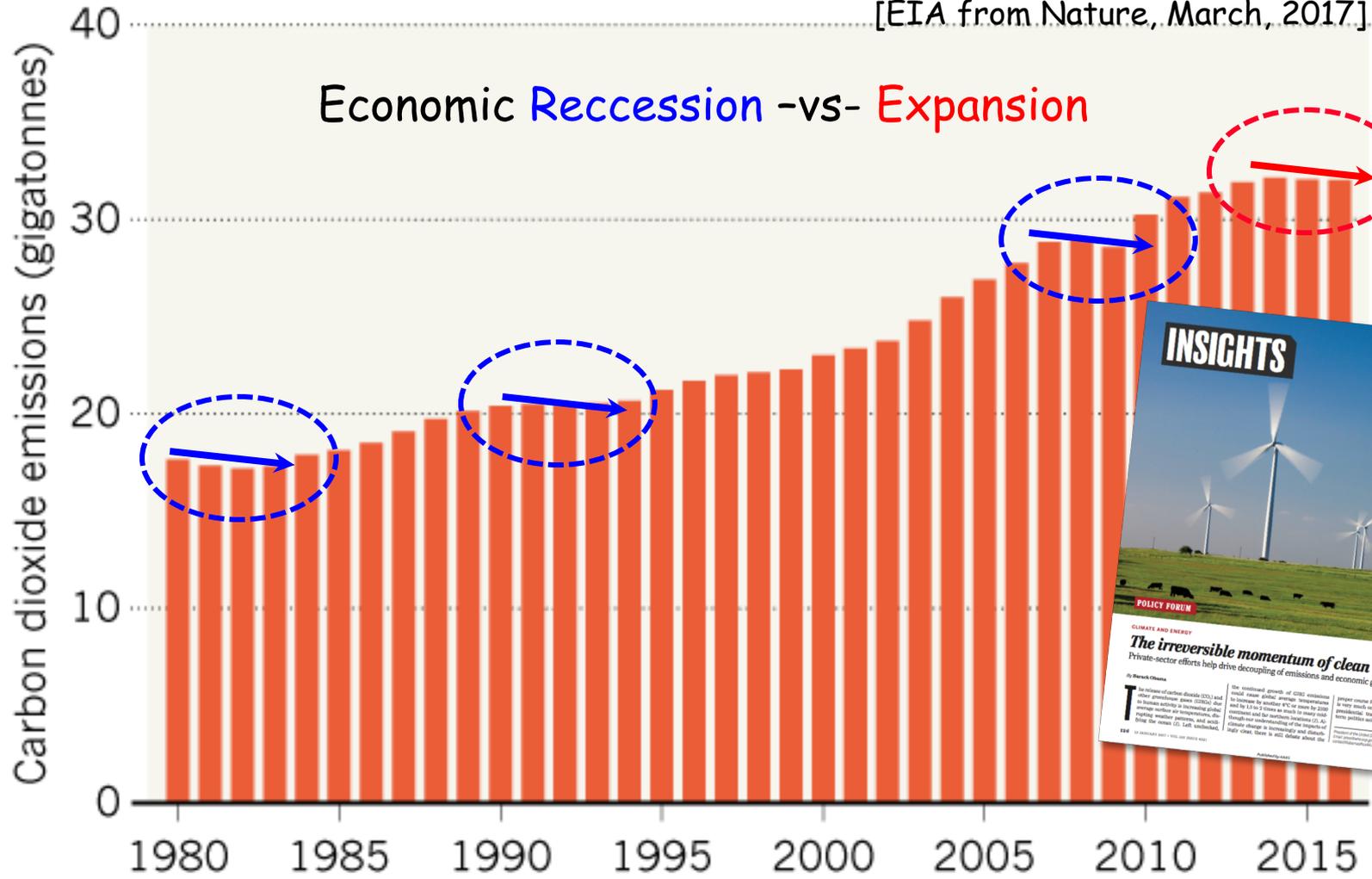


[Rationale in: Pacala & Socolow, *Science*, 2004, www.stabilisation2005.com/day3/Socolow.pdf]

CARBON DIOXIDE EMISSIONS FLAT FOR THIRD YEAR

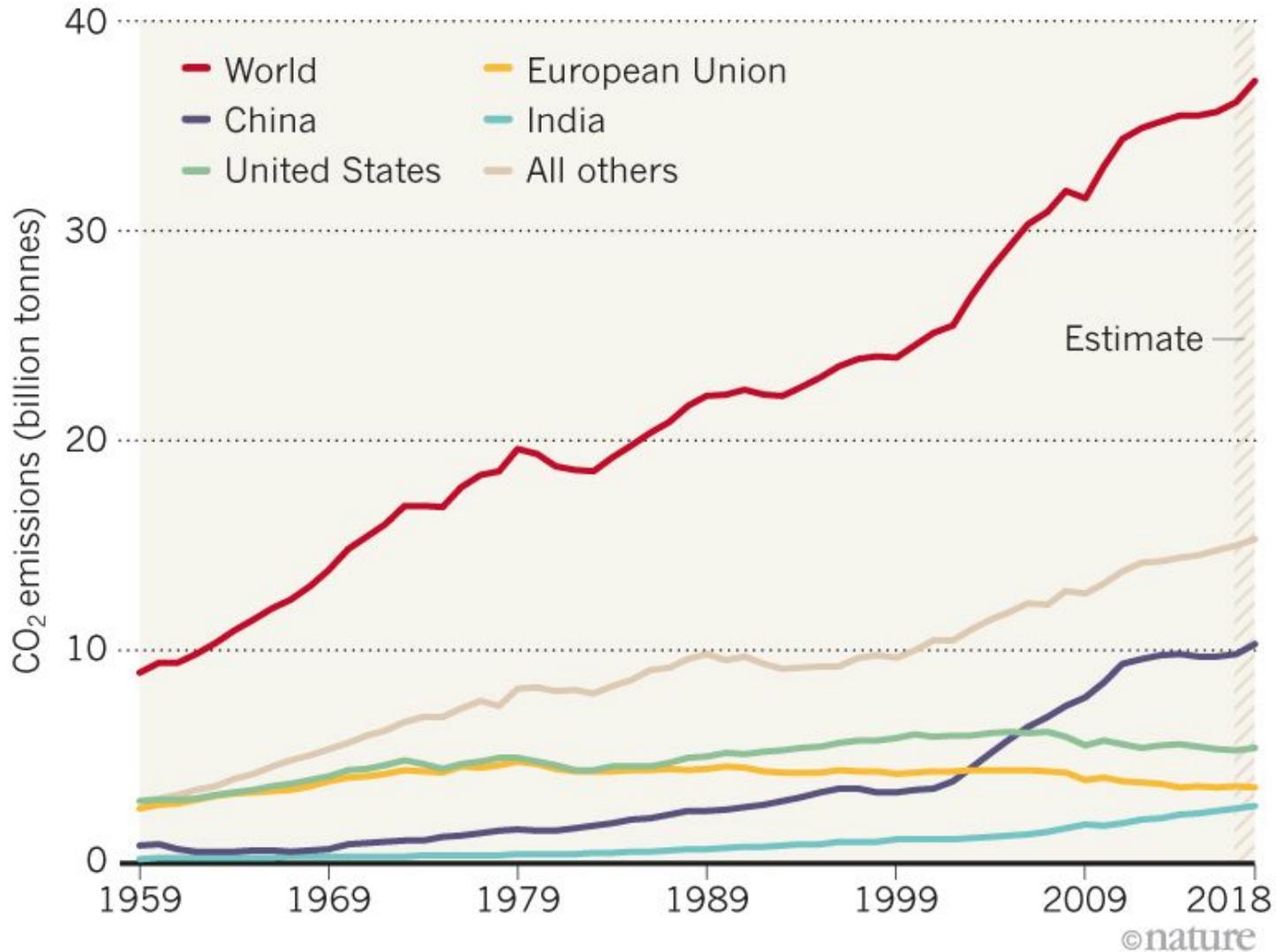
Rising renewables use and improvements in energy efficiency have kept the world's carbon dioxide emissions stable.

[EIA from Nature, March, 2017]



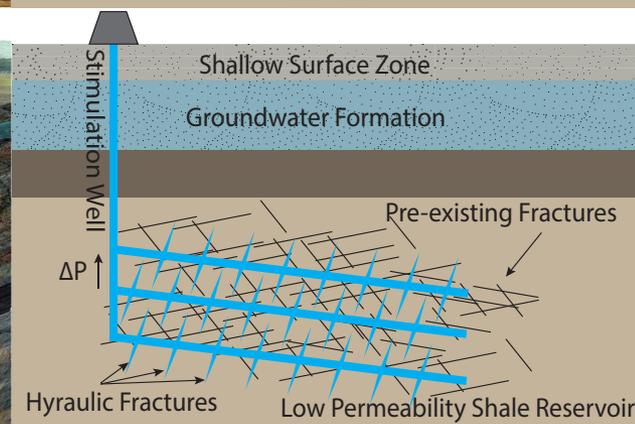
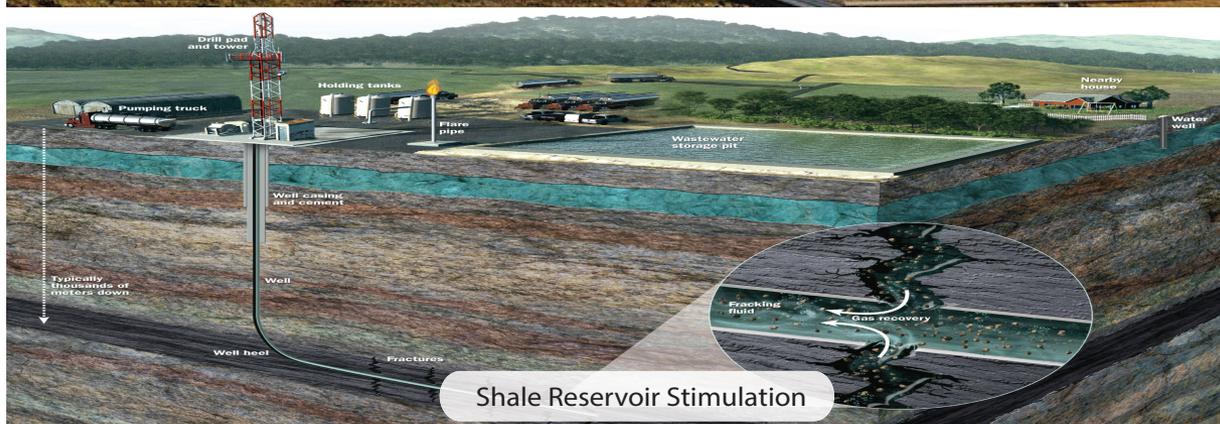
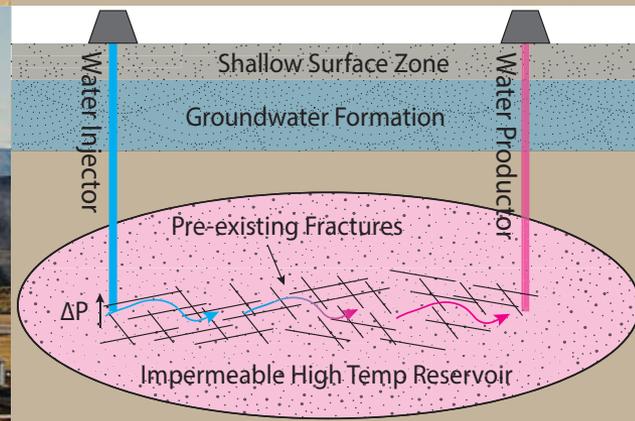
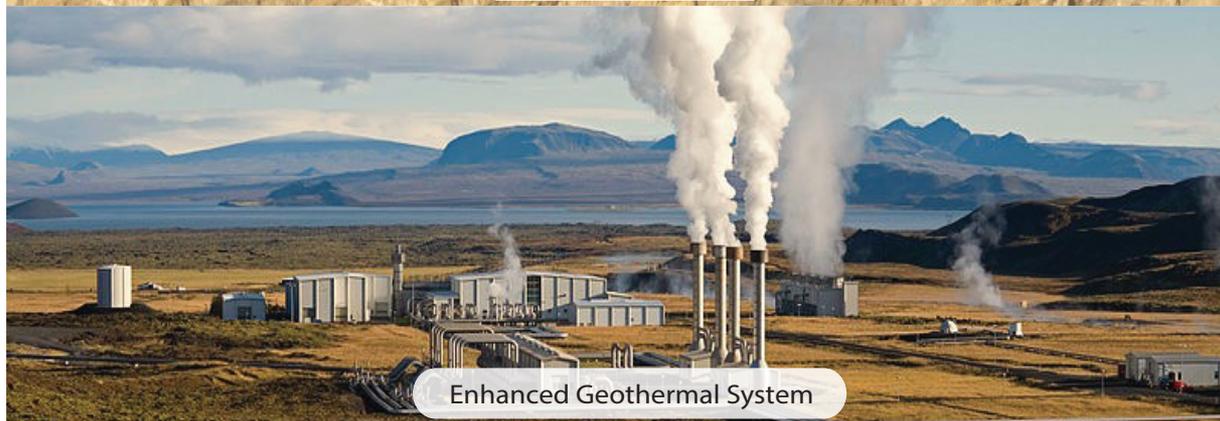
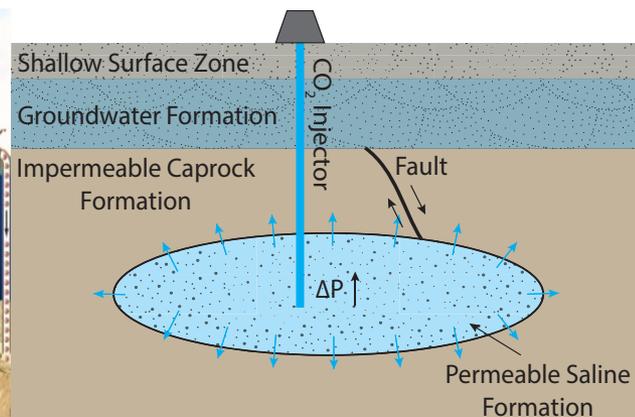
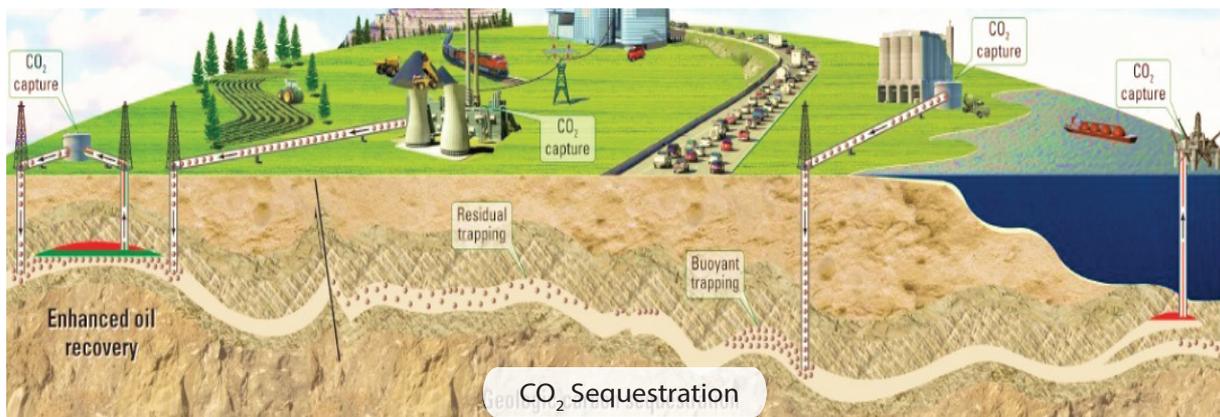
CO₂ EMISSIONS KEEP ON RISING

Industrial carbon-dioxide emissions are projected to rise again globally this year, even as individual countries' emissions look very different.



[From Nature, December, 2018]

Mechanical/Stability and Transport Properties of Fractured Rocks



Sub-Surface Geoengineering - Some Key Issues in Sustainable Recovery of Energy Resources

"All-of-the-Above"

Sequestration (CO₂/HLW)

- Permeability-seismicity coupling

 - Seismic-aseismic deformation and implications

 - Scale dependencies

 - Rational models for permeability-seismicity linkage

Gas Shales - making permeability

- Making permeability - Gas fracturing

- Sustaining permeability in fracs/refracs

- Elevating long term permeability - dp, dc, dT

EGS Geothermal Resources - controlling permeability

- Uniform sweep - permeability control

 - Complex coupled process interactions

 - Manifold approaches

 - Permeability-seismicity linkage for characterization

 - True control and engineering of reservoirs & migration of O/G technology

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Summary

Induced Seismicity

NEWSFOCUS



Ohio rumblings. Wastewater injected at this site in Youngstown triggered jolting earthquakes that prompted injection-well shutdowns and strong new regulations.

Arkansas. In the current March/April issue of *Seismological Research Letters*, the University of Memphis seismologist recounts his learn-as-you-go experience with injection-triggered quakes strong enough to seriously shake up the locals.

Fracking for natural gas, formally known as hydraulic fracturing, had come to Arkansas around 2009. Not that a seismologist in Memphis would have noticed. Injecting water into gas-bearing shale at high pressures does break the rock to free the gas—that's the point, after all. But the resulting tiny quakes rarely get above magnitude 0 (the logarithmic scale includes negative numbers), never mind to the magnitude-3 quakes that people might feel.

But shale gas drillers need to dispose of the millions of liters of water laden with natural brines and added chemicals that flow back up after a shale gas well has been fracked (*Science*, 25 June 2010, p. 1624). Injecting fracking wastewater into deep rock is a common solution, so starting in April 2009, 1- to 3-kilometer-deep disposal wells were sunk in the vicinity of Guy (population 706) and Greenbrier (population 4706), Arkansas.

That's when Horton and Scott Ausbrooks of the Arkansas Geological Survey took note of a curious cluster of earthquakes near Greenbrier. The Guy-Greenbrier area had had only one quake of magnitude 2.5 or greater in 2007 and two in 2008. But there were

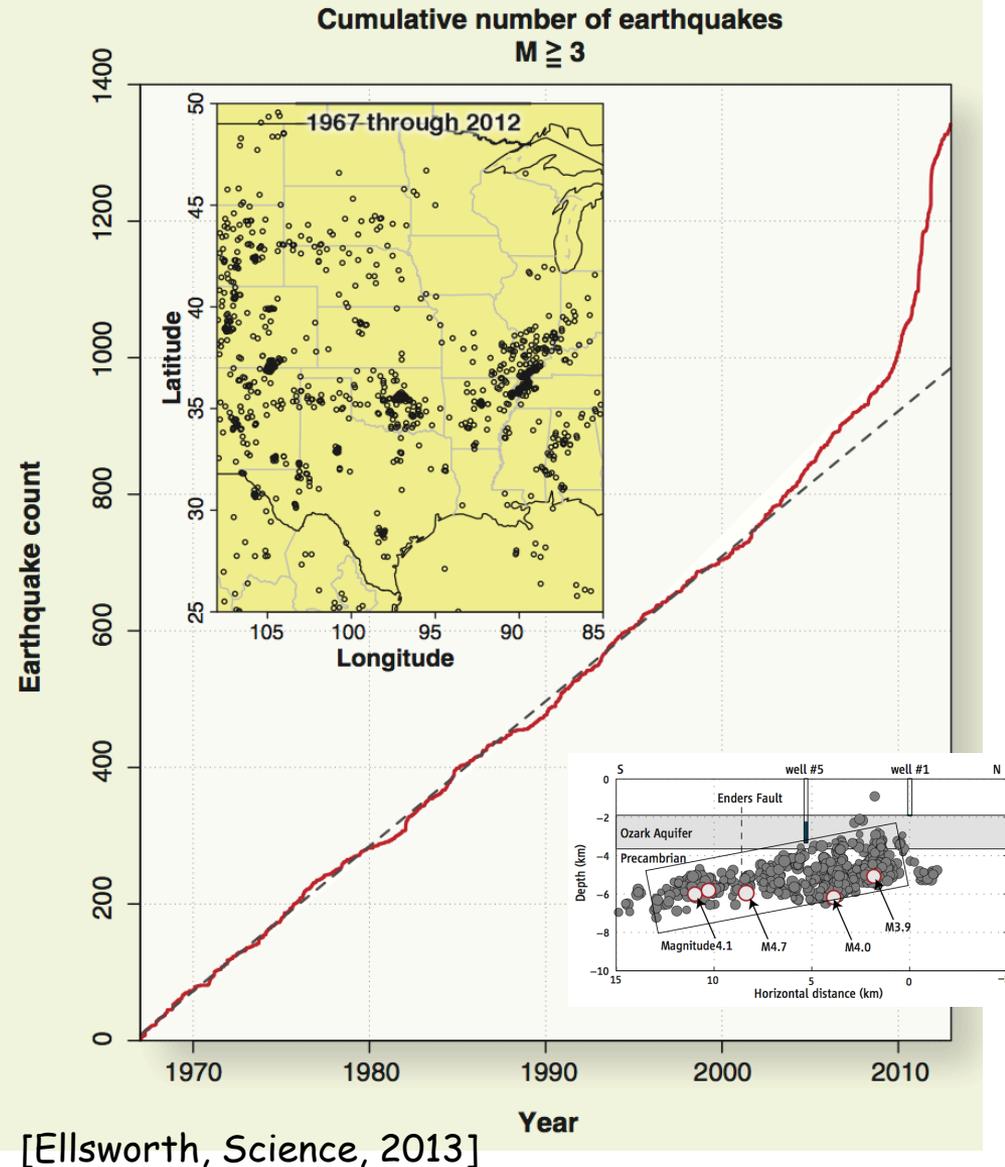
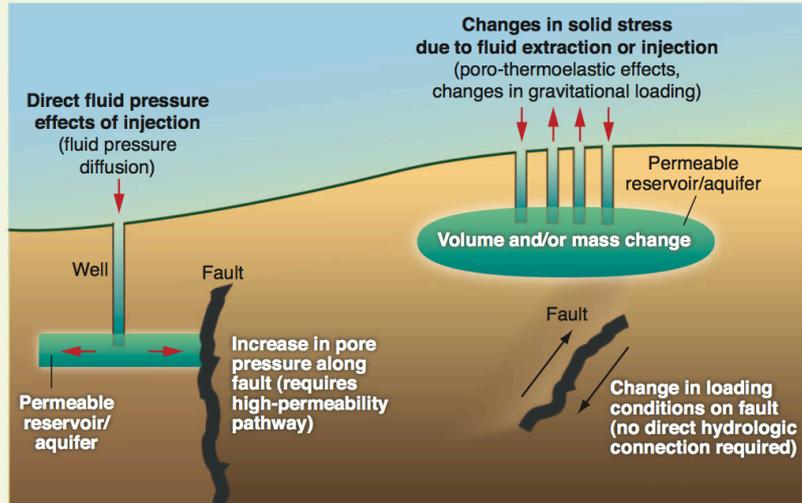
SEISMOLOGY

Learning How to NOT Make Your Own Earthquakes

As fluid injections into Earth's crust trigger quakes across the United States, researchers are scrambling to learn how to avoid making more

First off, fracking for shale gas is not touching off the earthquakes that have been shaking previously calm regions from New Mexico to Texas, Ohio, and Arkansas. But all manner of other energy-related fluid injection—including deep disposal of fracking's wastewater

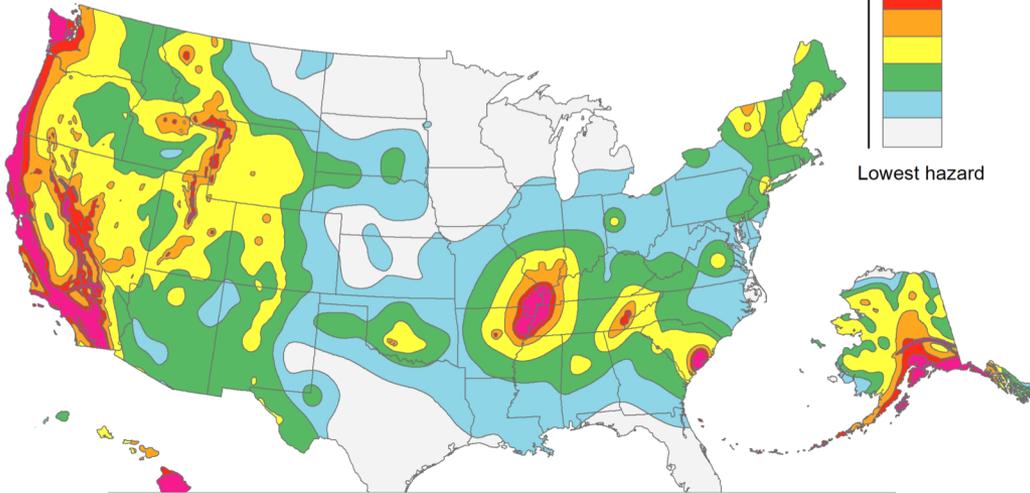
seismicity, they are beginning to see a way ahead: learn as you go. Thorough preinjection studies followed by close monitoring of cautiously increasing injection offer to lower, although never eliminate, the risk of triggering intolerable earthquakes.



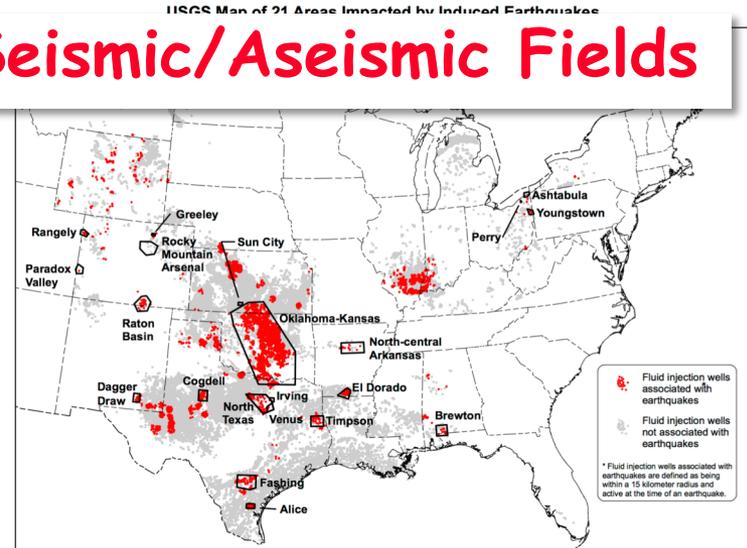
[Ellsworth, *Science*, 2013]

Induced Seismicity

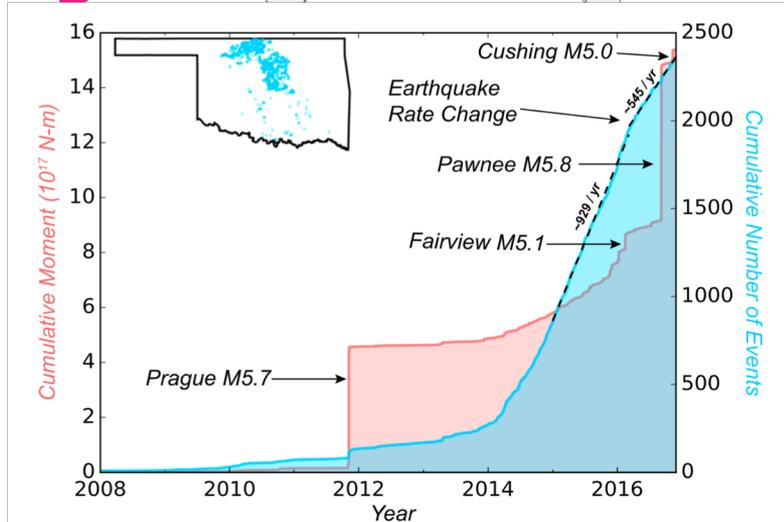
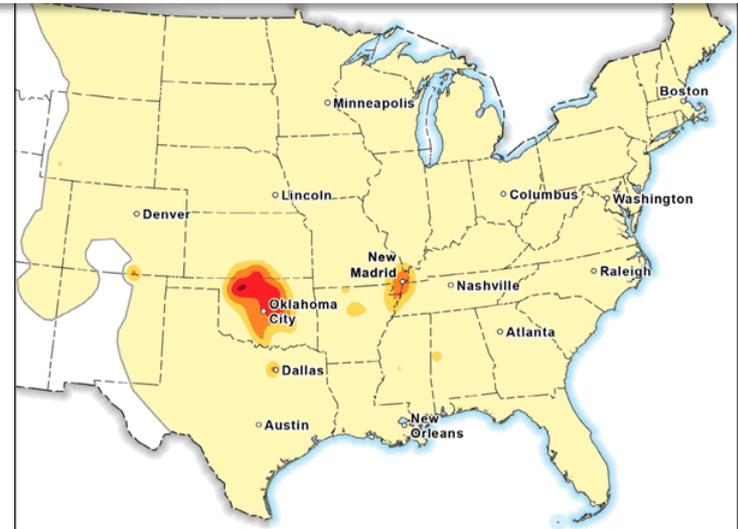
US Seismic Hazard



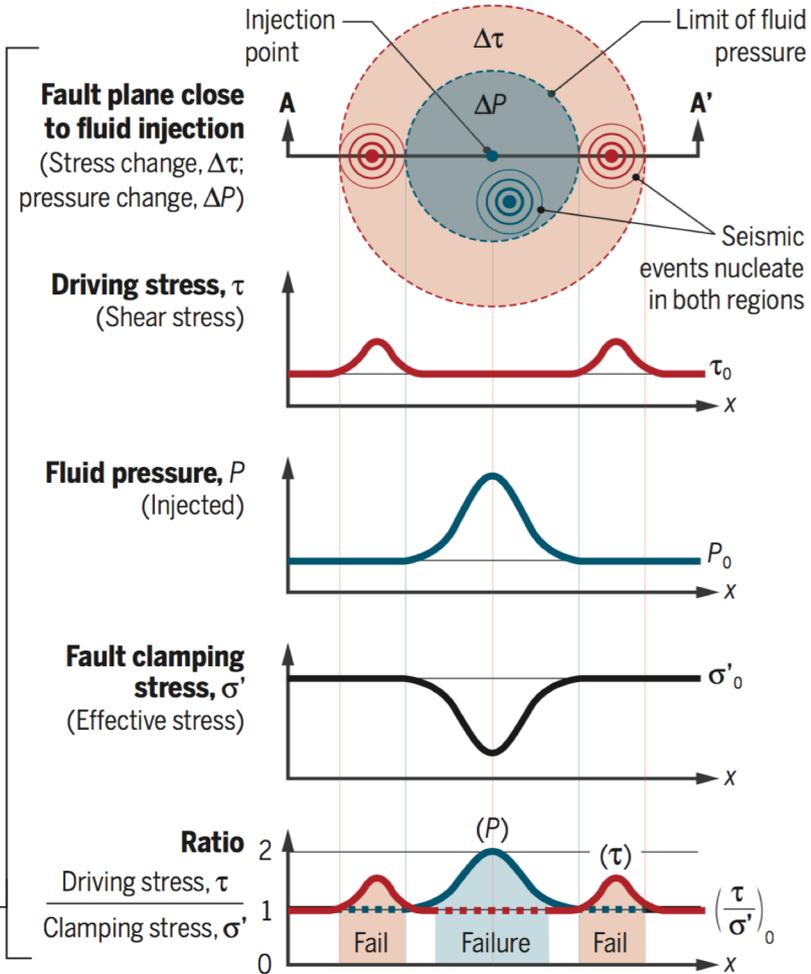
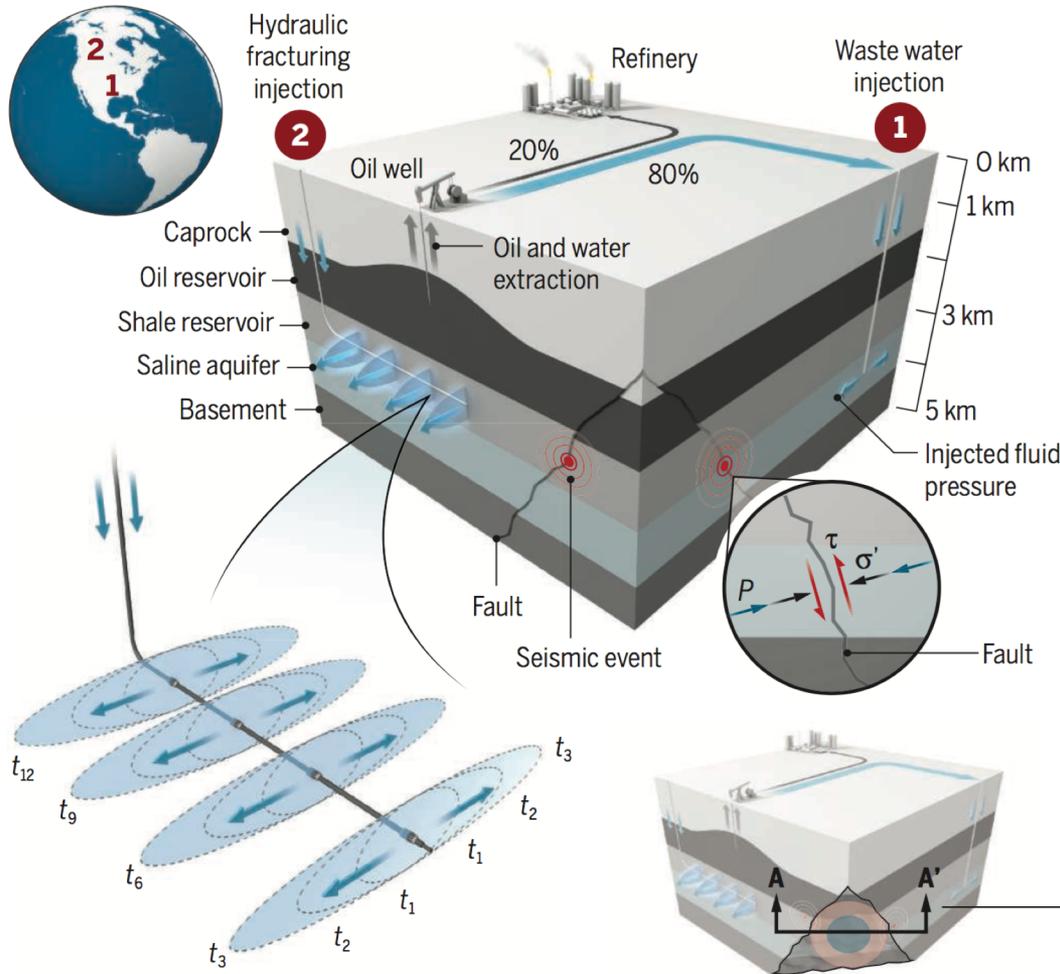
Seismic/Aseismic Fields



Mid-west Seismic Hazard



Induced Seismicity

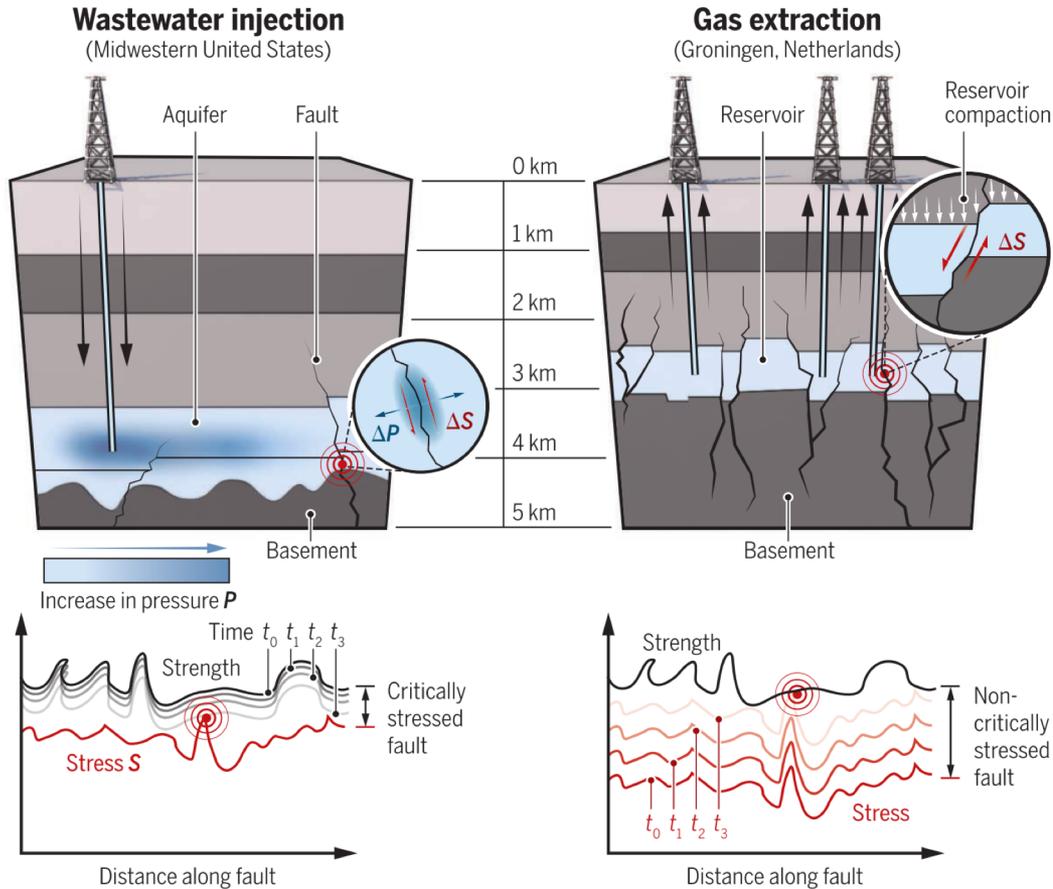


[Elsworth et al., Science, 2016]

Mechanisms of Induced Seismicity

Mechanisms of induced seismicity

Both wastewater injection and gas extraction can cause induced earthquakes. Detailed observations from the midwestern United States and Groningen, Netherlands, show that in both cases, preexisting conditions in Earth's crust are of central importance.



Injection of wastewater leads to a nonuniform pressure front. When the pressure front hits a critically stressed fault, an earthquake is triggered. Only a small strength decrease is needed to trigger an event.

Gas extraction leads to rock compaction, causing a buildup of stress. Sufficient shear stress is necessary to cause the initially noncritically stressed fault to fail, causing an earthquake.



[Candela et al., *Science*, 2018]

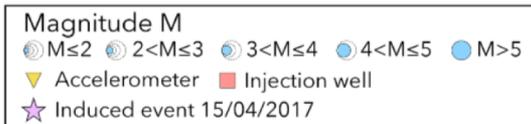
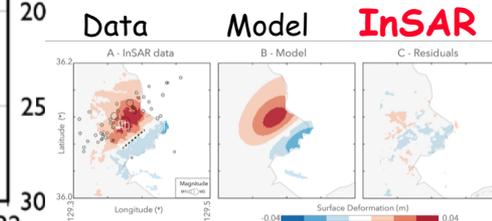
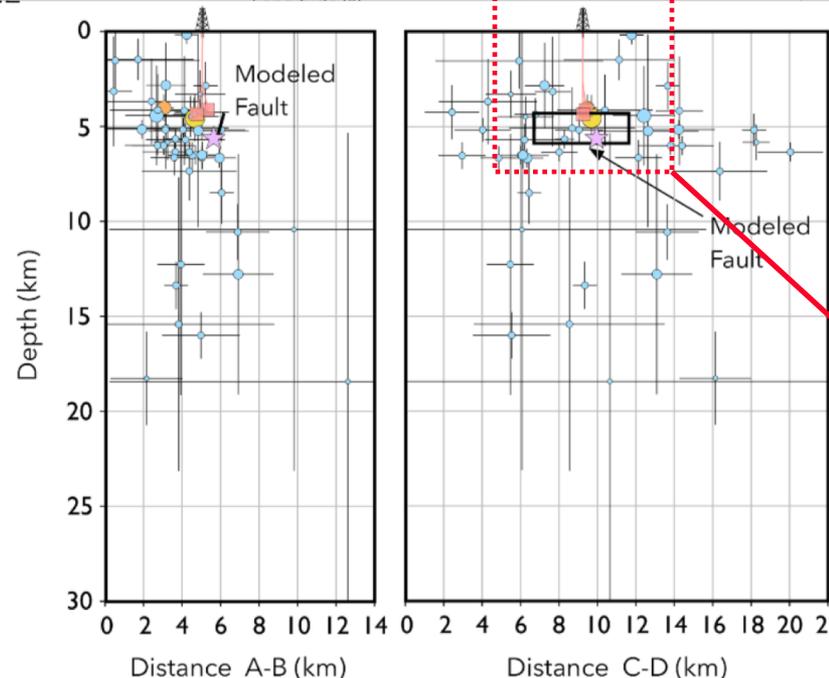
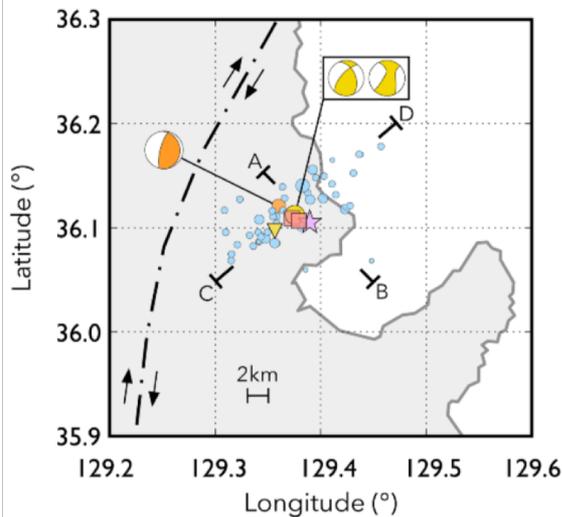
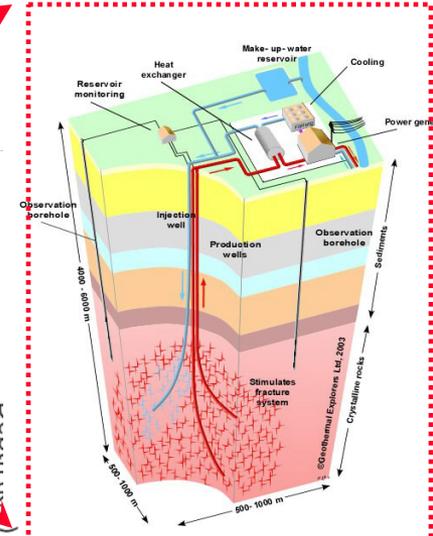
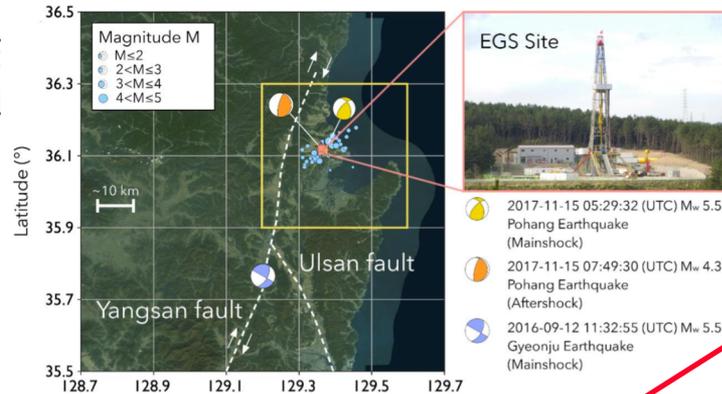
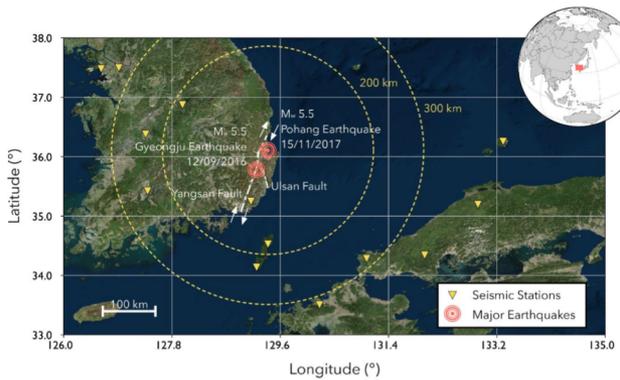
Pohang (South Korea) Earthquake (2017) Mw~5.5

EGS Stimulation Related?

Anatomy of the EQ

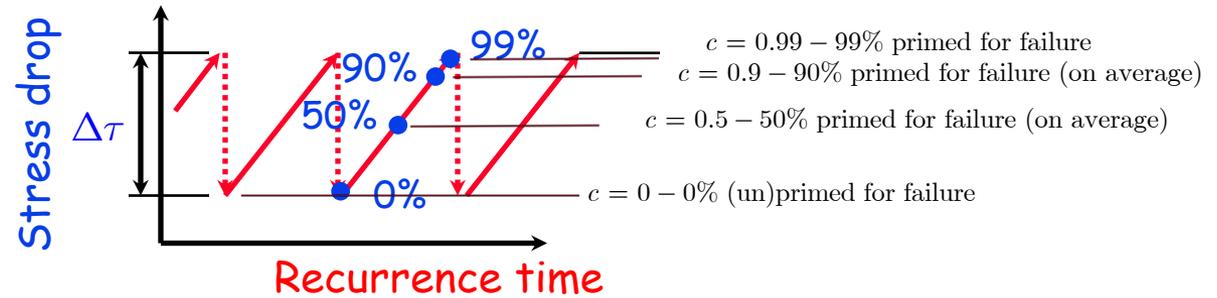
15th century EQs Mw~7
Mw<5 since instrumental
recording in 1903

Mw~5.5 ~30km south of EGS
Mw~5.5 Pohang ~4km depth
Same strike-slip fault



[Grigoli et al., Science, 2018]

Maximum Event Magnitude - Equivalent Porous Medium



Moment Magnitude (Deviatoric)

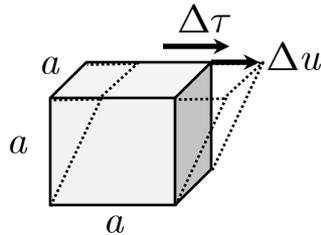
$$M = AG\Delta u$$

$$M = a^3G \frac{\Delta u}{a}$$

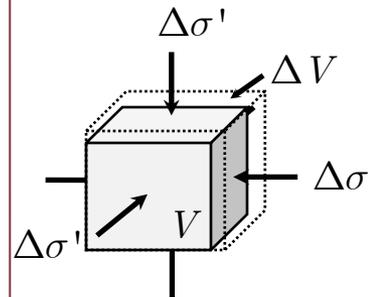
$$M = VG\gamma$$

$$M = V\Delta\tau$$

$$\Delta\tau = \frac{M}{V}$$



$$\Delta\tau \cdot (1 - c) = \mu \cdot \Delta\sigma'$$



Stress-Strain (Spherical)

$$\Delta\sigma' = \Delta\sigma - \alpha\Delta p \quad (\Delta\sigma = 0)$$

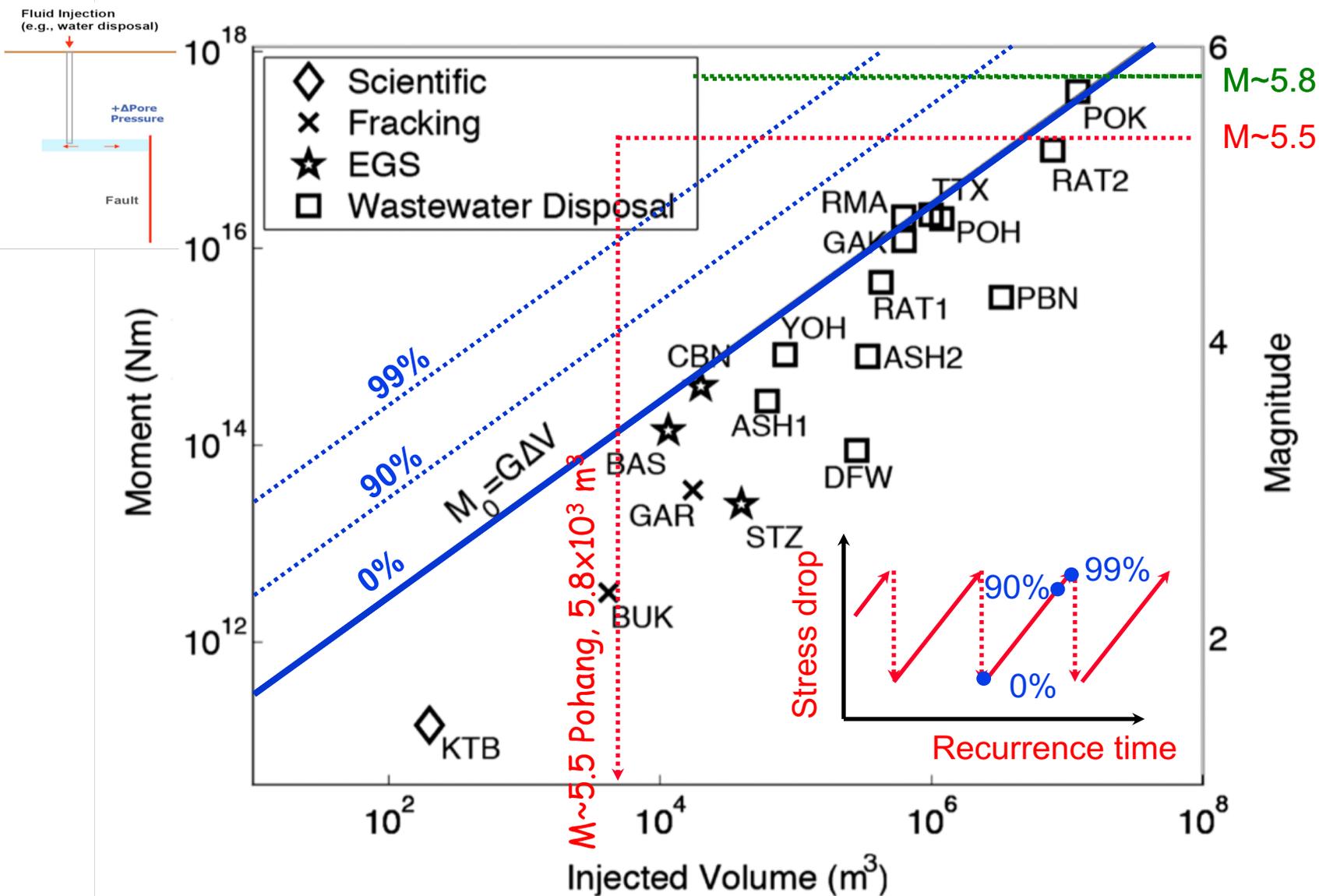
$$\alpha\Delta p = K \frac{\Delta V}{V}$$

$$\alpha\Delta p = \frac{2(1+\nu)}{3(1-2\nu)} G \frac{\Delta V}{V}$$

$$M = \frac{2(1+\nu)}{3(1-2\nu)} \frac{1}{(1-c)} \mu G \Delta V$$

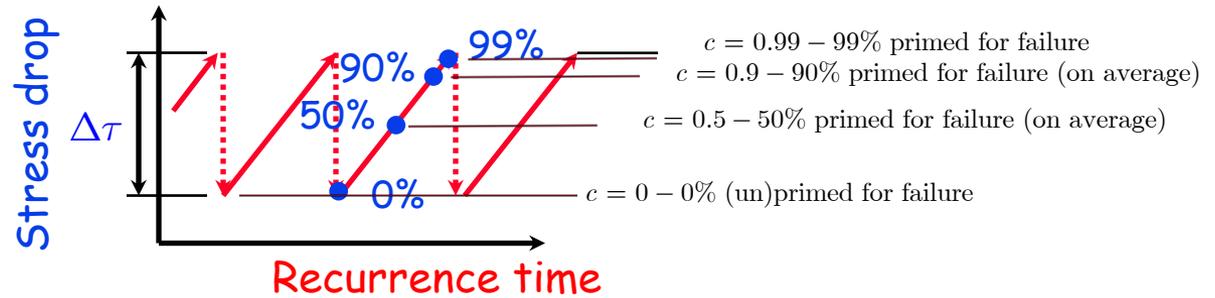
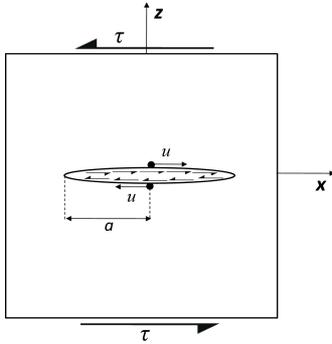
$$M = \frac{1}{(1-c)} G \Delta V \left\{ \begin{array}{l} \nu = 0.25 \\ \mu = 0.6 \end{array} \right\}$$

Maximum Anticipated Moment Magnitude - M or M_{dot} ? M_{Gross} or M_{Net} ? Triggered -vs- Induced?



After [McGarr, JGR, 2014]

Maximum Event Magnitude - Penny-Shaped Crack



Moment Magnitude (Deviatoric)

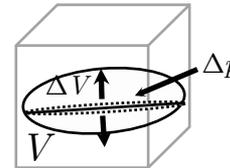
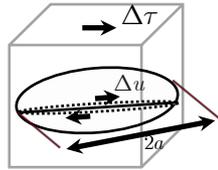
$$M = AG\Delta\bar{u}$$

$$\Delta\bar{u} = \frac{8(1-\nu)}{3(2-\nu)} \frac{\Delta\tau a}{G\pi}$$

$$M = AG \frac{8(1-\nu)}{3(2-\nu)} \frac{\Delta\tau a}{G\pi}$$

$$\Delta\tau = \frac{M\pi}{Aa} \frac{3(2-\nu)}{8(1-\nu)}$$

$$\Delta\tau \cdot (1 - c) = \mu \cdot \Delta p$$



Stress-Strain (Spherical)

$$\frac{\Delta V}{A} = \frac{16(1-\nu^2)}{3\pi} \frac{\Delta p a}{E}$$

$$\Delta p = \frac{\Delta V}{Aa} \frac{3\pi}{16} \frac{E}{(1-\nu^2)}$$

$$M = \frac{1}{(2-\nu)} \frac{1}{(1-c)} \mu G \Delta V$$

$$M = \frac{1}{(1-c)} \frac{24}{70} G \Delta V \sim \frac{1}{(1-c)} \frac{1}{3} G \Delta V \left\{ \begin{array}{l} \nu = 0.25 \\ \mu = 0.6 \end{array} \right\}$$

Anticipated Thermal Stressing in EGS

For a closed system in thermal equilibrium:

Heat carried by water:

$$H = \Delta V \rho_f c_f \Delta T_f$$

Heat in closed system:

$$H = V(n\rho_f c_f + (1-n)\rho_s c_s)\Delta T_{res}$$

Volume*Temperature Product:

$$V\Delta T_{res} = \Delta V\Delta T_f \frac{1}{(n + (1-n)\frac{\rho_R c_R}{\rho_f c_f})}$$

Event magnitude:

$$M = \frac{1}{(1-c)} G\alpha_T V\Delta T_{res} \left\{ \begin{array}{l} \nu = 0.25 \\ \mu = 0.6 \end{array} \right\}$$

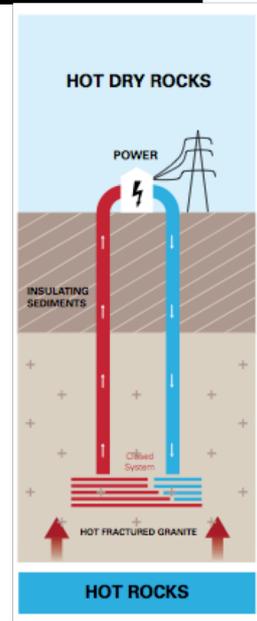
Injected volume:

$$M = \frac{1}{(1-c)} G\alpha_T \Delta V\Delta T_f \frac{1}{(n + (1-n)\frac{\rho_R c_R}{\rho_f c_f})} \left\{ \begin{array}{l} \nu = 0.25 \\ \mu = 0.6 \end{array} \right\}$$

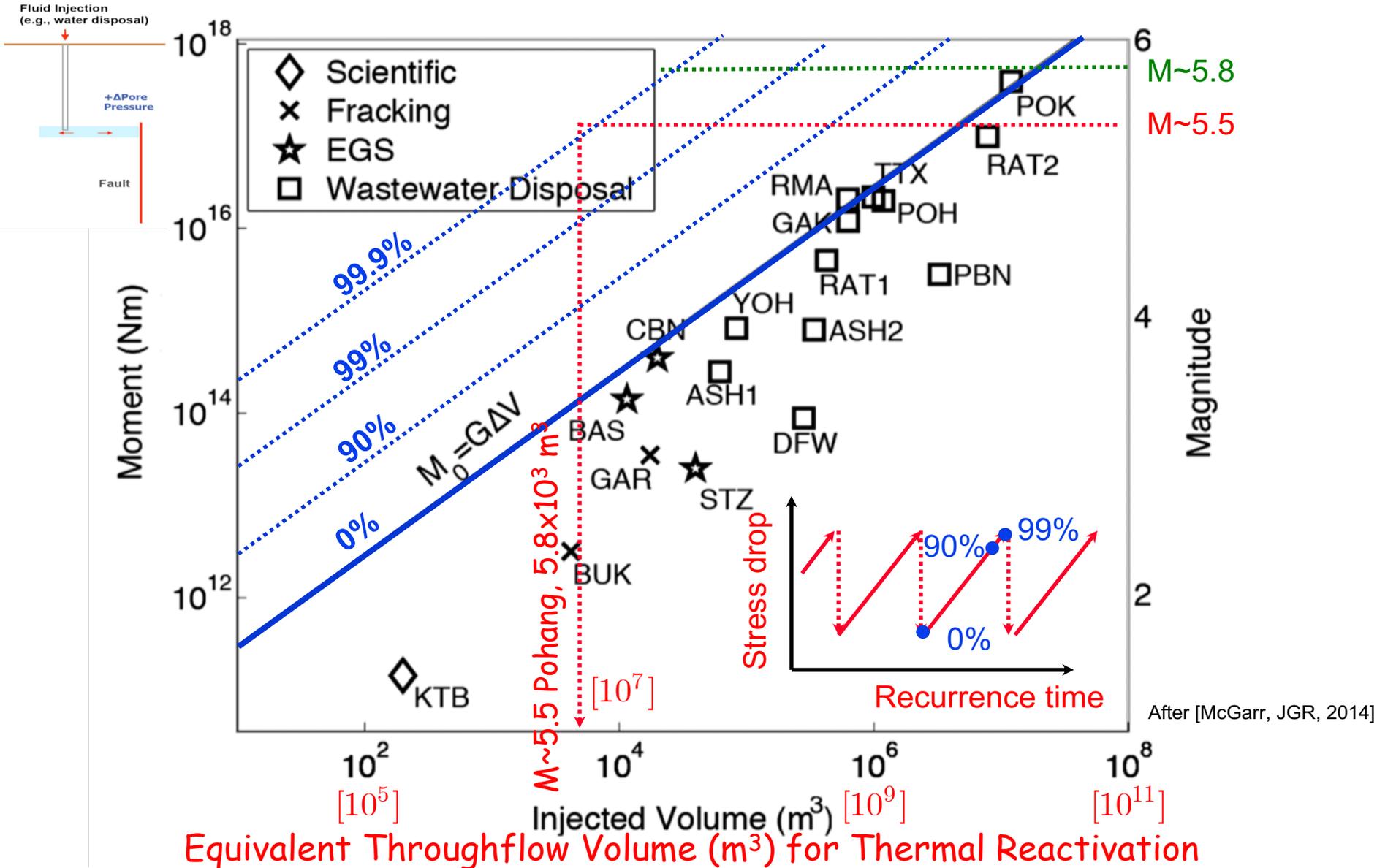
For an open and circulating system (last term loses the preceding porosity):

$$M = \frac{1}{(1-c)} G\Delta V \underbrace{\left[\alpha_T \Delta T_f \frac{1}{(1-n)} \frac{\rho_f c_f}{\rho_R c_R} \right]}_{\text{postfactor}} \left\{ \begin{array}{l} \nu = 0.25 \\ \mu = 0.6 \end{array} \right\}$$

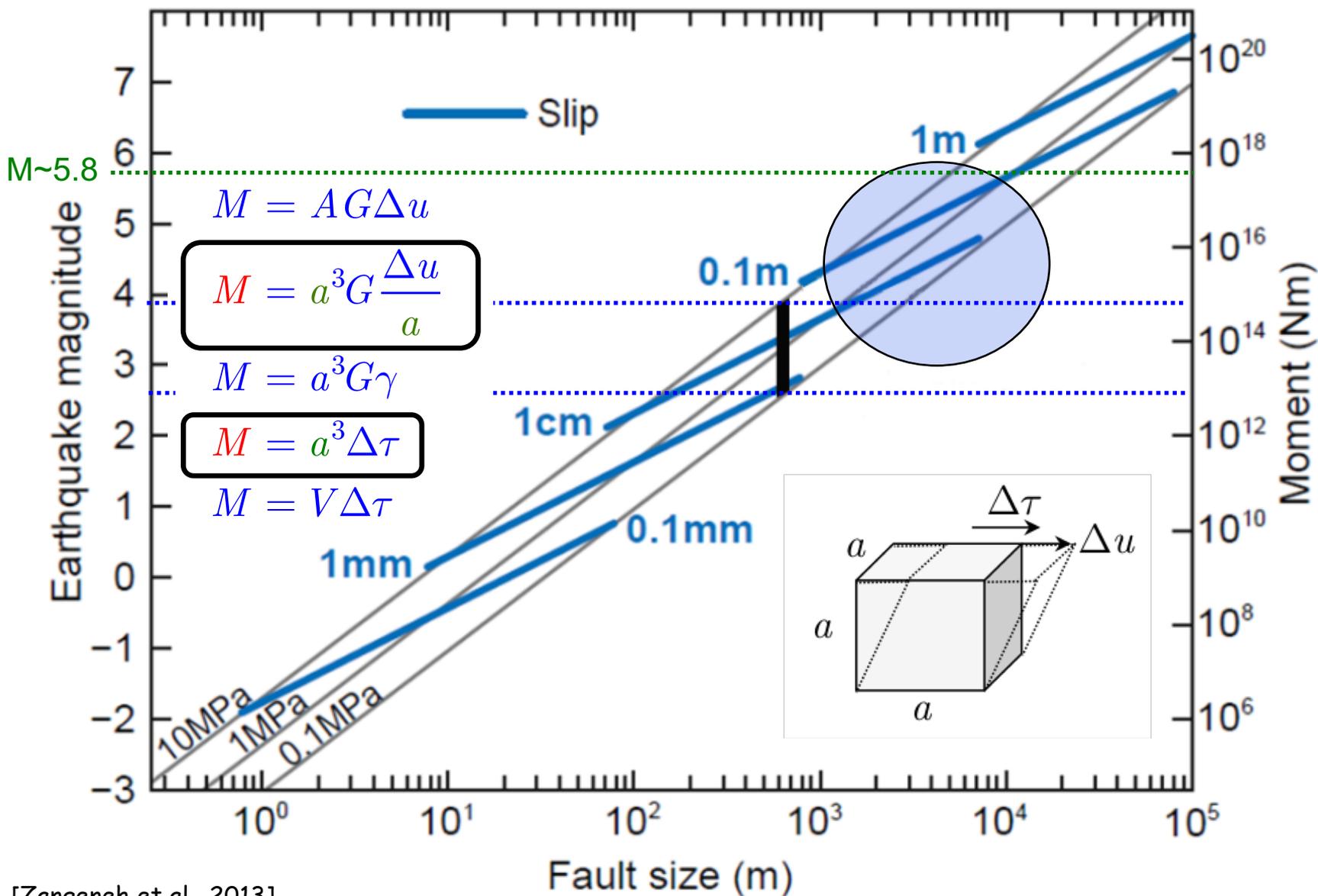
$$\text{postfactor} = O[10^{-5}(\frac{1}{K}) \times 100(K) \times 1 \times \frac{1}{2}] \sim 10^{-3}$$



Fluid Pressure -versus- Thermal Stressing-based Reactivation



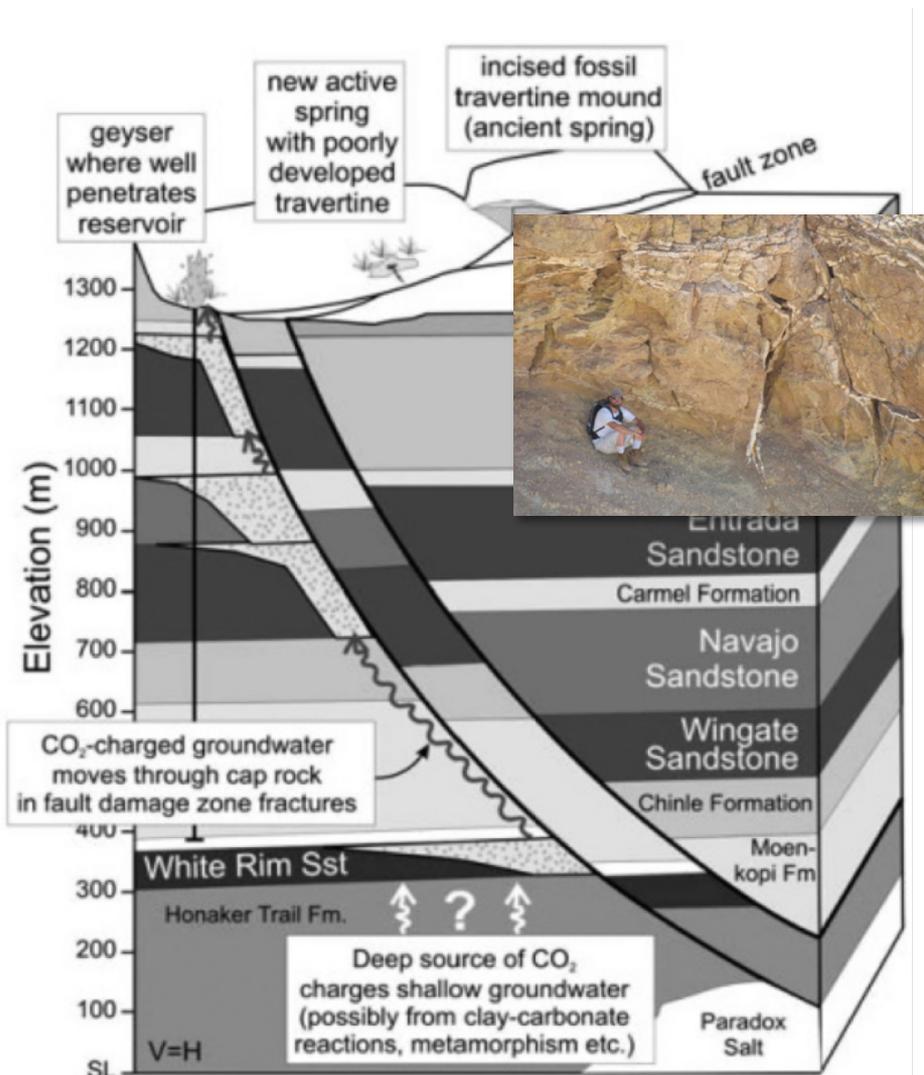
Shear Offset Scaling - Seismic Only



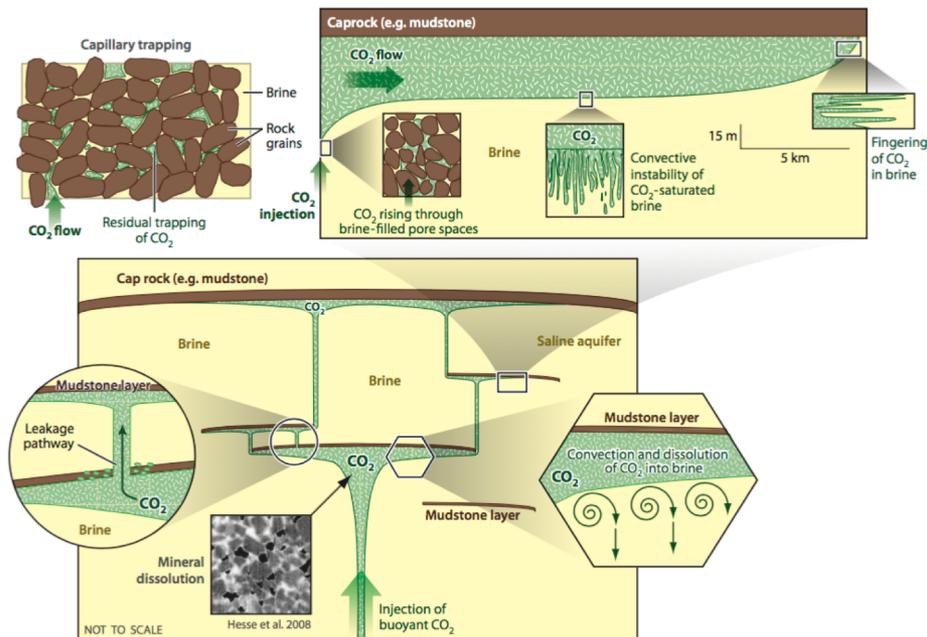
[Zangeneh et al., 2013]

Fault Zones as Seals and Pathways

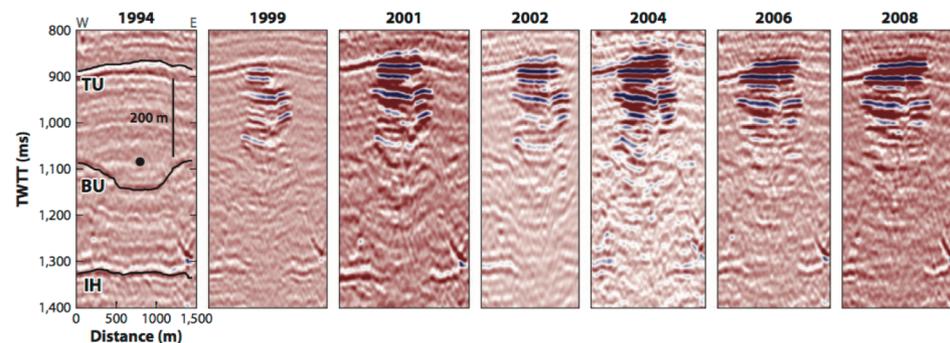
Little Grand Wash Fault, UT



[Patil et al., 2017; after Vrolijk et al., 2005]

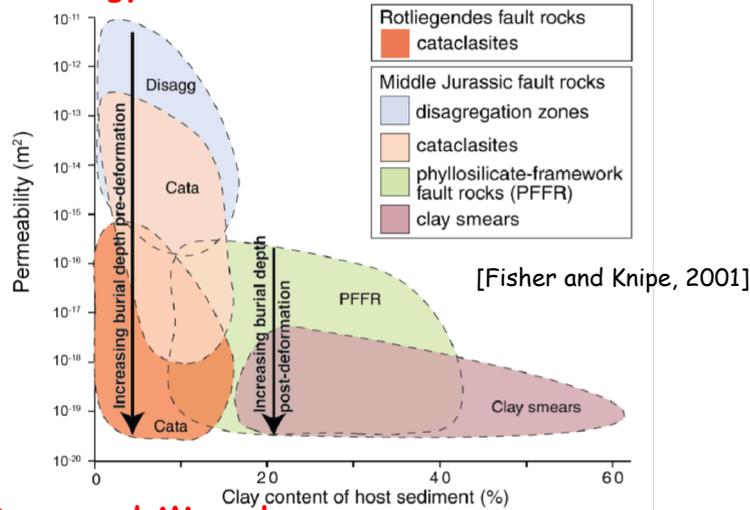


[Huppert and Neufeld, Ann. Rev. Fluid Mechs., 2014]

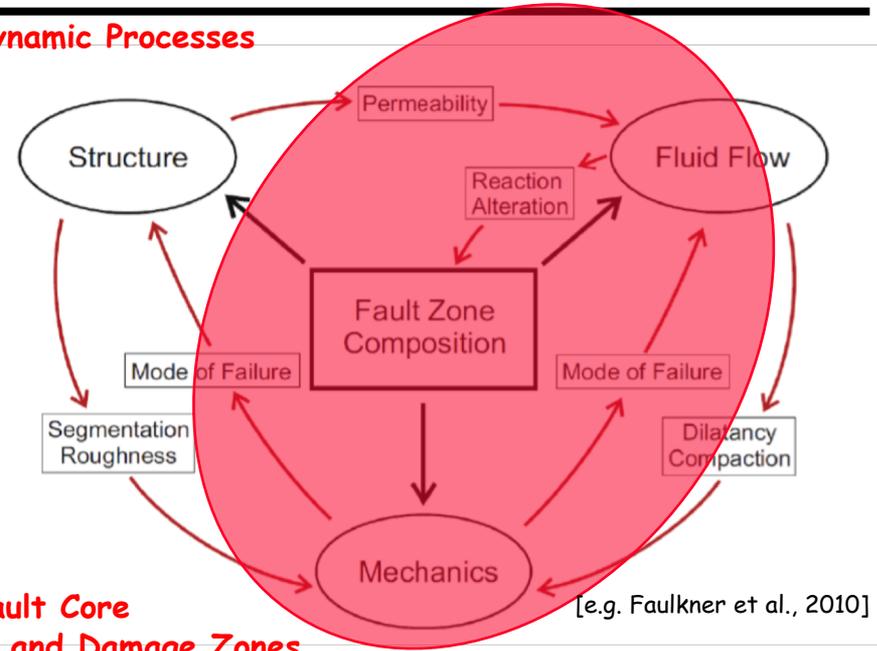


Controls on Permeability Structure

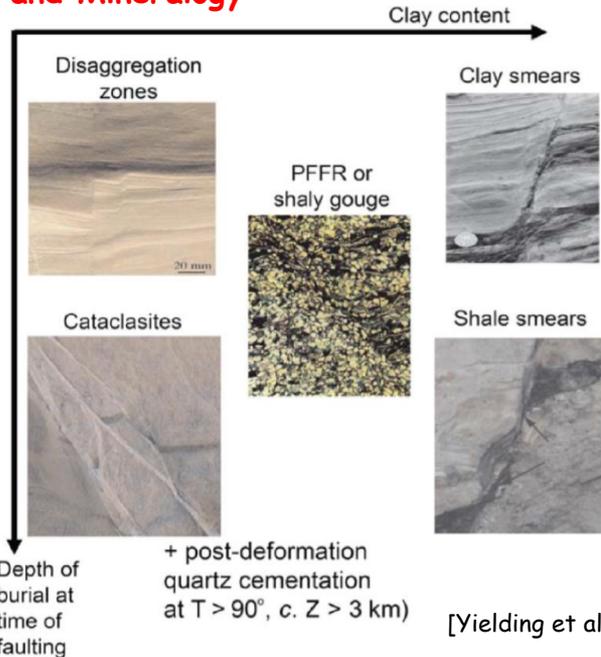
Mineralogy



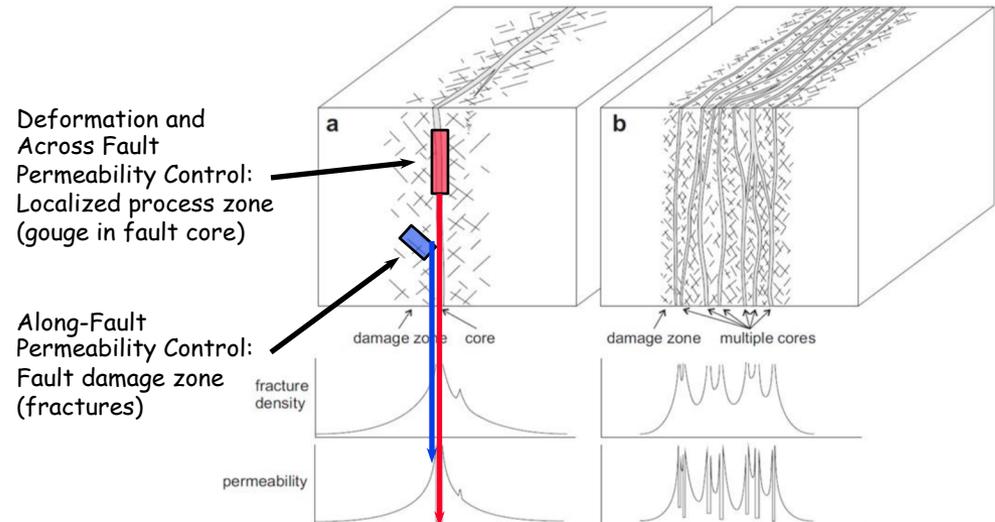
Dynamic Processes



Stress and Mineralogy

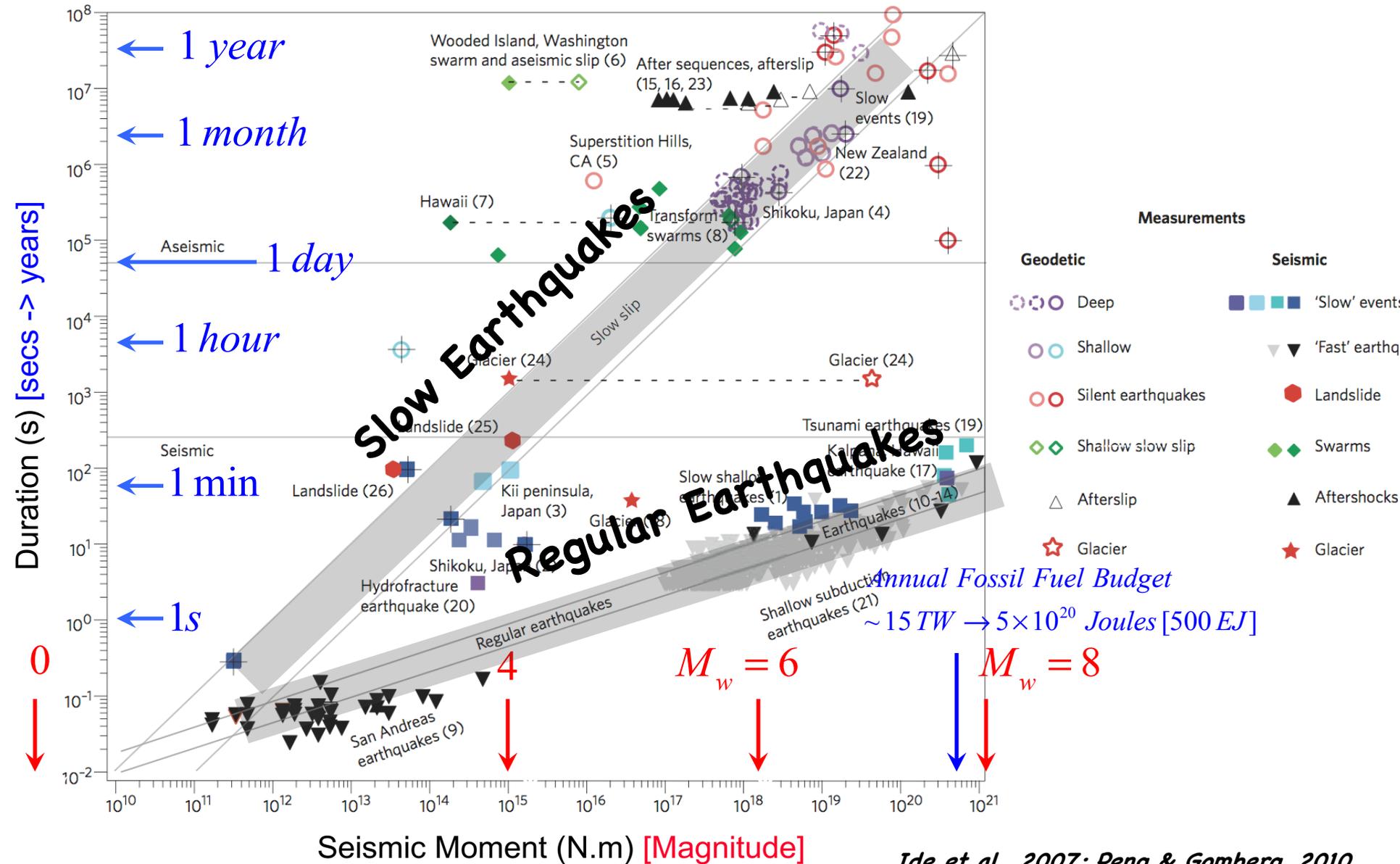


Fault Core and Damage Zones



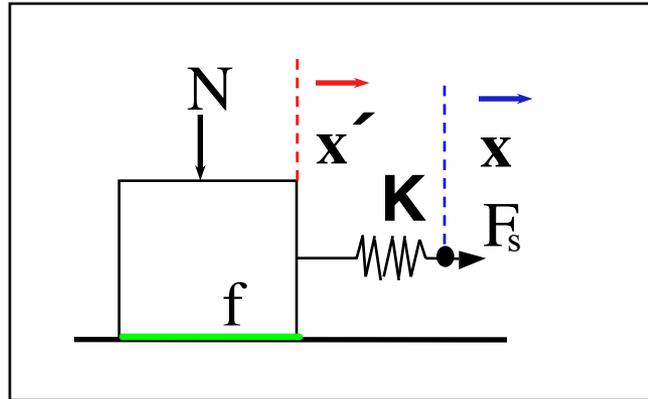
[IEAGHG, "Fault Permeability," 2016; after Faulkner et al., 2010]

Subduction Zone Megathrusts and the Full Spectrum of Fault Slip Behavior



Brittle Friction Mechanics, Stick-slip

Stick-slip (unstable) versus stable shear

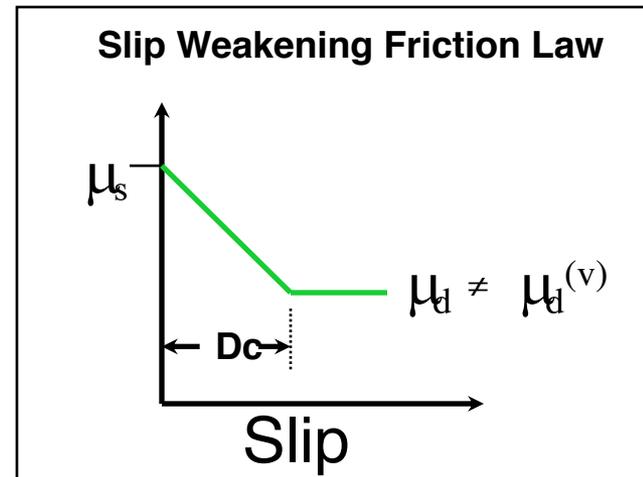
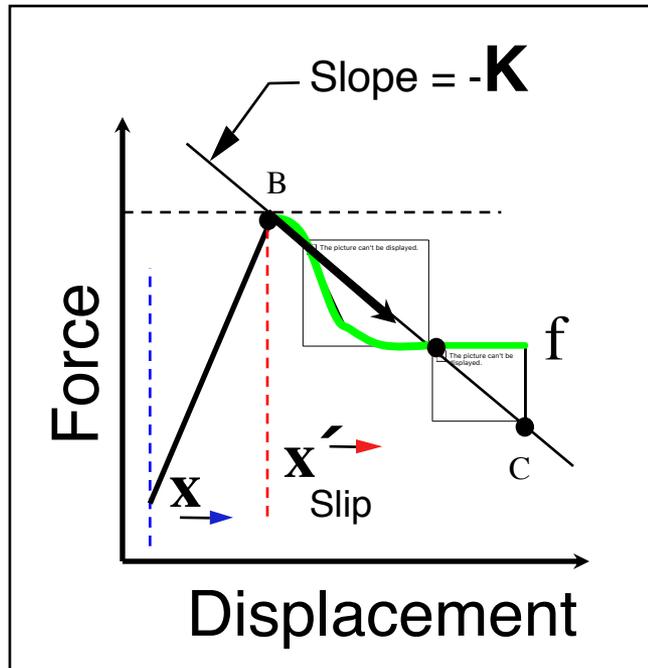


Stick-slip dynamics

$$m\ddot{x}' + \Gamma\dot{x}' + f(\dot{x}', x', t, \theta) = F_s$$

$$m\ddot{x}' + \Gamma\dot{x}' + f(\dot{x}', x', t, \theta) = K(v_{lp} - v)t$$

$$m\ddot{x}' + Fx' = K(v_{lp} - v)t$$



[After C.J. Marone, Pers. Comm., 2017]

Requirements for Instability

1. Shear strength on the fault is exceeded - *i.e.*

$$\tau > \mu \sigma'_n$$

2. When failure occurs, strength is velocity (or strain) weakening - *i.e.*

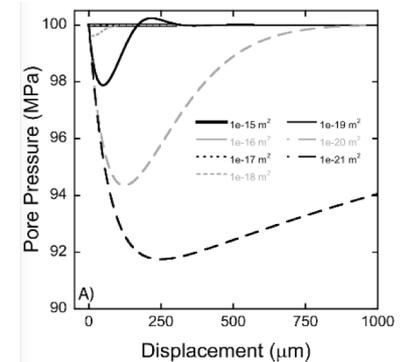
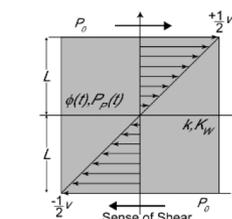
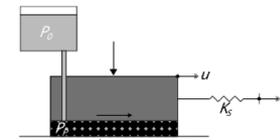
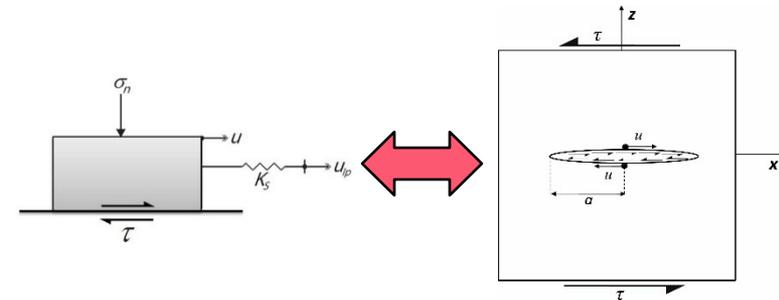
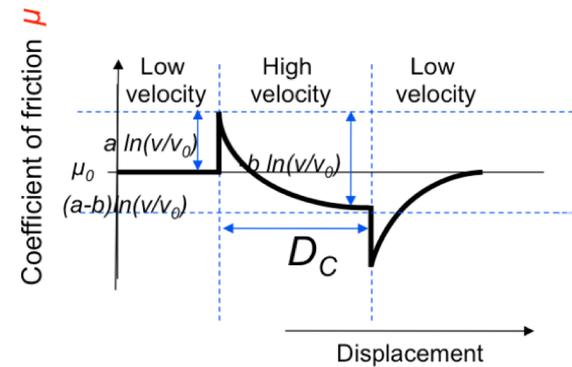
$$a - b < 0$$

2. That the failure is capable of ejecting the stored strain energy adjacent to the fault (shear modulus and fault length) - *i.e.*

$$\frac{G}{l} < K_c = \frac{(b-a)\sigma'_n}{D_c}$$

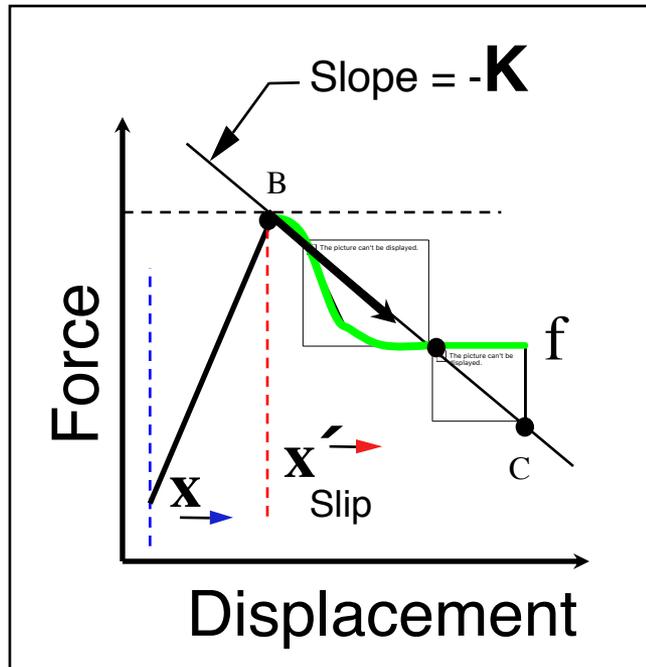
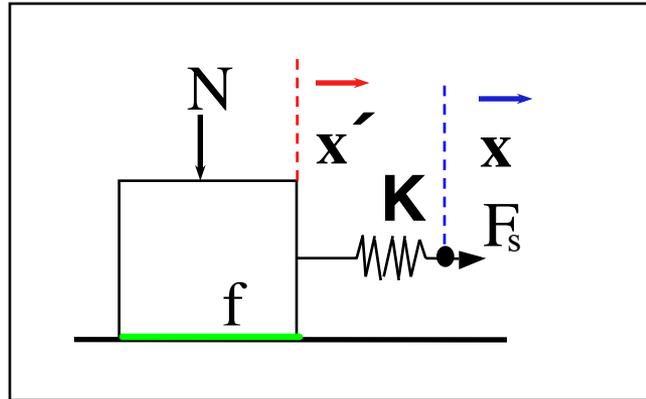
4. That effective normal stresses evolve that do not dilatantly harden the fault and arrest it via the failure criterion of #1 - *i.e.*

$$1 \gg v_D = \frac{w^2}{k} \frac{v_s \eta}{K_s D_c}$$



Seismic - Aseismic Transition

Full Spectrum of Slip Behaviors



$$K_c = -\frac{(\sigma_n - p)(a - b)}{D_c} > \frac{G}{l} = K$$

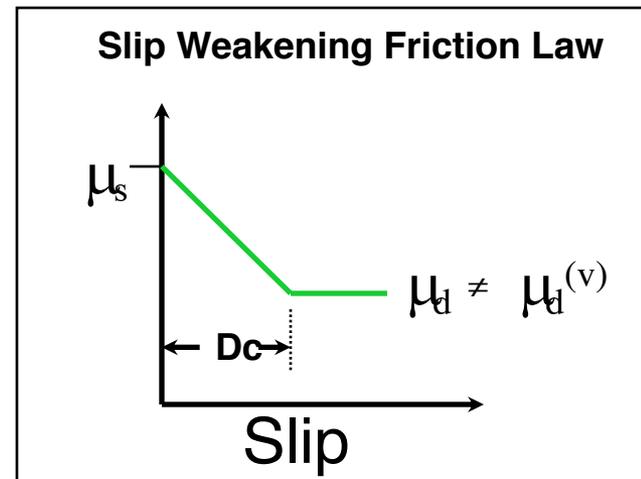
Promote Aseismic Response: $K_c < K$

Otherwise Seismic Slip if: $K_c > K$

Increase: $K_c; (\sigma_n - p); (a - b); l$

Decrease: $D_c; G$

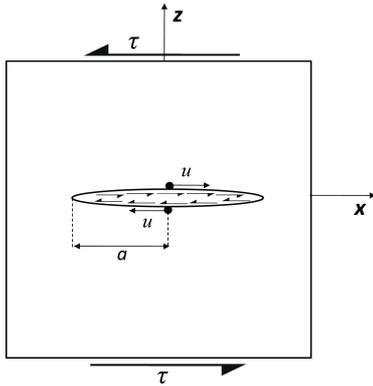
Recurrence Requires: *Healing*



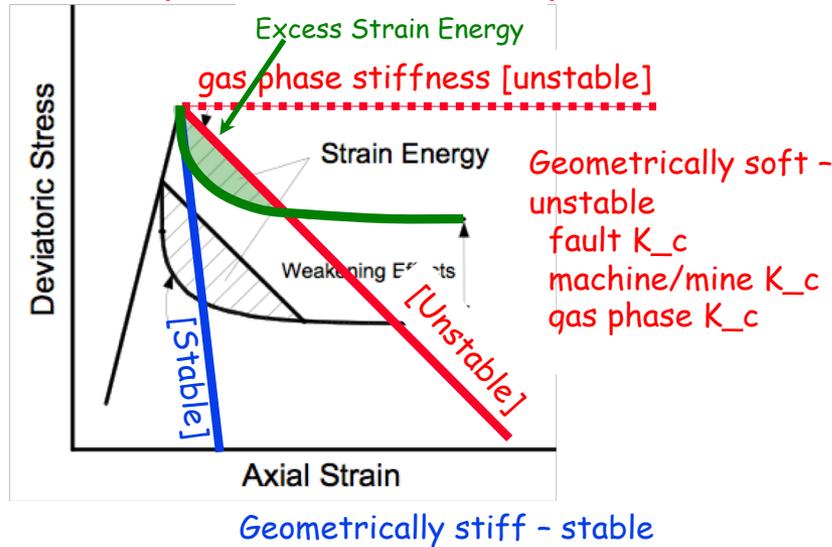
[Adapted from C.J. Marone, Pers. Comm., 2017]

Instability Threshold - Penny-Shaped Crack

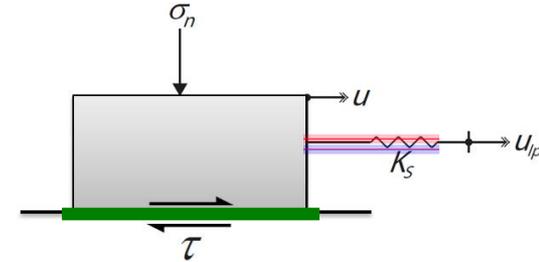
System Stiffness



System-Fault Response



Fault Stiffness



$$\frac{\Delta\tau}{\Delta\bar{u}} = \frac{G}{a} \frac{3\pi(2-\nu)}{8(1-\nu)} < K_c = \frac{(b-a)\sigma'}{D_c} \left[1 + \frac{mv^2}{\sigma' a D_c} \right]$$

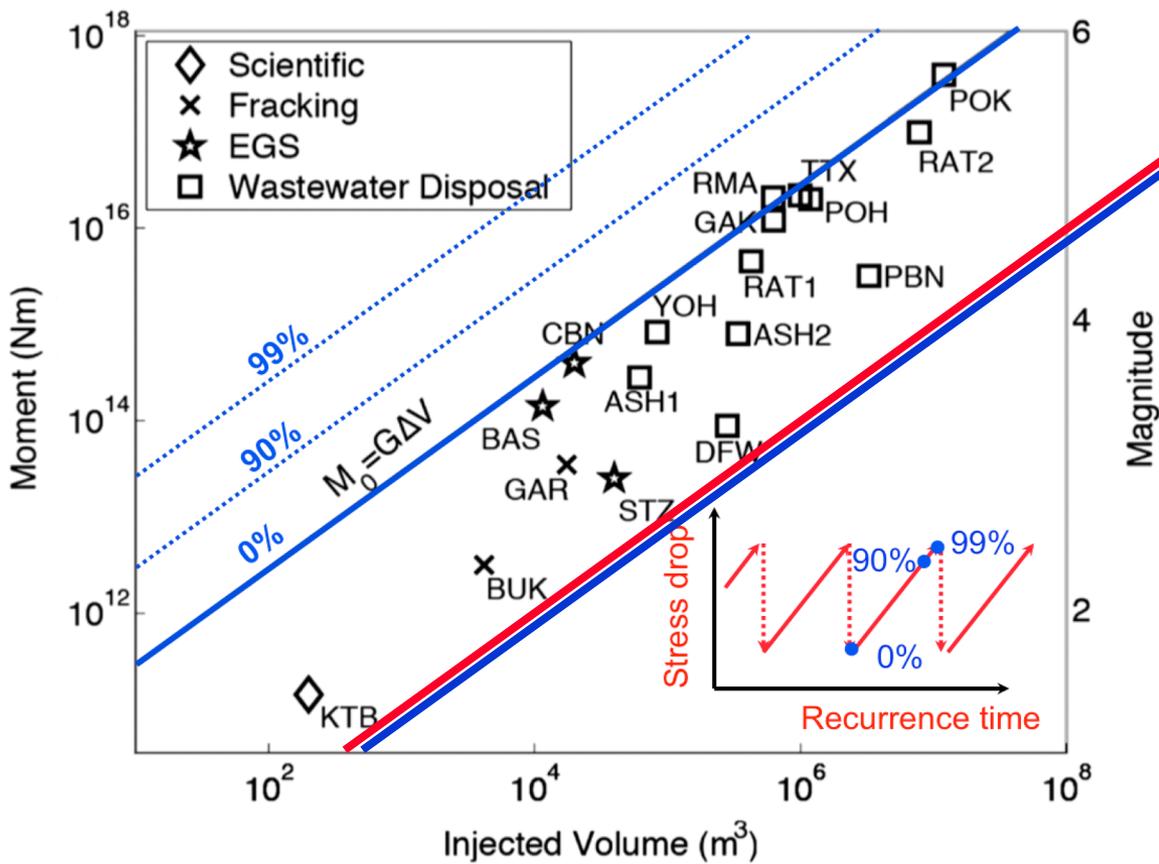
$$\sim 5 \frac{G}{2a} < \frac{(b-a)\sigma'}{D_c} = K_c \left\{ \begin{array}{l} \nu = 0.25 \\ \mu = 0.6 \\ \text{inertia negligible} \end{array} \right.$$

Instability Threshold - Penny-Shaped Crack

Stored strain energy: $M \sim \frac{1}{(1-c)} \frac{1}{3} G \Delta V$

Instability criterion: $M \sim \frac{1}{(1-c)} \frac{1}{3} G \Delta V \cdot \left[\frac{6}{K_c} \frac{G}{2a} \right]$

$$2a = 6 \frac{G}{K_c}$$



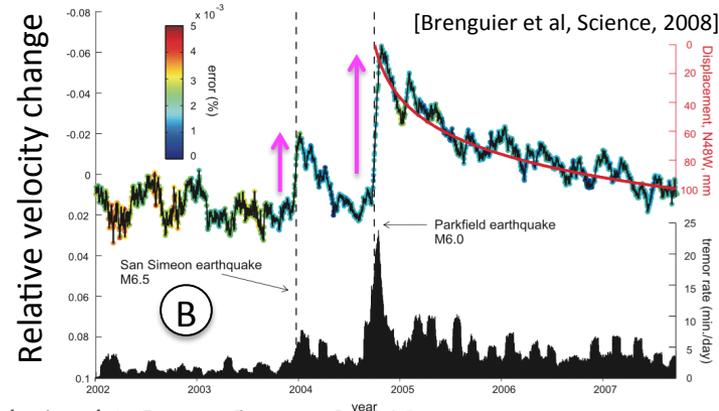
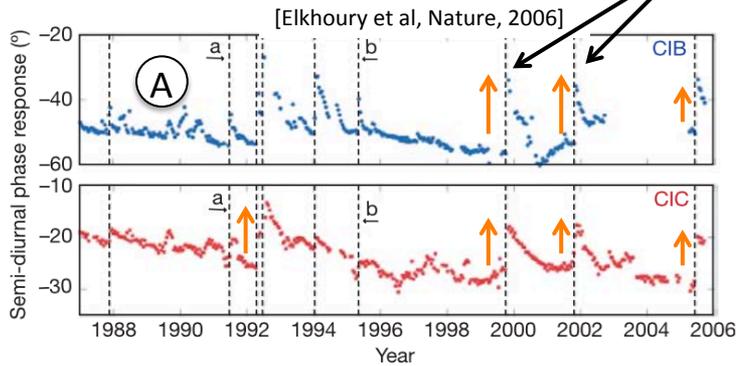
Unstable?
Stable?

Permeability and Elastic Softening

Field-scale

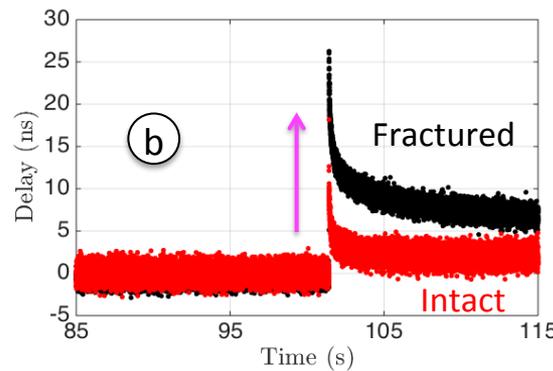
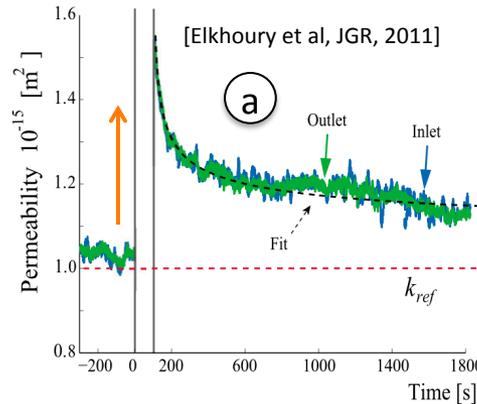
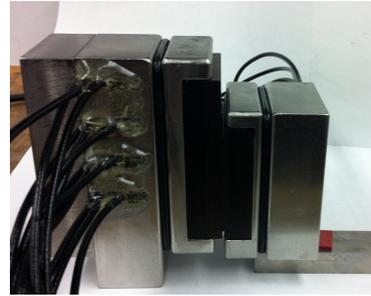


earthquakes



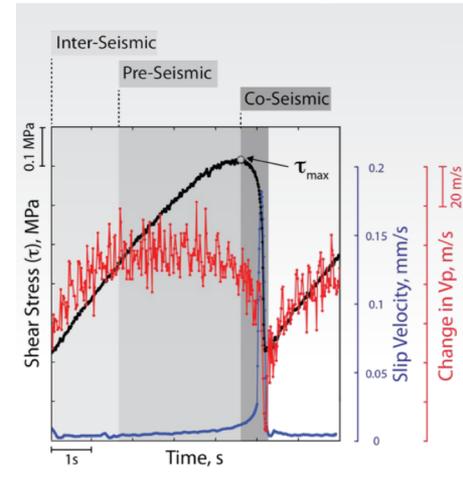
[Shokouhi, Pers. Comm. 2016]

Laboratory-scale



During the Seismic Cycle

- Seismic waves trigger transient changes in elastic properties
- Elastic softening coincides with increased permeability
- Lab observations of precursors to earthquake-like failure (i.e., elastic wave speed)
- Monitoring to assess the critical stress-state in Earth's crust
- Potential for management of induced seismicity to maximize geothermal energy production



[Scuderi et al., Nature Geosc, 2016]

Permeability

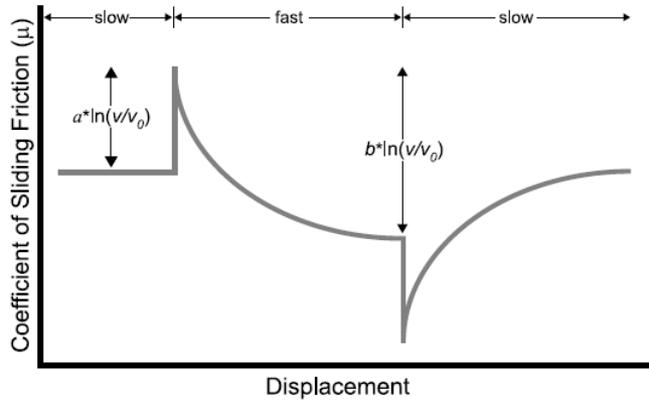
Elastic Softening

Permeability

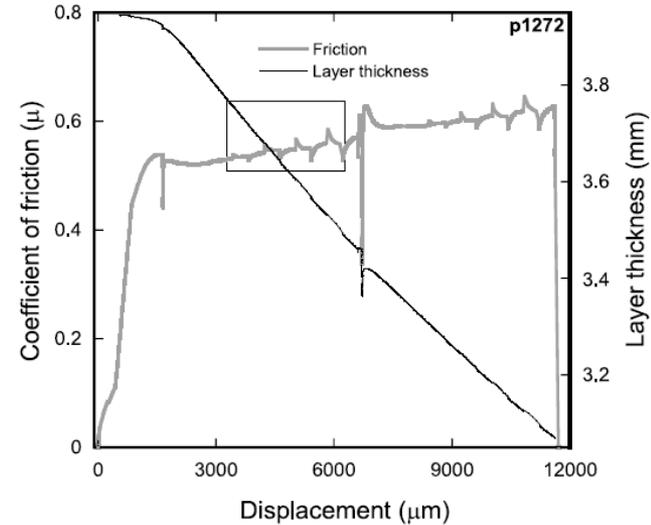
Elastic Softening

Rate-State Friction [1]

Velocity Steps



Multiple Velocity Steps



R-S Friction

$$\left. \begin{aligned} \mu &= \mu_0 + a \ln\left(\frac{v}{v_0}\right) + b \ln\left(\frac{v_0 \theta}{D_C}\right) \\ \frac{d\theta}{dt} &= 1 - \frac{v\theta}{D_C} \quad (\text{Dieterich Evolution}) \\ \frac{d\theta}{dt} &= \frac{-v\theta}{D_C} \ln\left(\frac{v\theta}{D_C}\right) \quad (\text{Ruina Evolution}) \end{aligned} \right\}$$

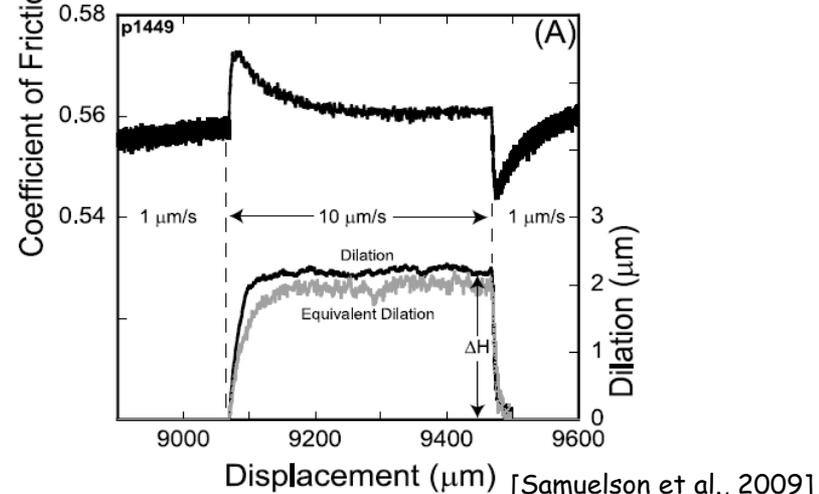
Dilation

$$\frac{\Delta H}{H} \cong \Delta \phi = -\epsilon \ln\left(\frac{v}{v_0}\right) = -\epsilon \ln\left(\frac{v_0 \theta}{D_c}\right)$$

Permeability Evolution

$$\frac{k}{k_0} = \left(1 + \frac{\Delta b}{b_0}\right)^3 = \left(1 + \frac{\Delta H}{H}\right)^3$$

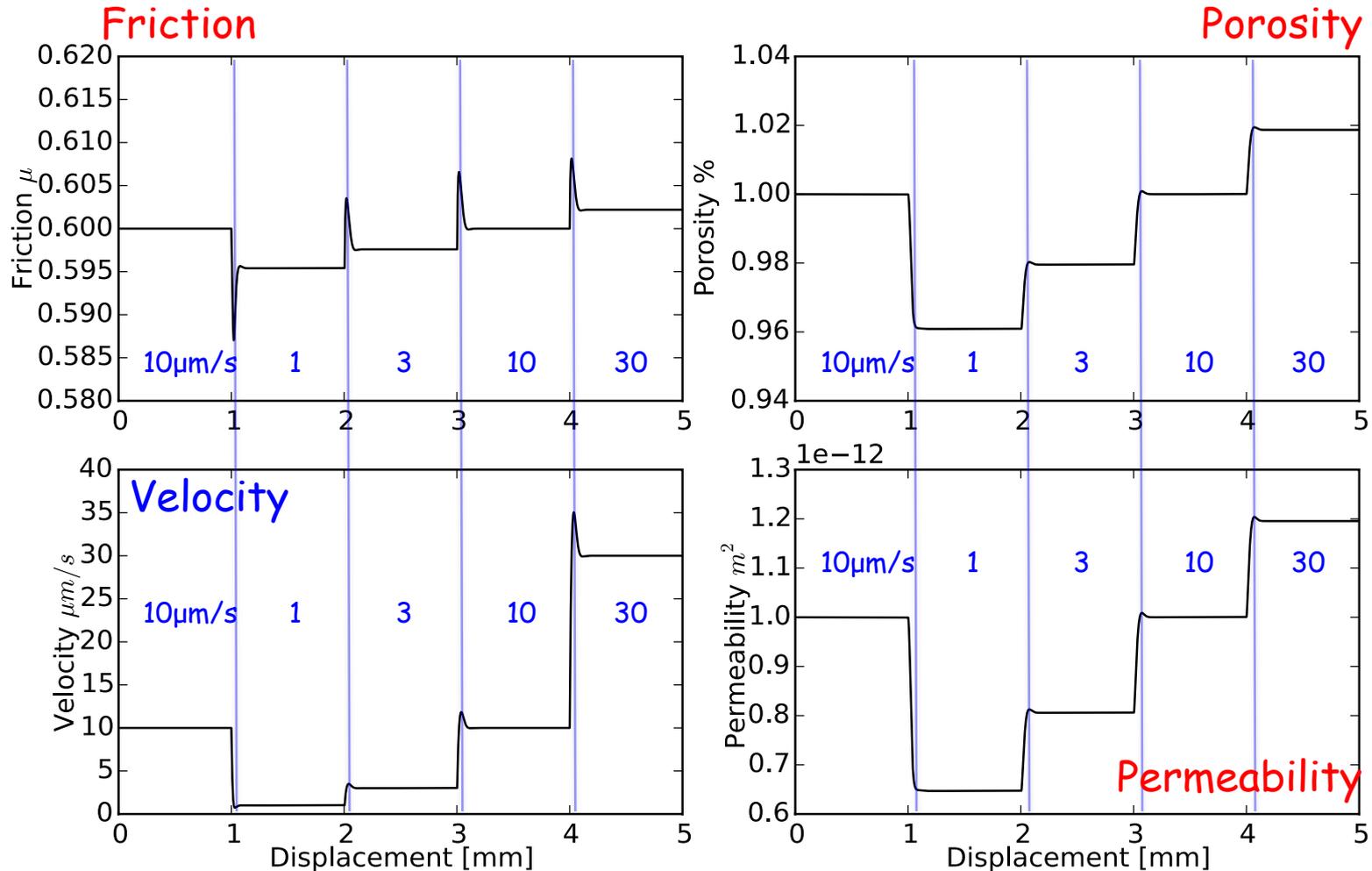
Single Velocity Step



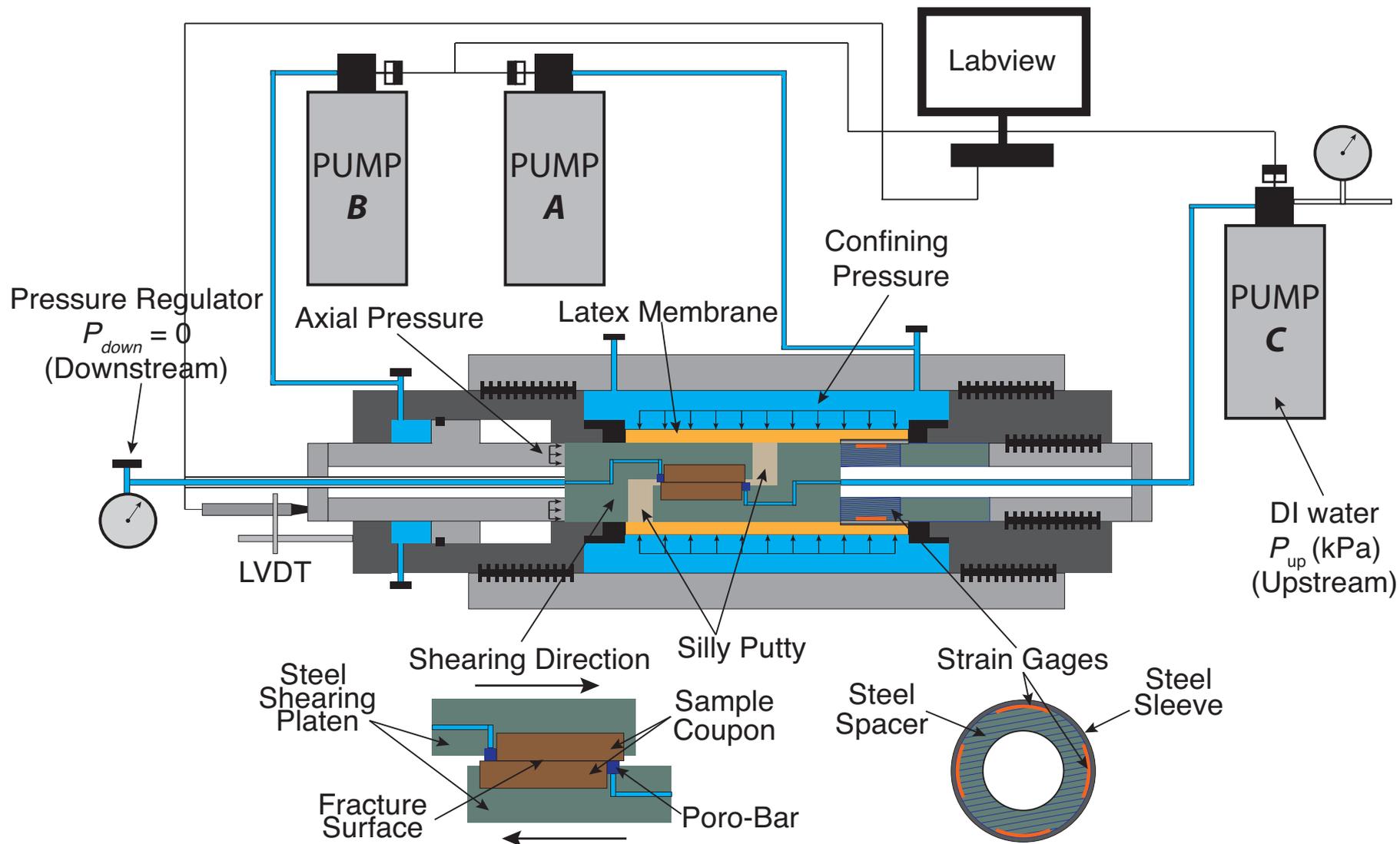
Rational Linkages: Rate-State Friction, Porosity and Permeability

$$\dot{\phi}_{plastic} = -\frac{V}{D_c}(\phi_{plastic} - \phi_{ss}), \quad \phi_{ss} = \phi_0 + \varepsilon \ln\left(\frac{V}{V_0}\right), \quad \frac{k(\phi)}{k_0} = \left(\frac{\phi - \phi_c}{\phi_0 - \phi_c}\right)^n$$

High Stiffness, positive dilatational coefficient

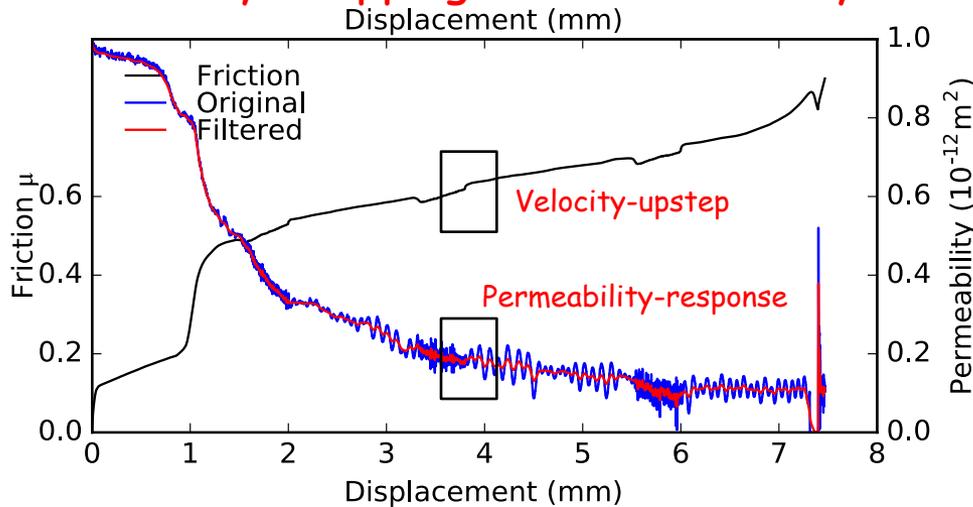


Frictional Stability-Permeability Experiments

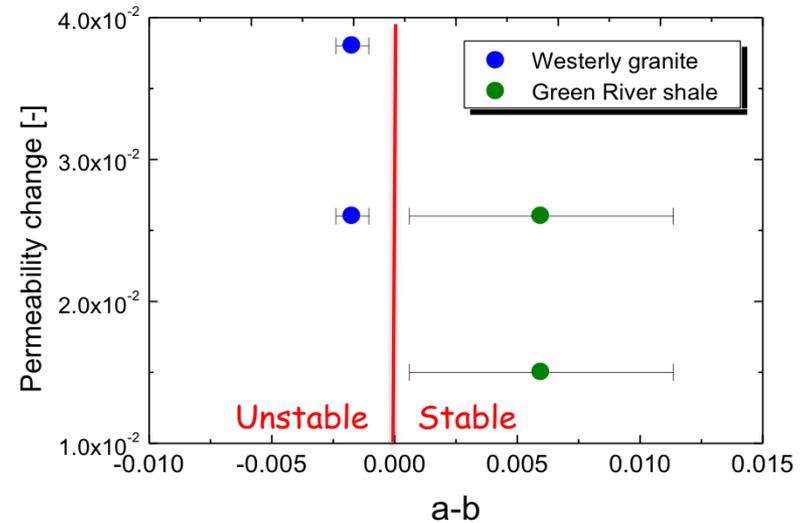


Frictional Stability-Permeability Observations

Velocity-stepping and Permeability

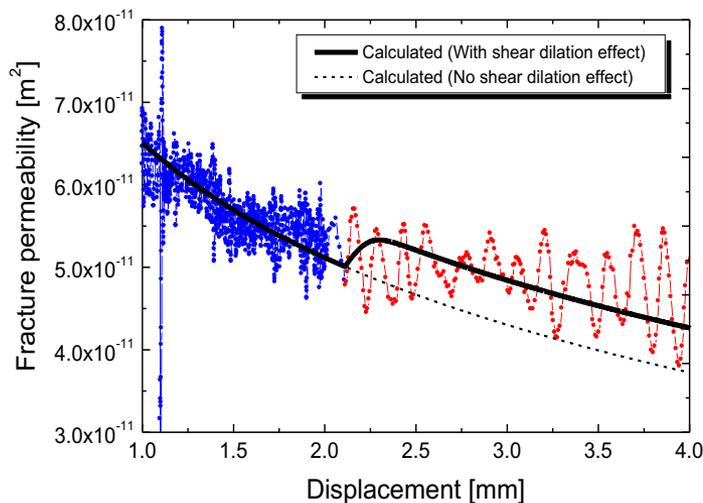


Permeability-Frictional Stability

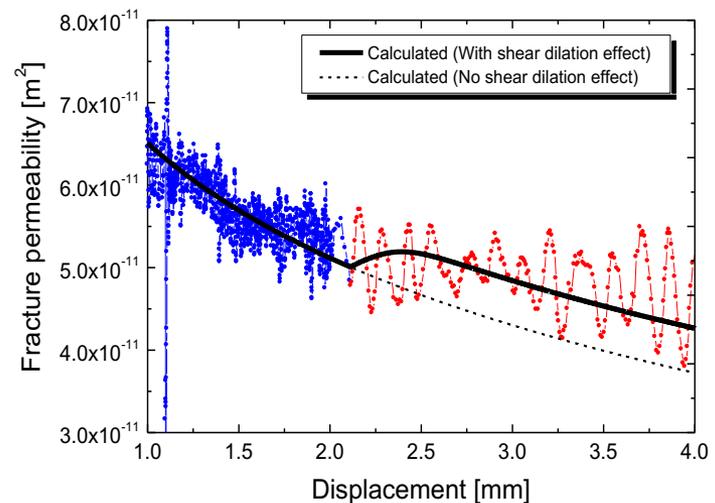


Permeability Evolution

$\varepsilon=0.0224$ ($n=2$), $D_c=50$ [μm]



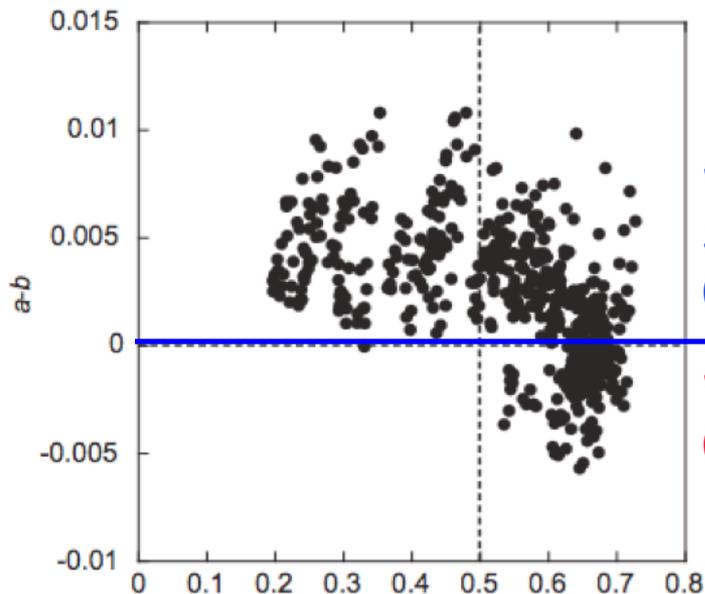
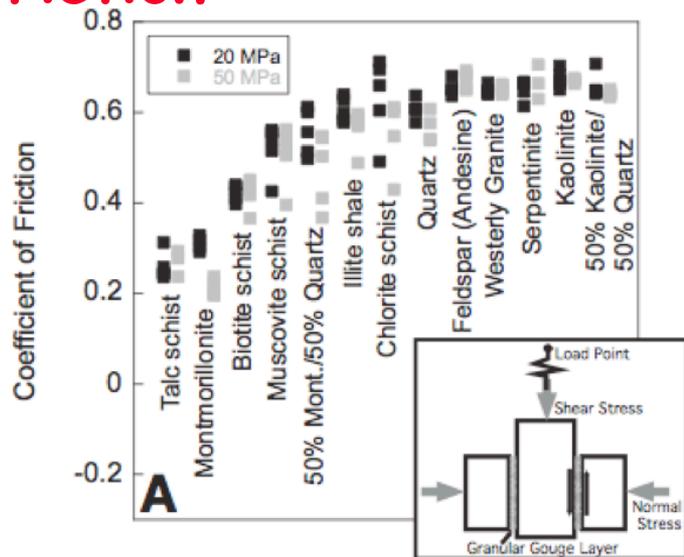
$\varepsilon=0.0224$ ($n=2$), $D_c=100$ [μm]



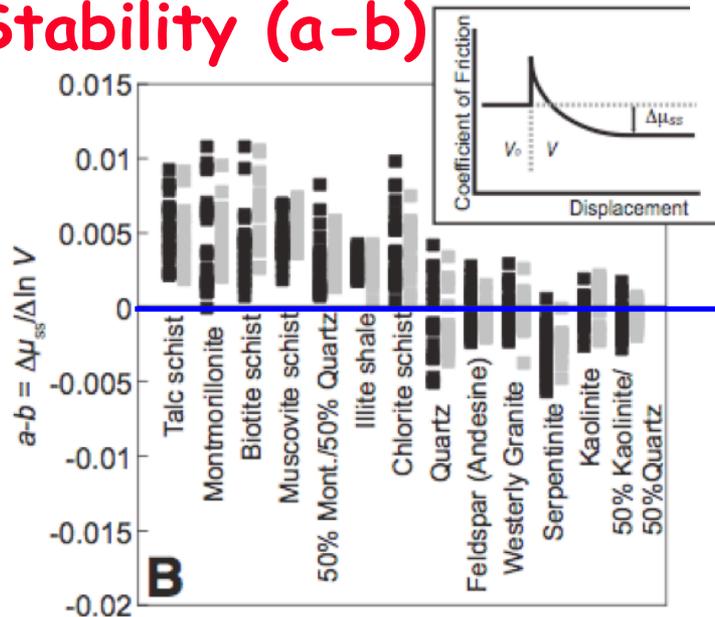
Mineralogical Controls on Instability

Friction

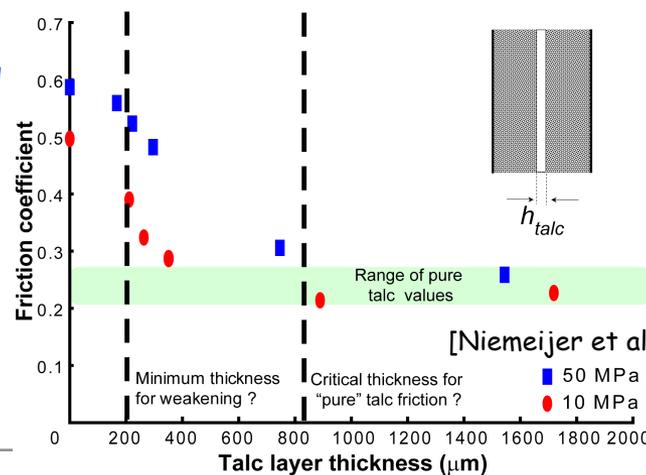
[Ikari et al., *Geology*, 2011]



Stability (a-b)

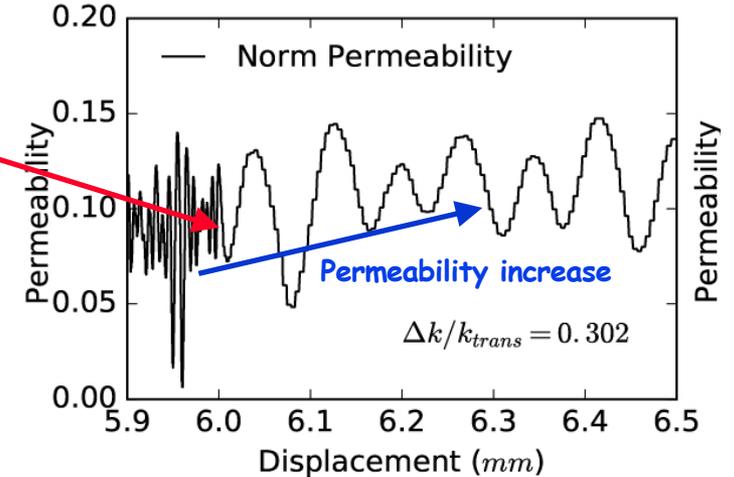
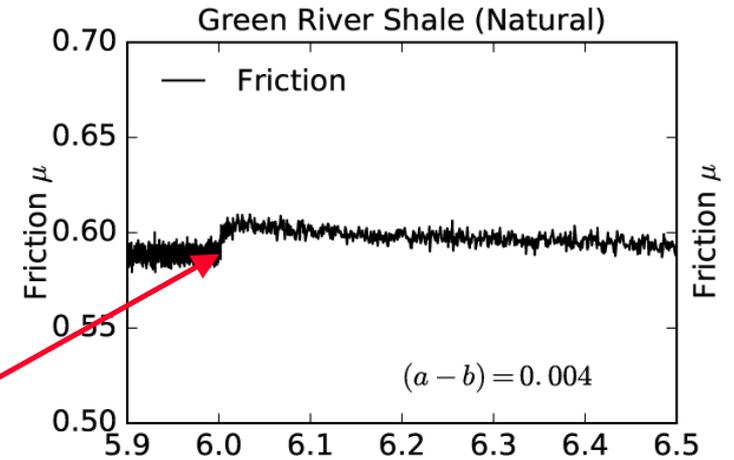
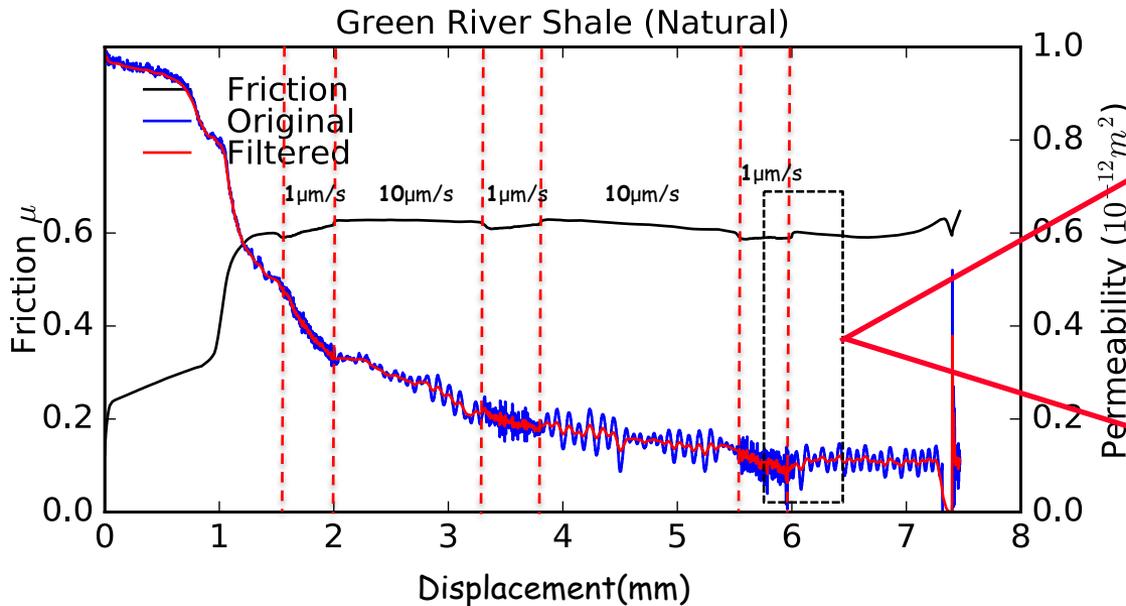


Frictional Response of Mixtures



Green River Shale- Permeability Enhancement

| | Tectosilicate | Carbonate | Phyllosilicate |
|-------------------|---------------|-----------|----------------|
| Green River Shale | 45.44% | 51.96% | 2.60% |



Before



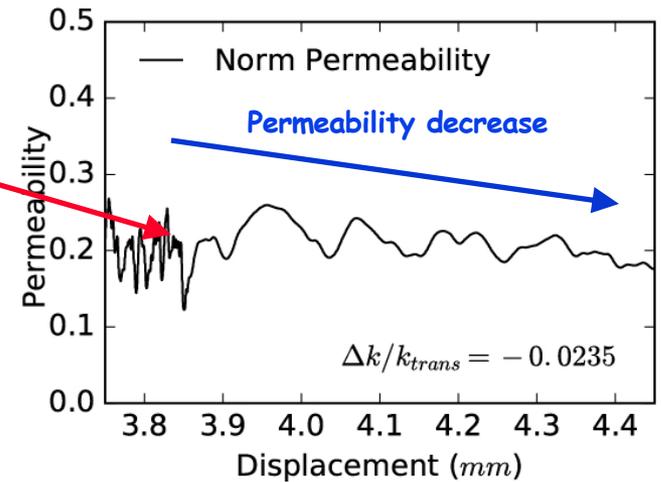
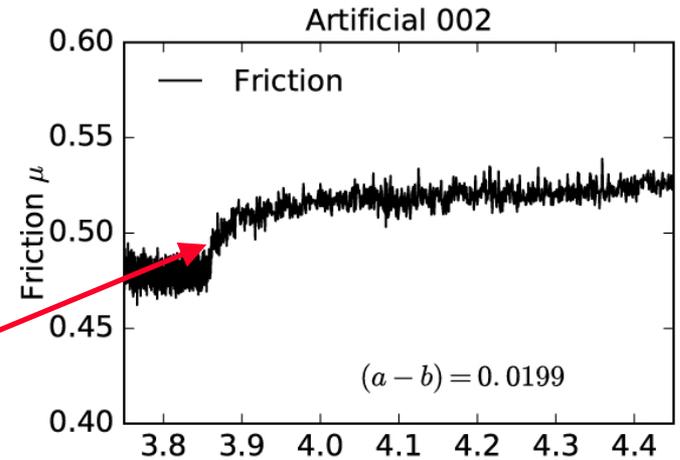
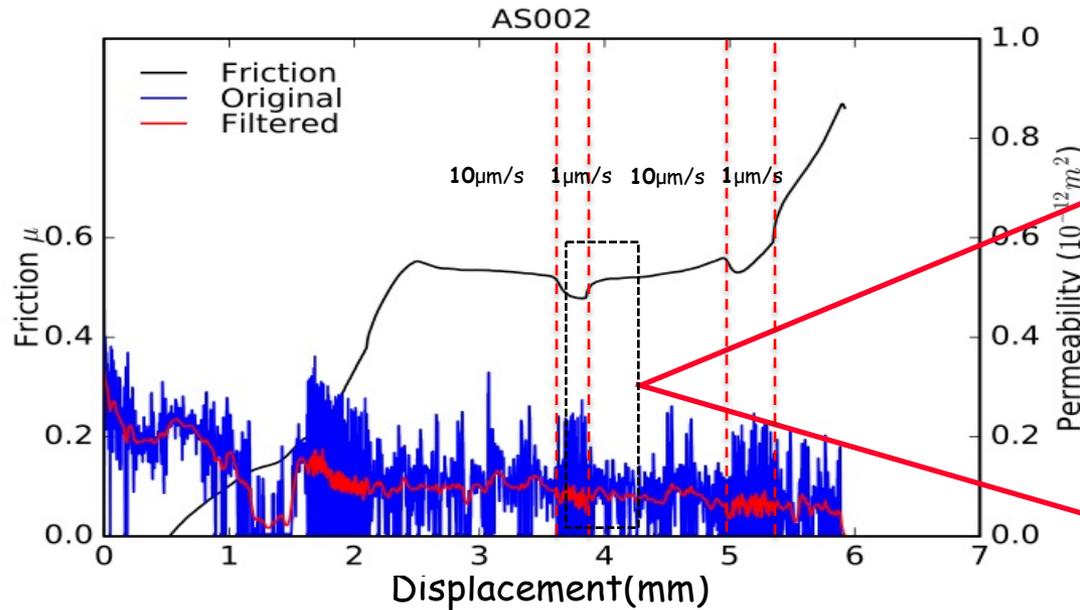
After

Wear products after slip

Velocity-upstep results in a permeability increase due to dilation

Phyllosilicate-dominant Artificial Sample- Permeability Decrease

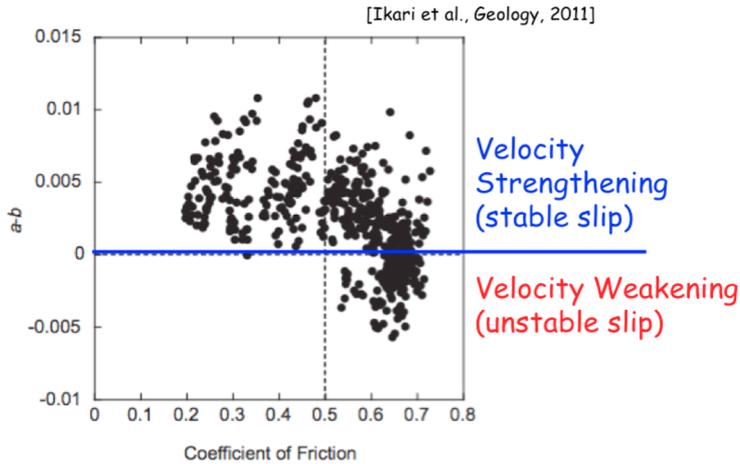
| | Tectosilicate | Carbonate | Phyllosilicate |
|-------|---------------|-----------|----------------|
| AS002 | 10% | 10% | 80% |



Before After
Clay swelling concurrent
with shear damage

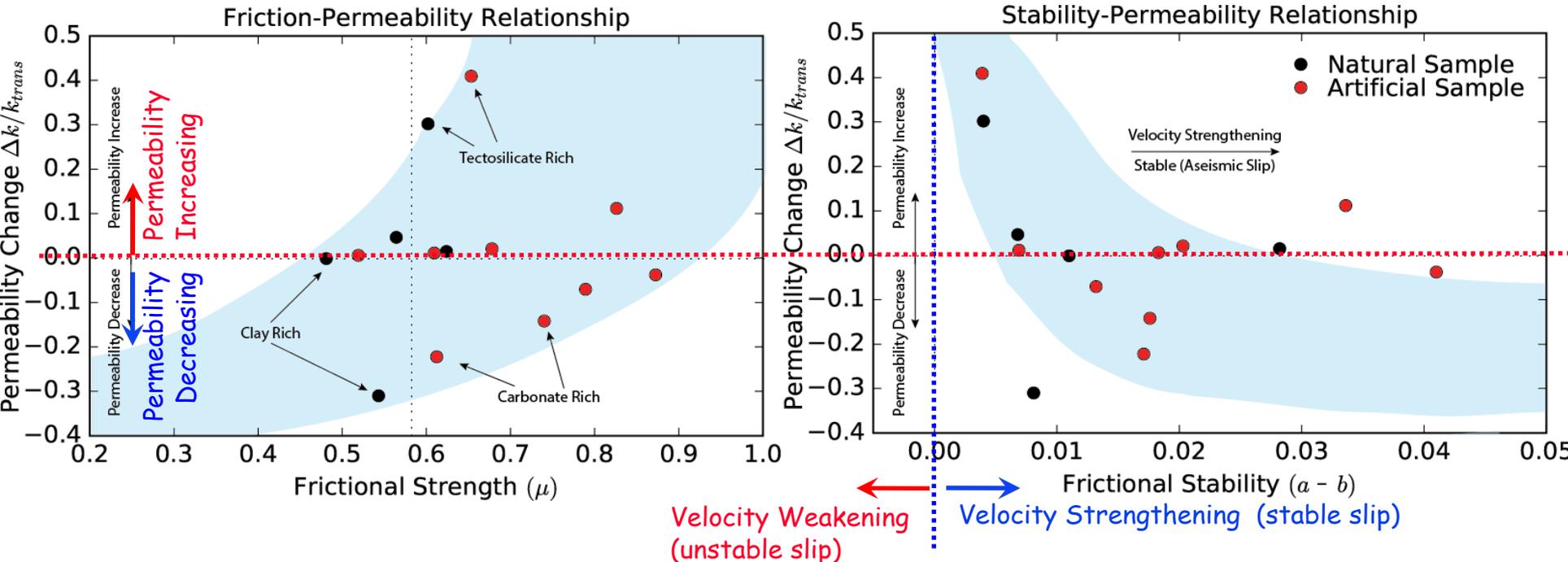
Velocity-upstep results in a permeability decrease due to wear products and swelling

Nascent Friction-Stability-Permeability Relationships



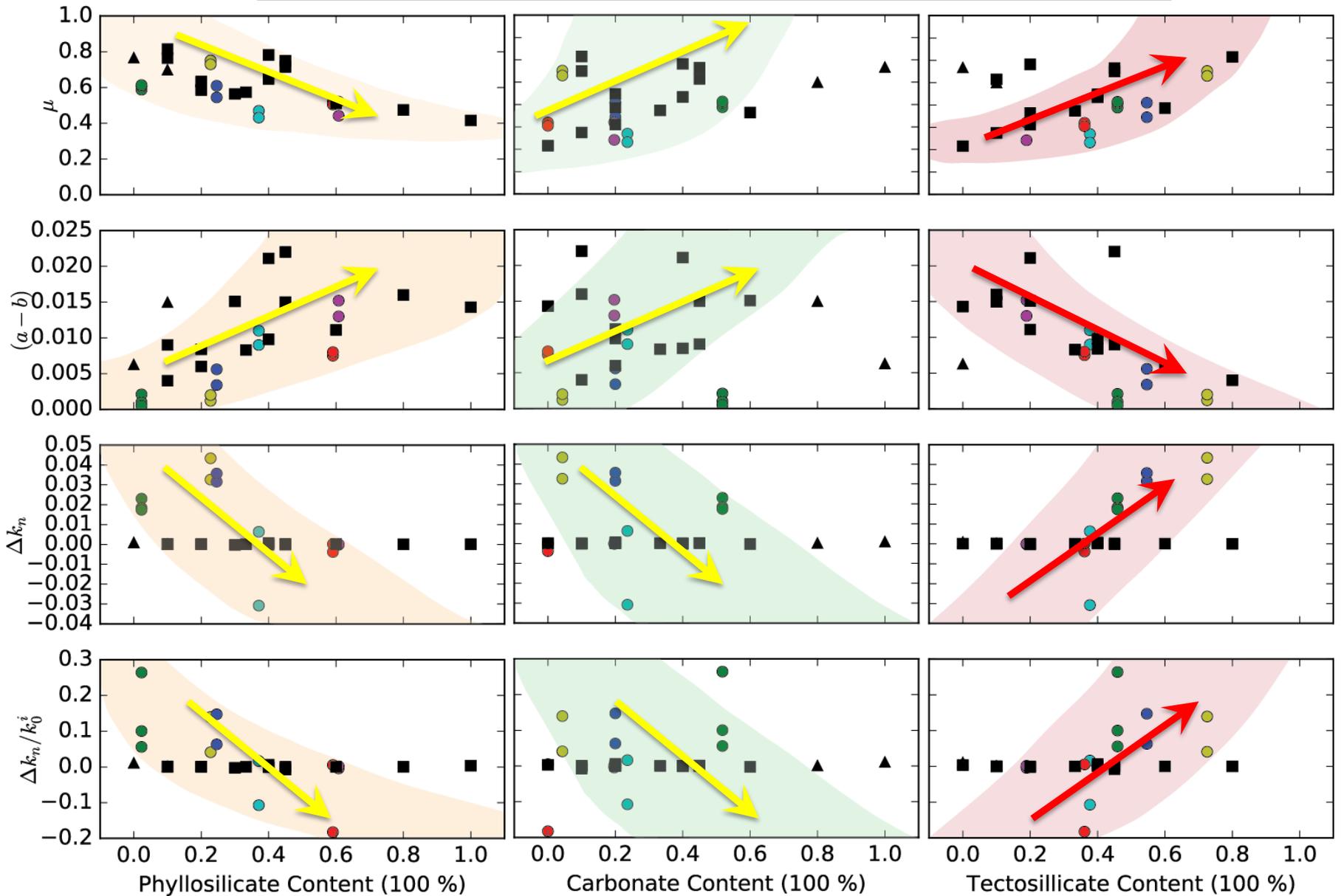
Observations

- dk/k_0 increases with increased brittleness $(a-b) < 0$
- dk/k_0 increases with increased frictional strength
- Roles of mineralogy and surface roughness?



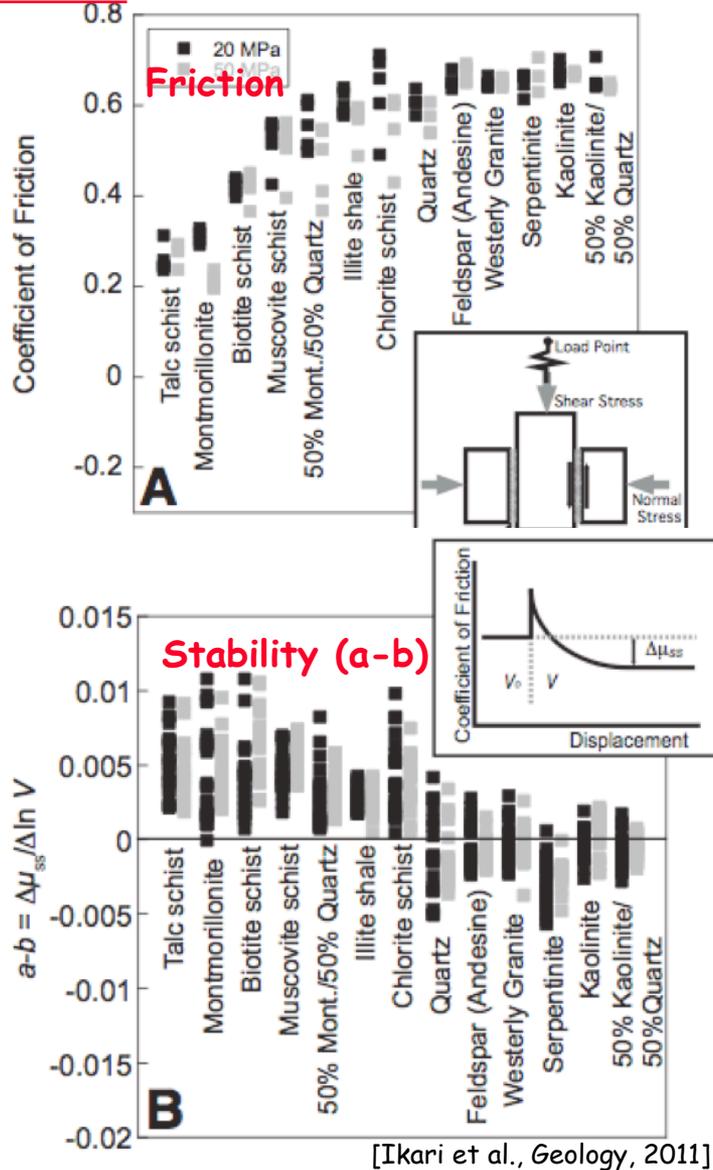


Seismicity-Permeability Linkages – Natural Samples

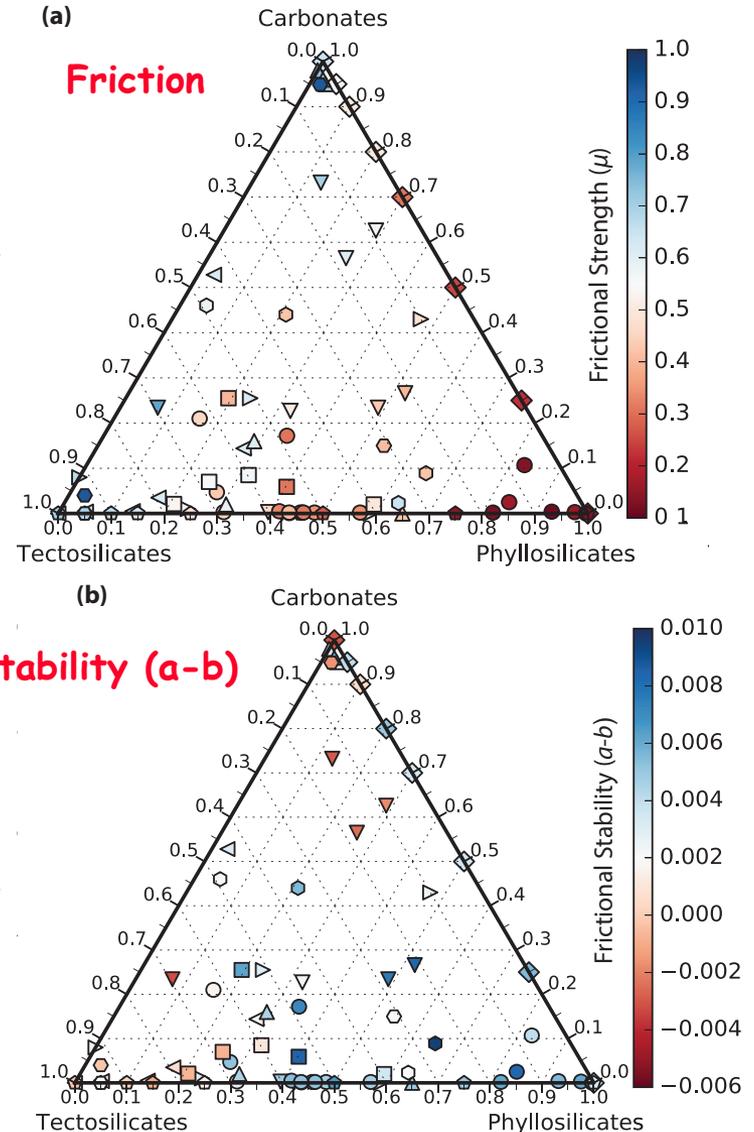


Stability-Permeability Relations in Composites/Mixtures

Mono-mineralic

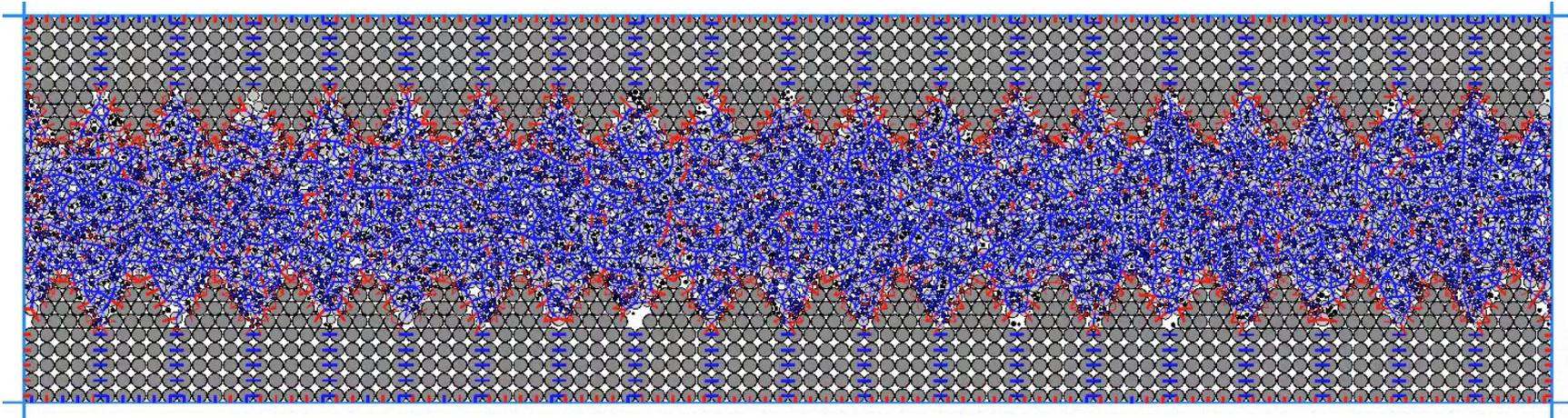


Multi-mineralic

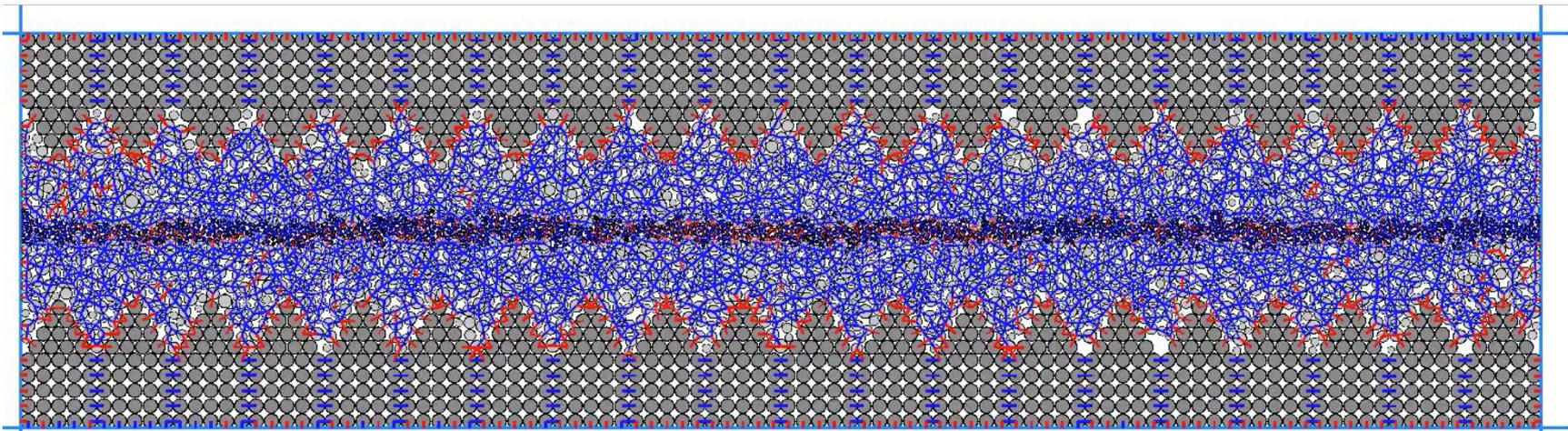


Role of Texture in Friction-Stability-Permeability

Heterogeneous Mixture

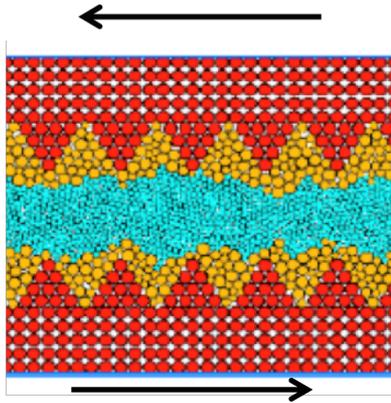


Textured/Layered Mixture

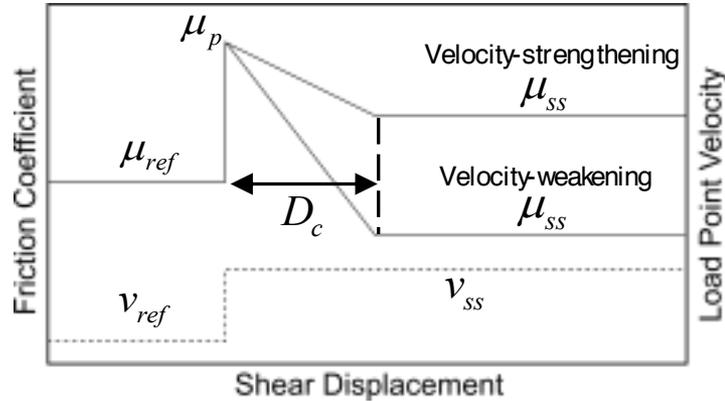


Multi-Mineral Frictional Strength

DEM Model



Particle-Particle Friction



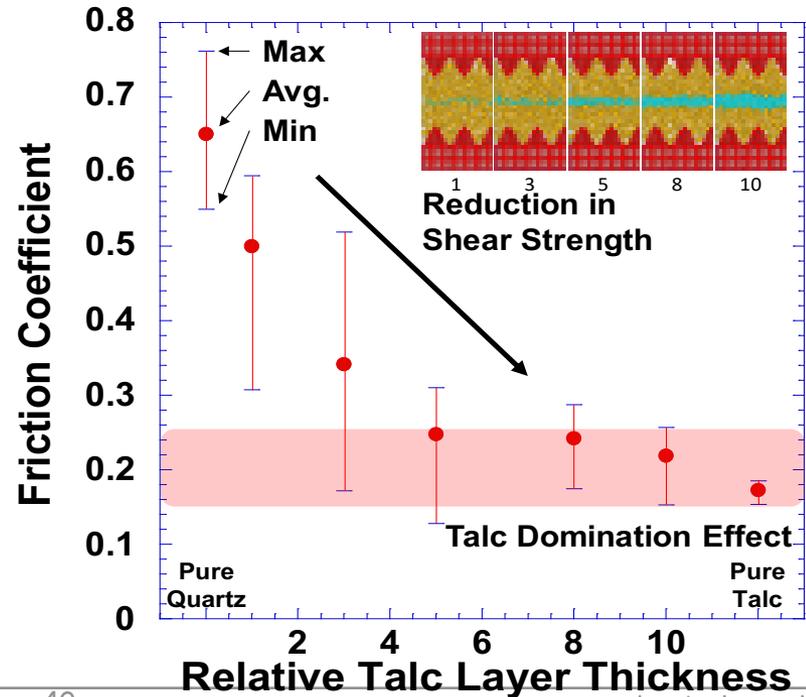
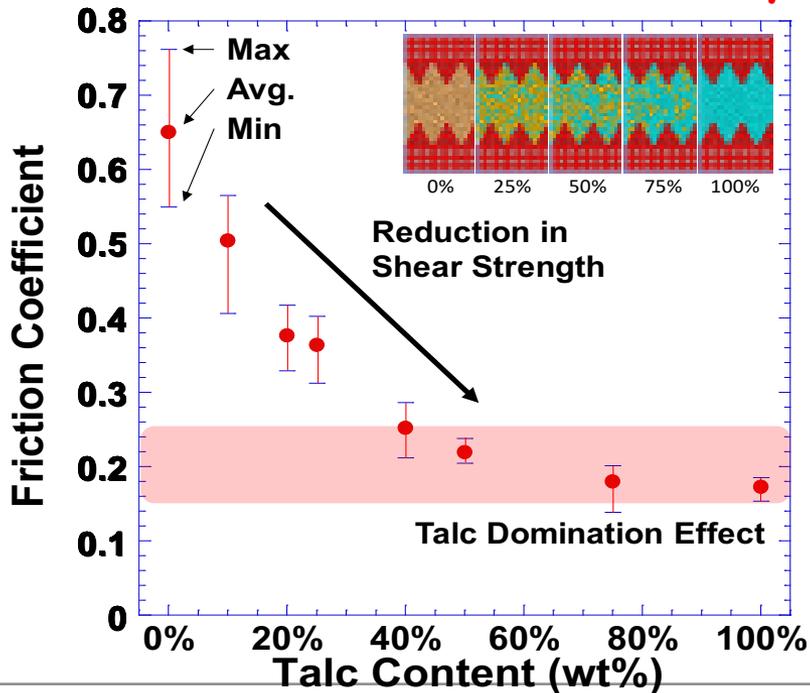
RSF Notation

$$\mu_p = \mu_{ref} + a \ln \left(\frac{V_{ss}}{V_{ref}} \right)$$

$$\mu_{ss} = \mu_{ref} + (a-b) \ln \left(\frac{V_{ss}}{V_{ref}} \right)$$

$$\mu = \begin{cases} \mu_p & D_{acc} = 0 \\ \mu_p - \left(\frac{\mu_p - \mu_{ss}}{D_c} \right) D_{acc} & D_{acc} \in (0, D_c) \\ \mu_{ss} & D_{acc} = D_c \end{cases}$$

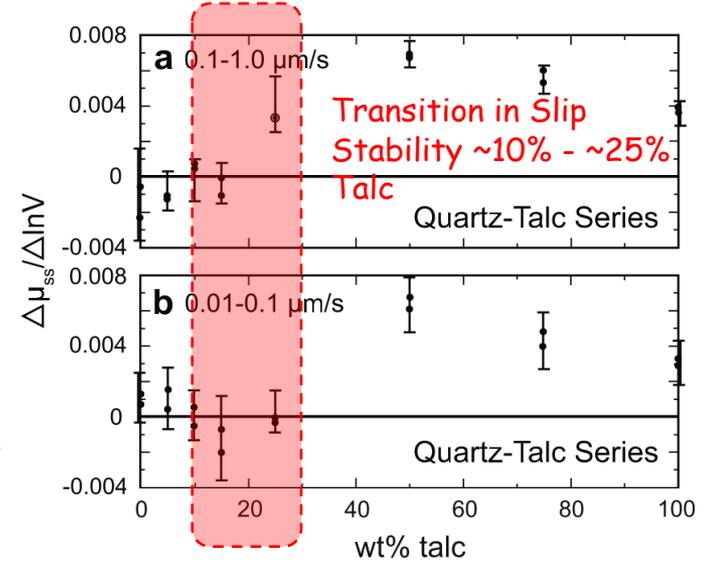
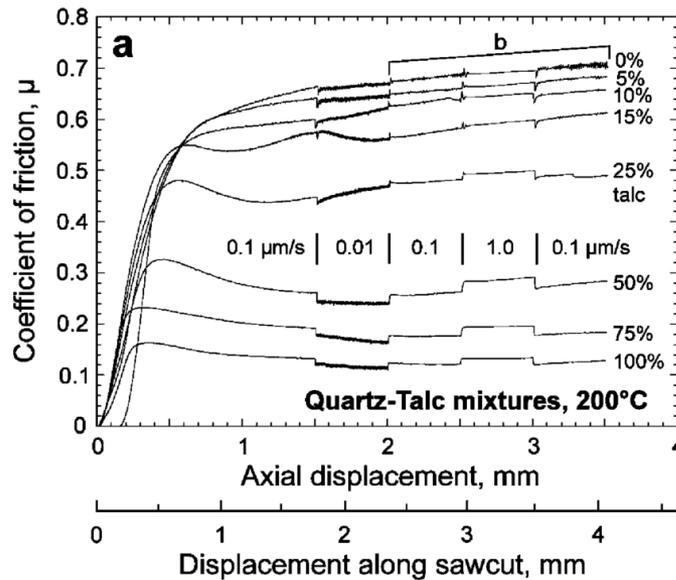
Steady-State Friction



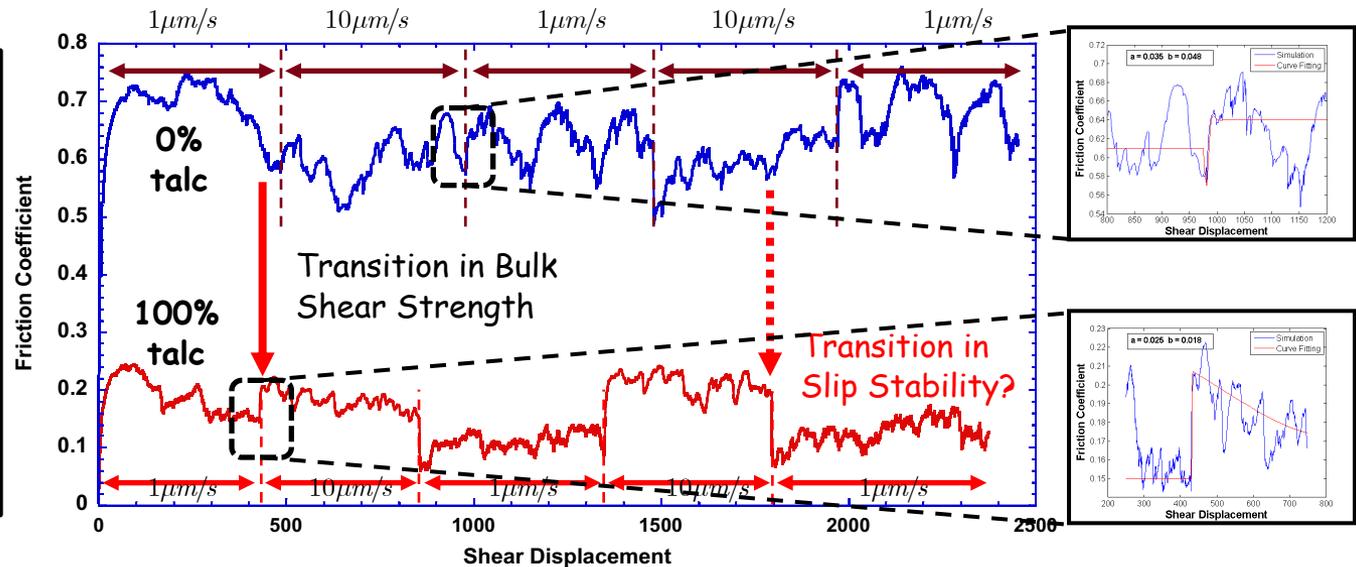
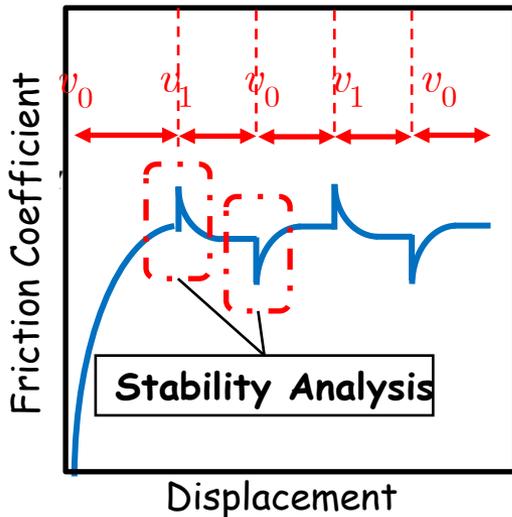
Mixture Controls of Frictional Instability

Observations

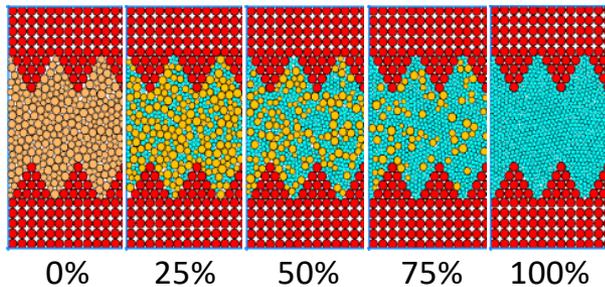
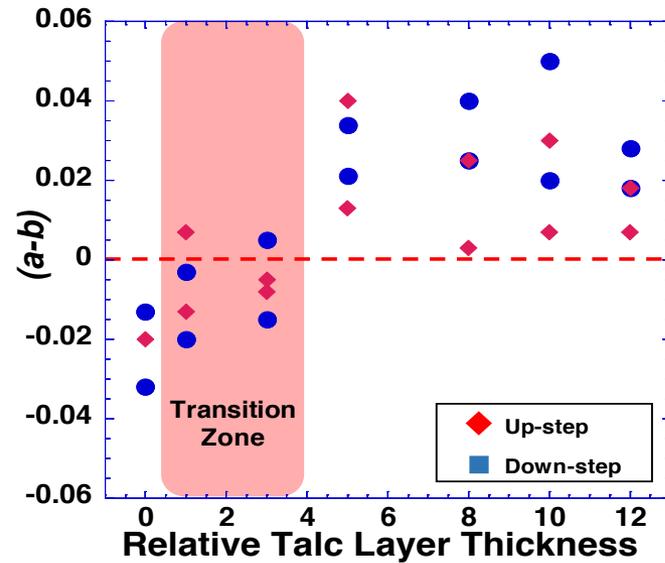
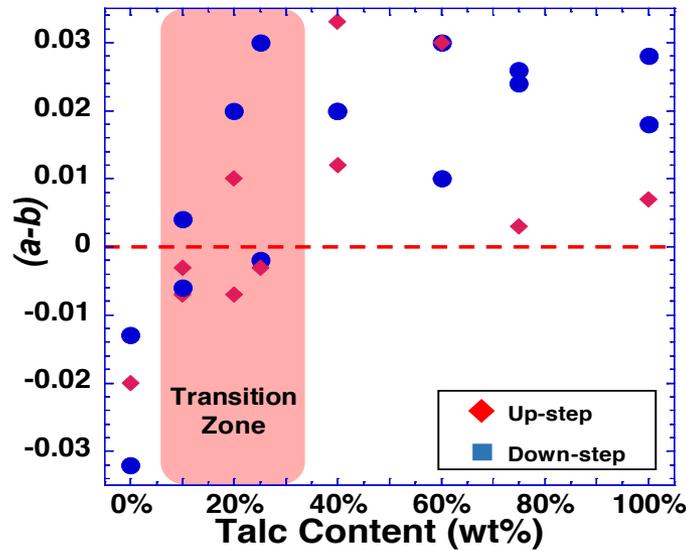
[Moore & Lockner 2011]



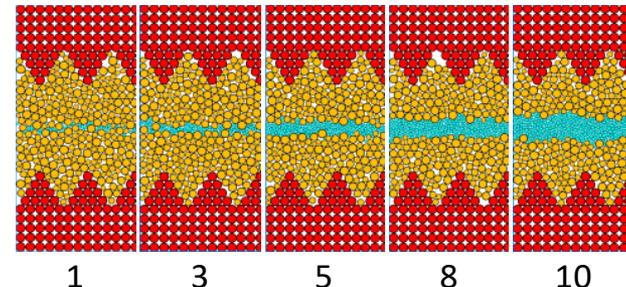
Analysis



Multi-Mineral Frictional Stability

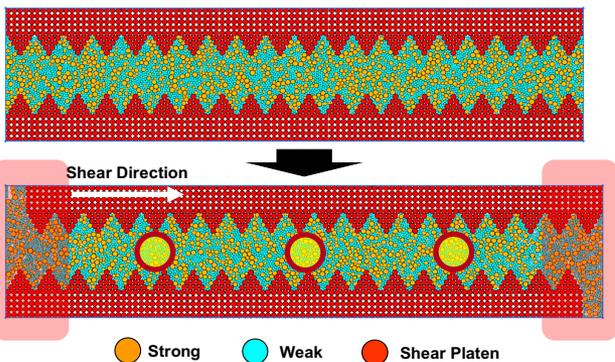


Transition zone appears at ~10% to ~25% talc content



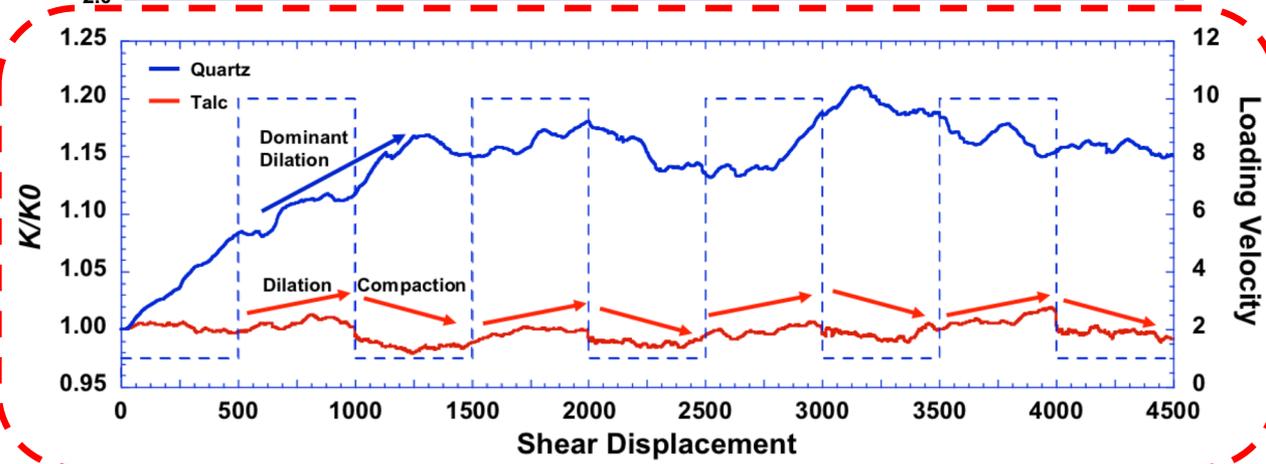
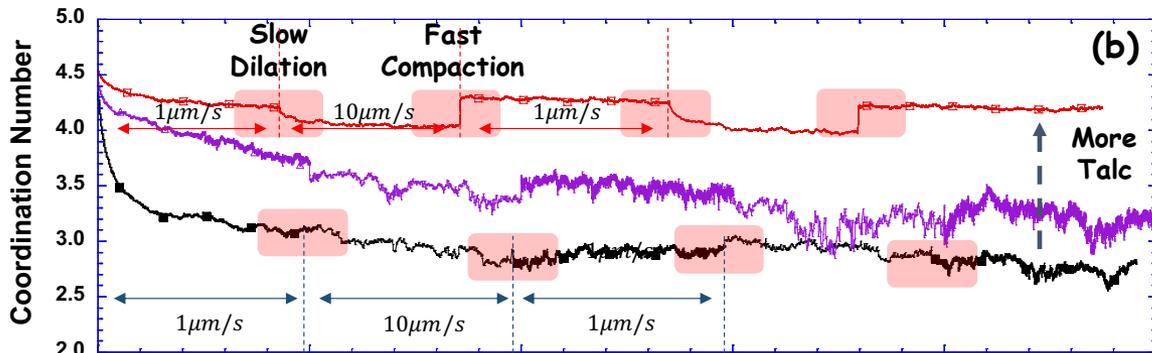
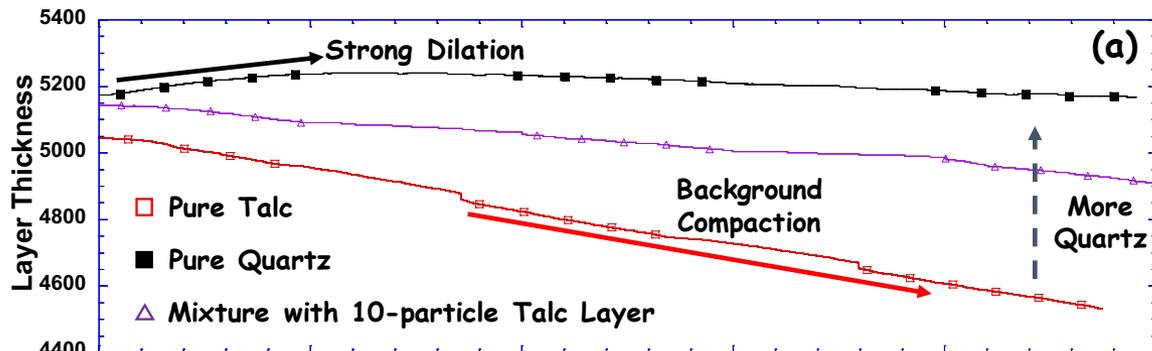
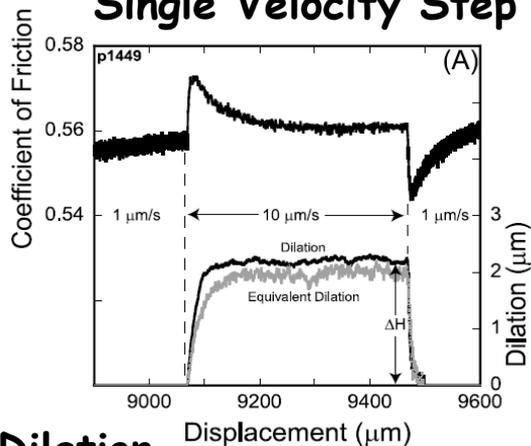
Transition zone appears at ~2% to ~3% talc content

Evolution of Layer thickness, Coord. Num, and Porosity



Background Compaction

Single Velocity Step



Dilatation

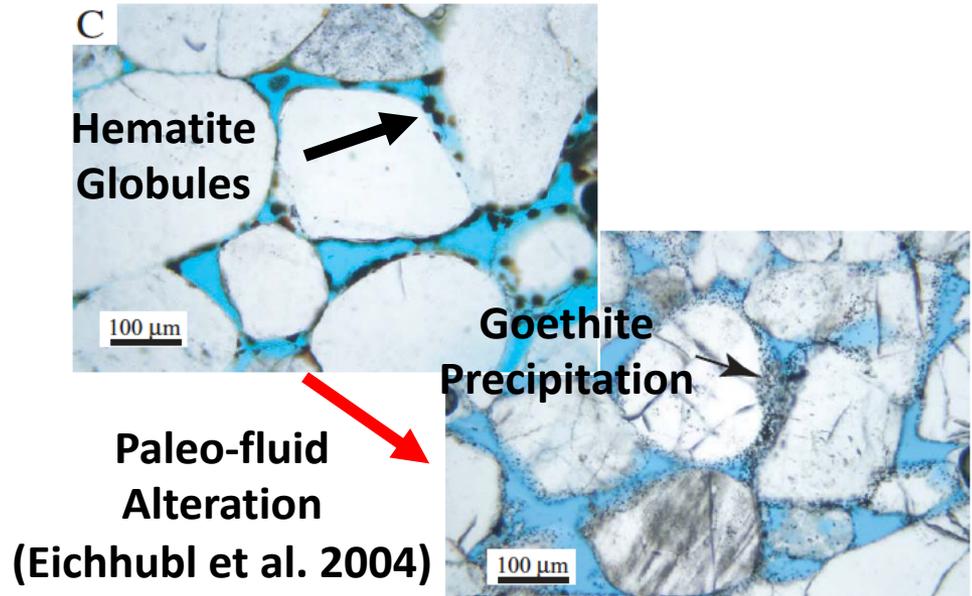
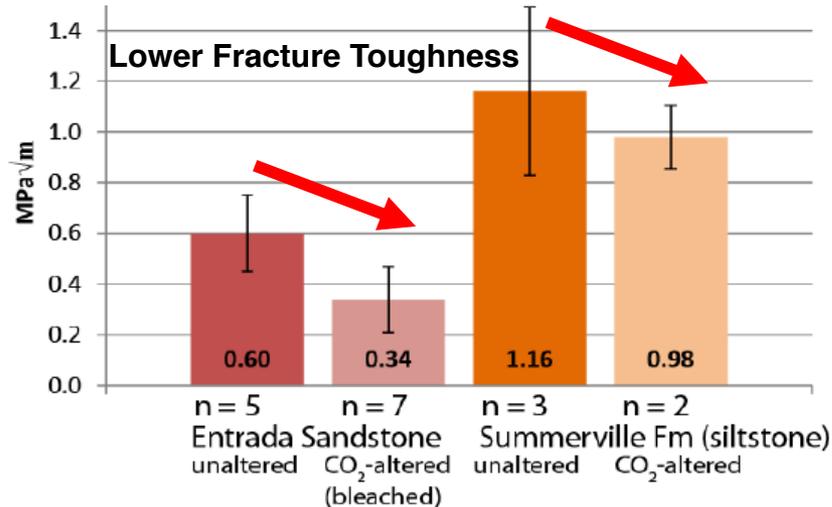
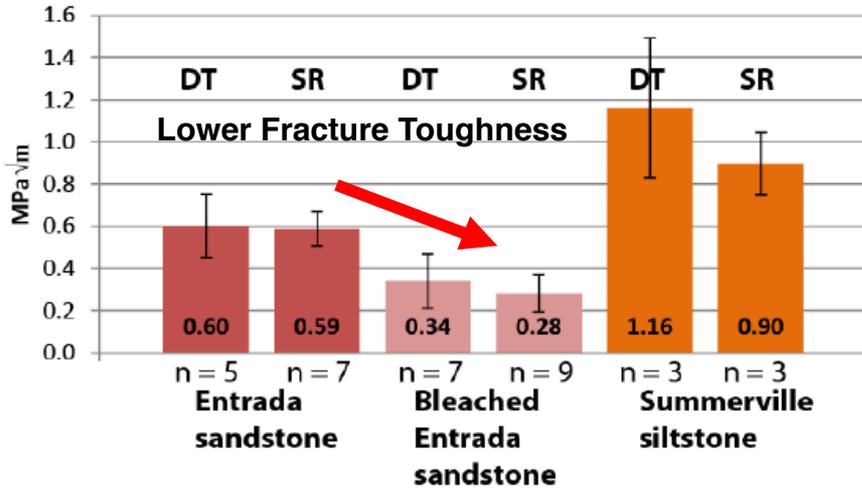
$$\frac{\Delta H}{H} \cong \Delta \phi = -\epsilon \ln\left(\frac{v}{v_0}\right) = -\epsilon \ln\left(\frac{v_0 \theta}{D_c}\right)$$

Permeability Evolution

$$\frac{k}{k_0} = \left(1 + \frac{\Delta b}{b_0}\right)^3 = \left(1 + \frac{\Delta H}{H}\right)^3 \cong (1 + \Delta \phi)^3$$

Introduction & Motivation

CO₂ bleached sand stone and silt stone showed lower fracture toughness
(Major et al. 2014)



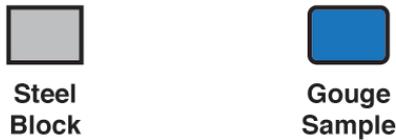
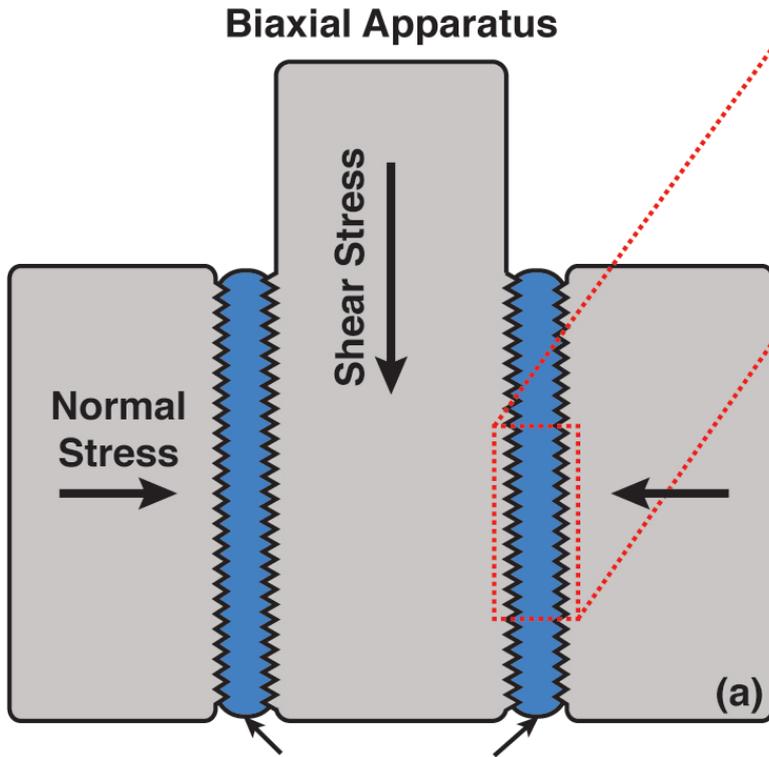
Mineralogic Difference

Unaltered Entrada Sand Stone: quartz rich, minor feldspar and calcite, with hematite coating.

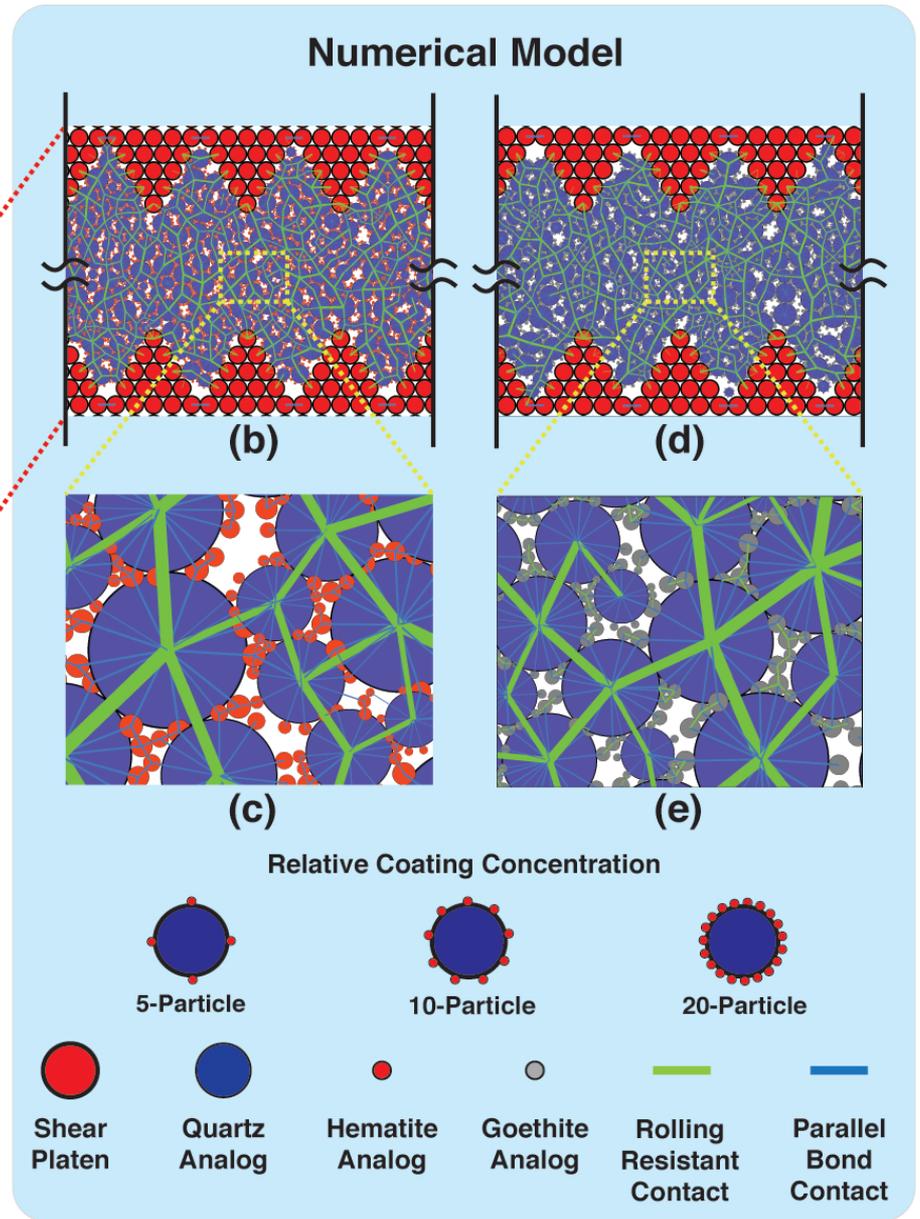
Altered Entrada Sand Stone: hematite coating is dissolved, replaced by goethite, no significant change in quartz, feldspar, and calcite.

(Major et al. 2014)

DEM Model Setup

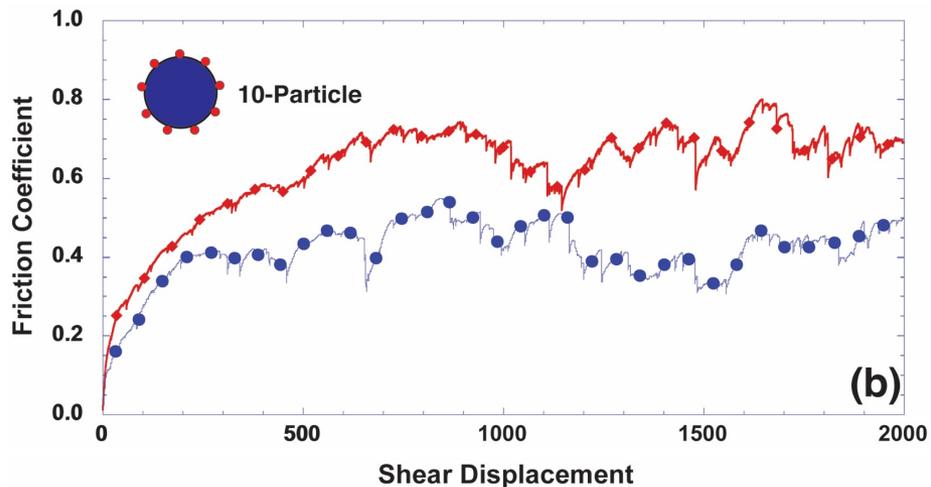
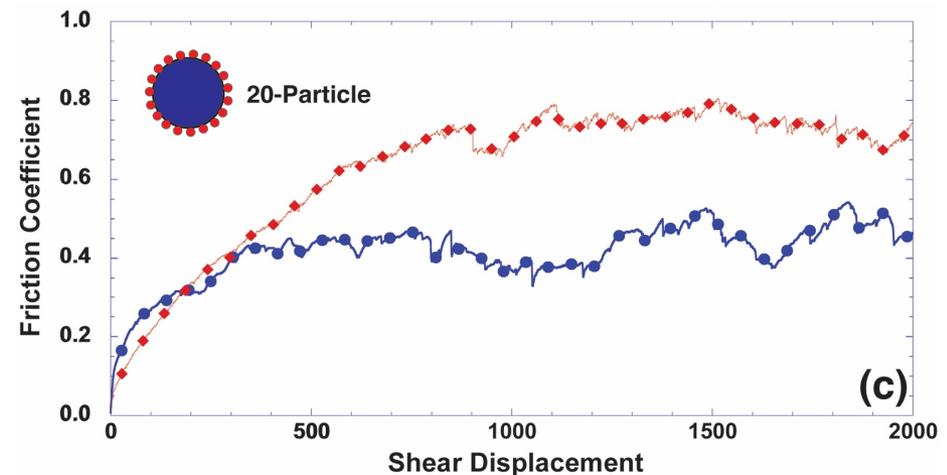
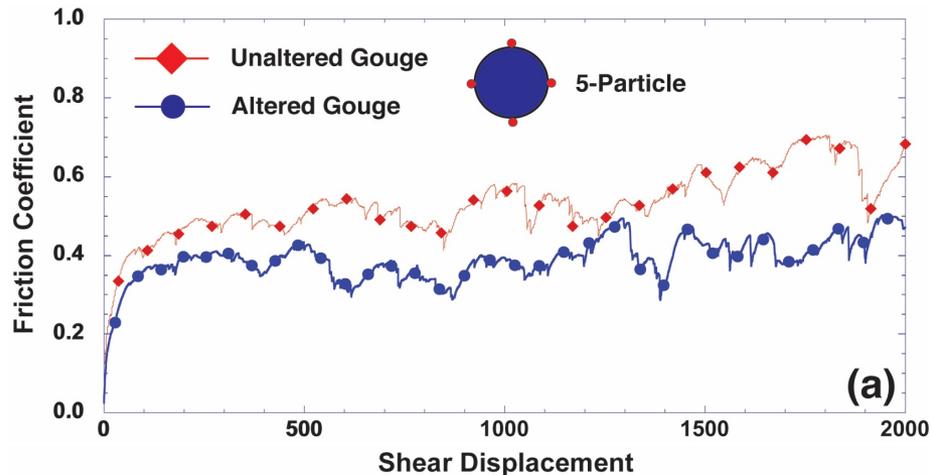


(Marone, 1999)



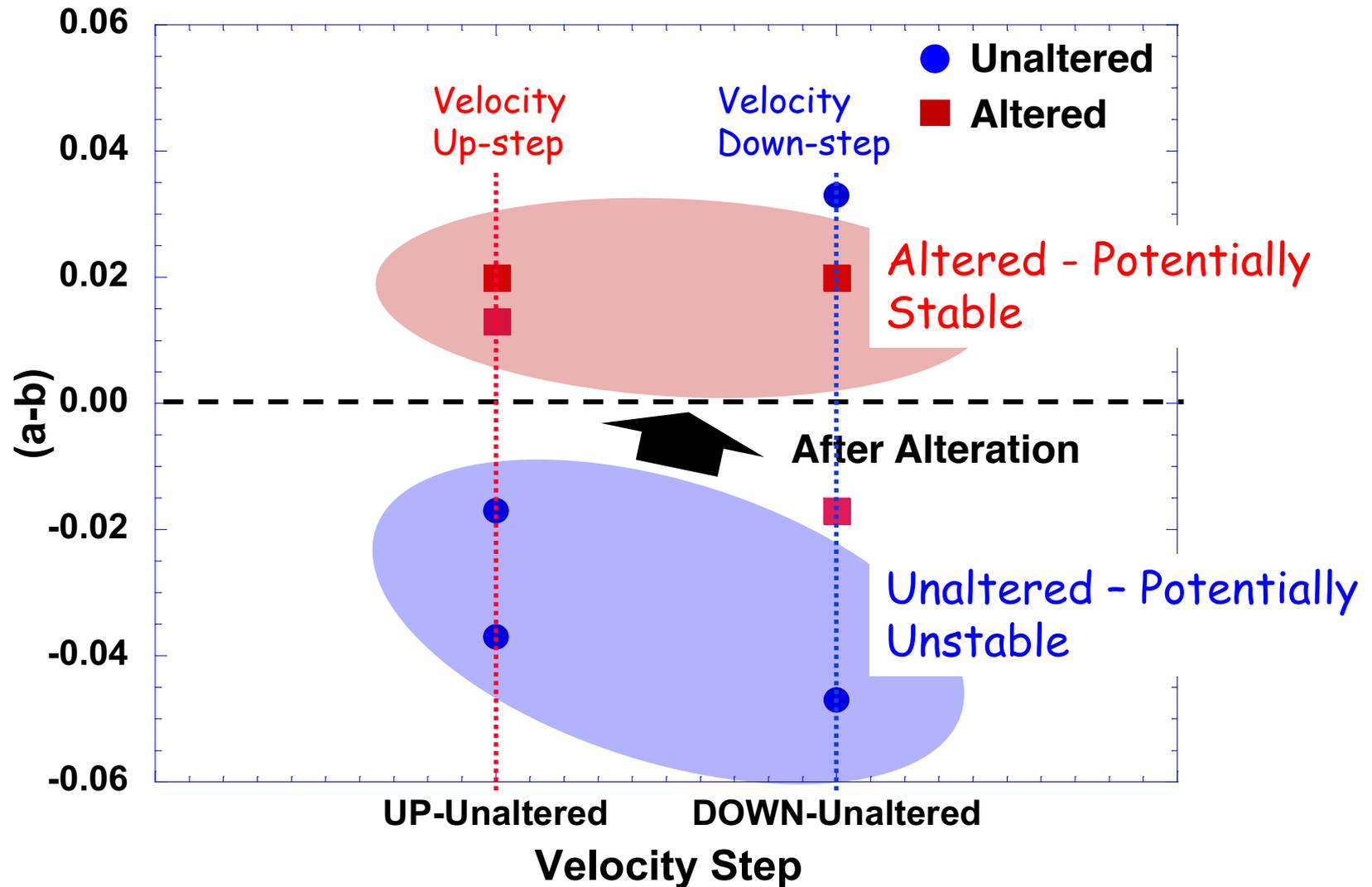
Shear Strength -- Unaltered vs Altered

Evolution of friction at 10 MPa normal stress [other normal stresses (5, 15 MPa) show similar trend].

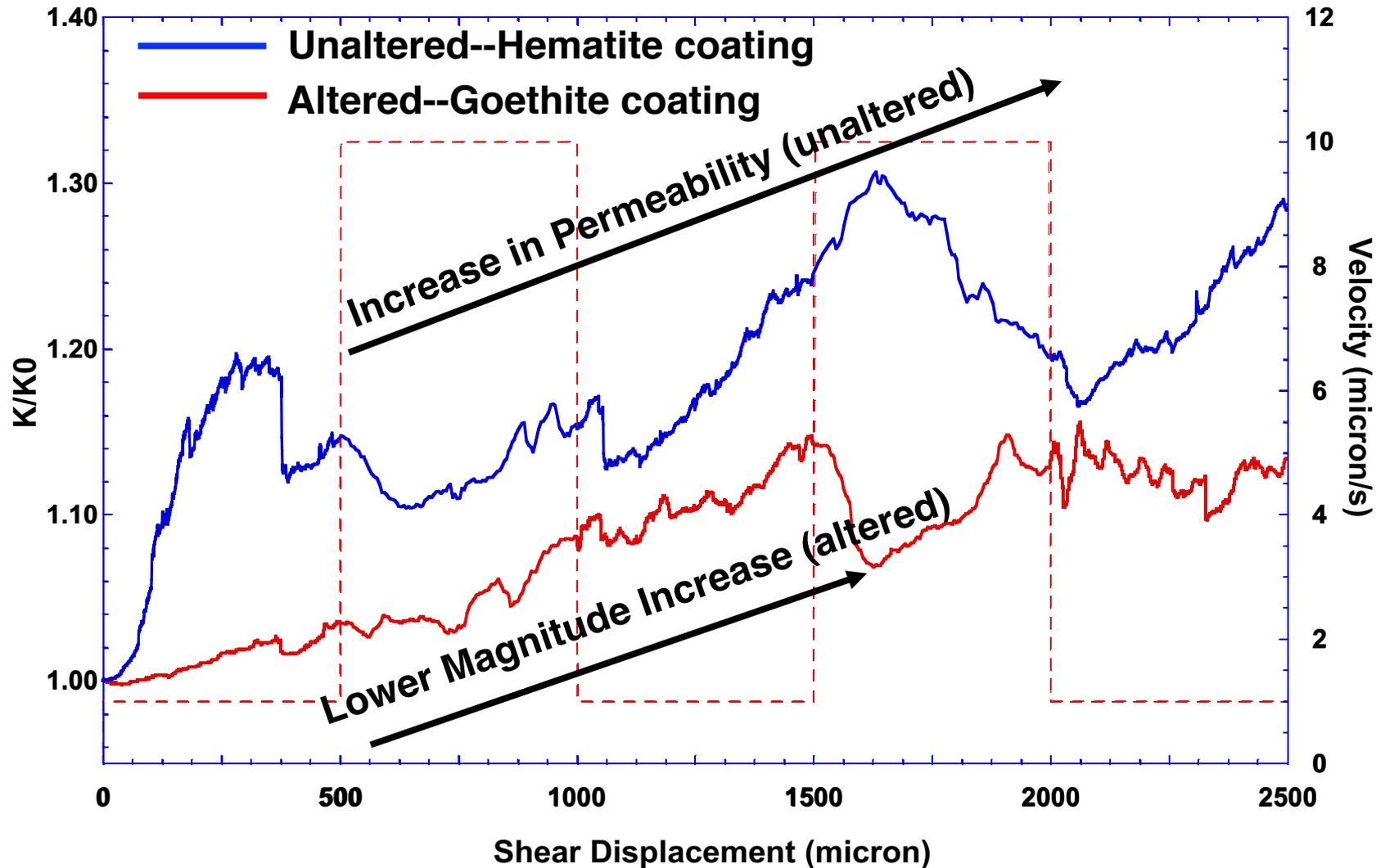


- CO₂ altered synthetic gouge shows **LOWER** frictional strength (shear strength) than unaltered synthetic gouge.
- Unaltered gouge shows **HIGHER** shear strength with more coating particles.

Slip-Stability - Unaltered versus Altered

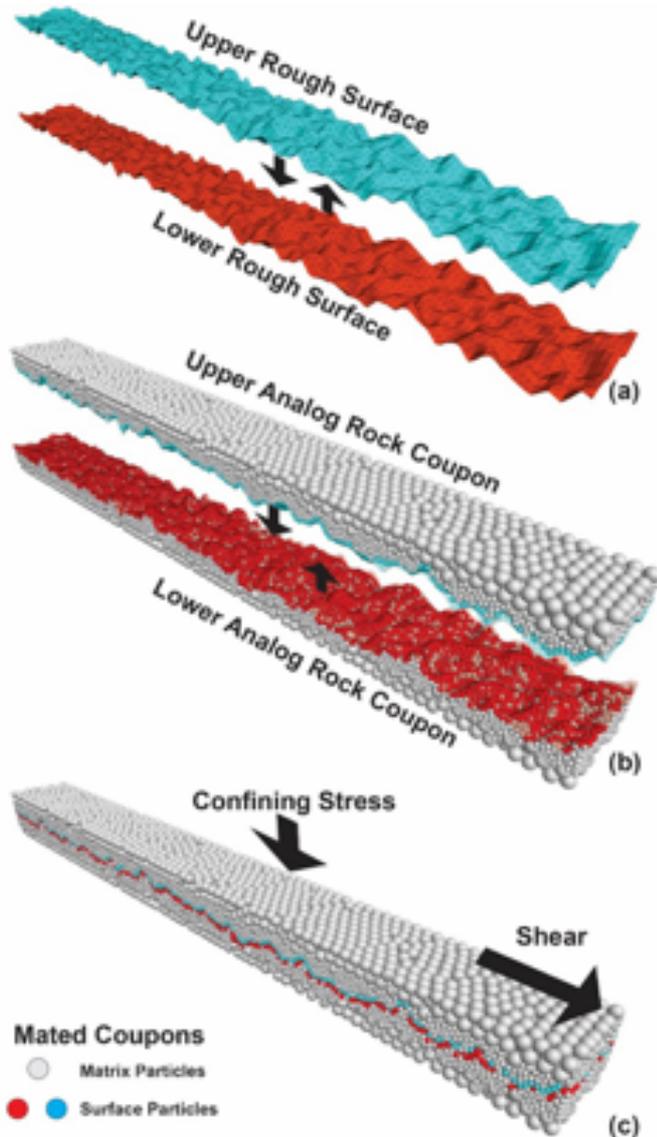


Permeability Evolution

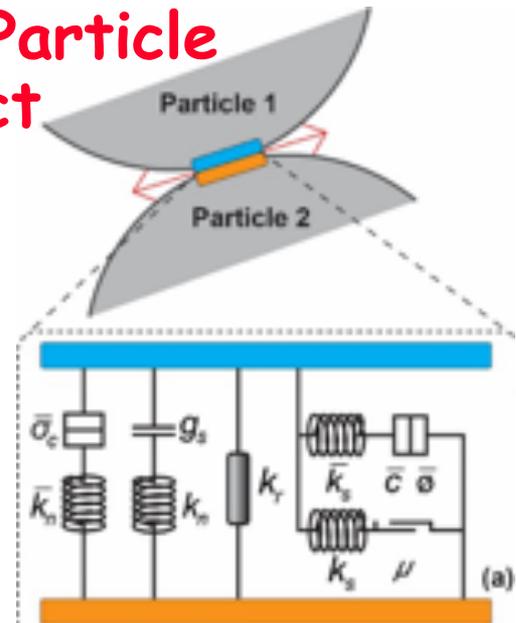


Digital Fractures

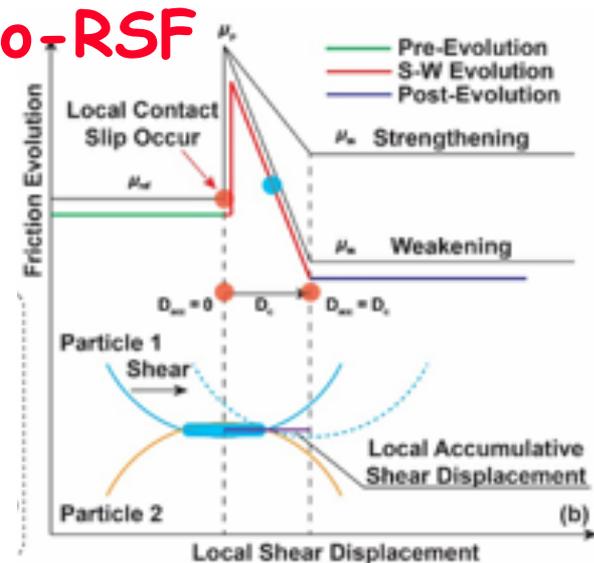
Mated Fractures



Particle-Particle Contact

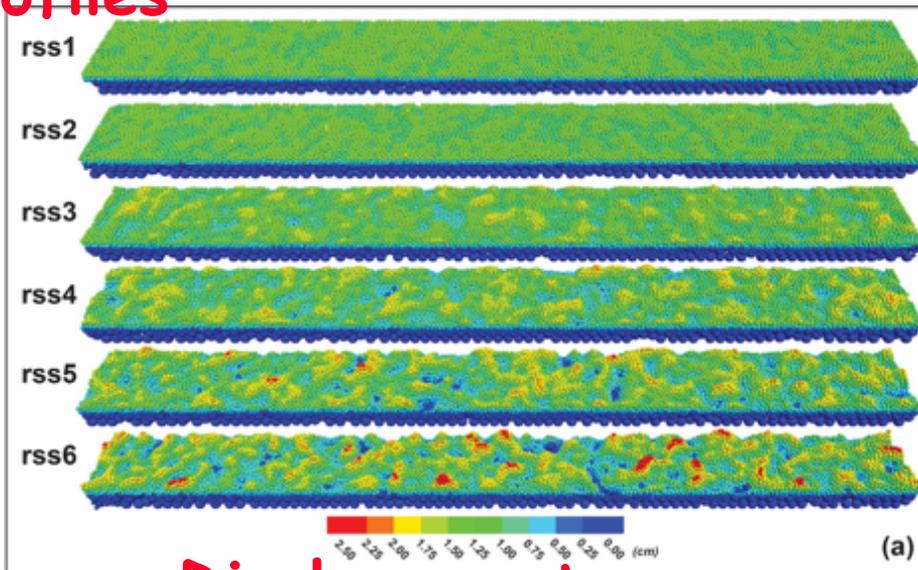


Pseudo-RSF

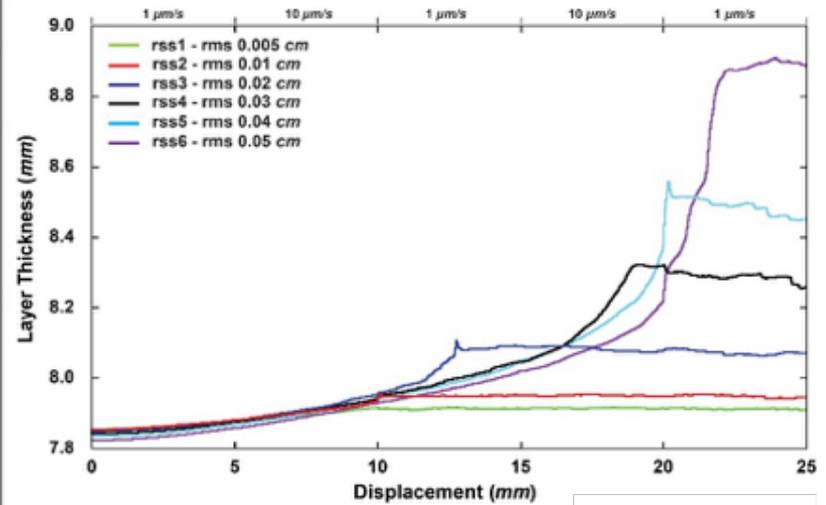


DEM Modeling of Rough Fractures

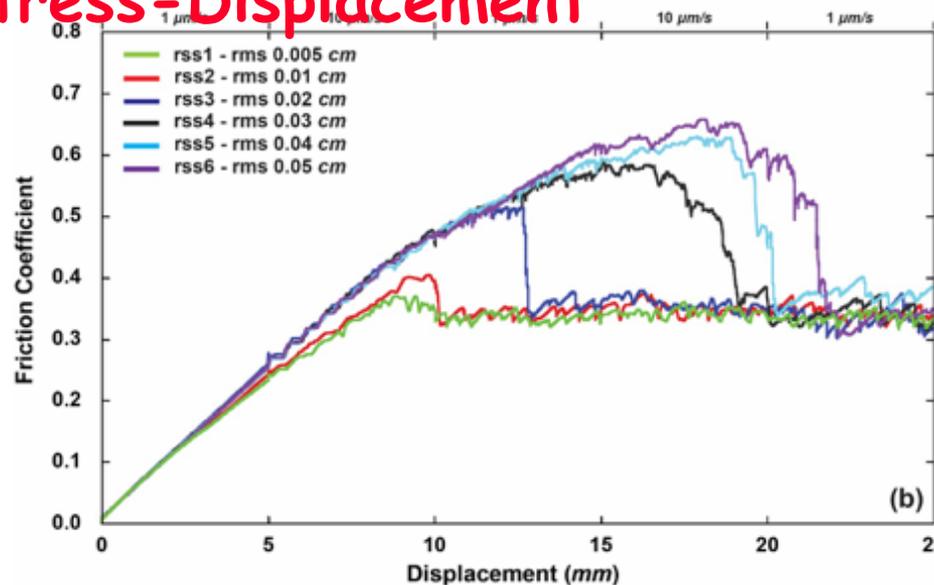
Profiles



Dilation

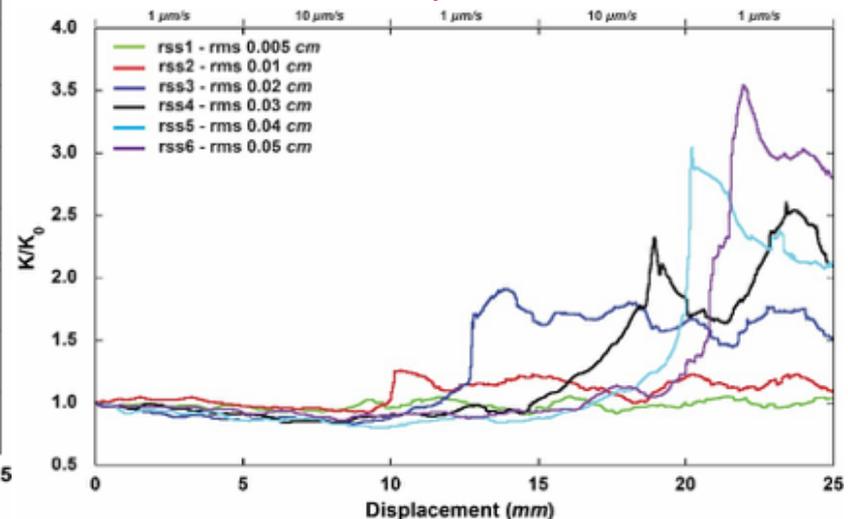


Stress-Displacement



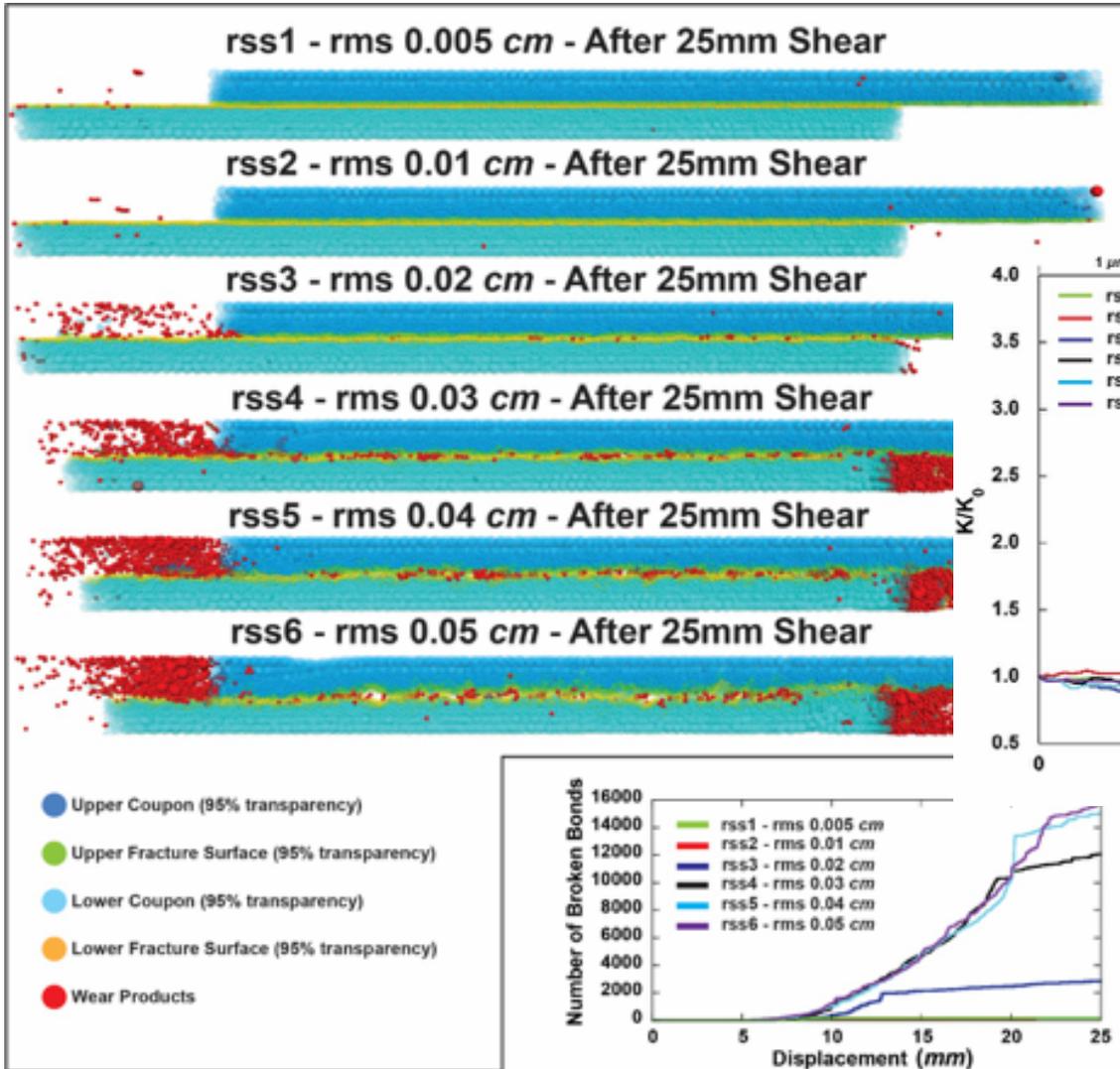
Permeability

$$\frac{k}{k_0} \cong (1 + \Delta\phi)^3$$

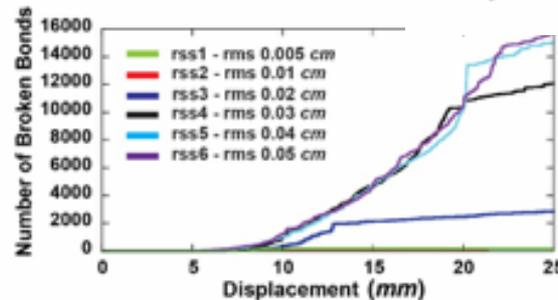
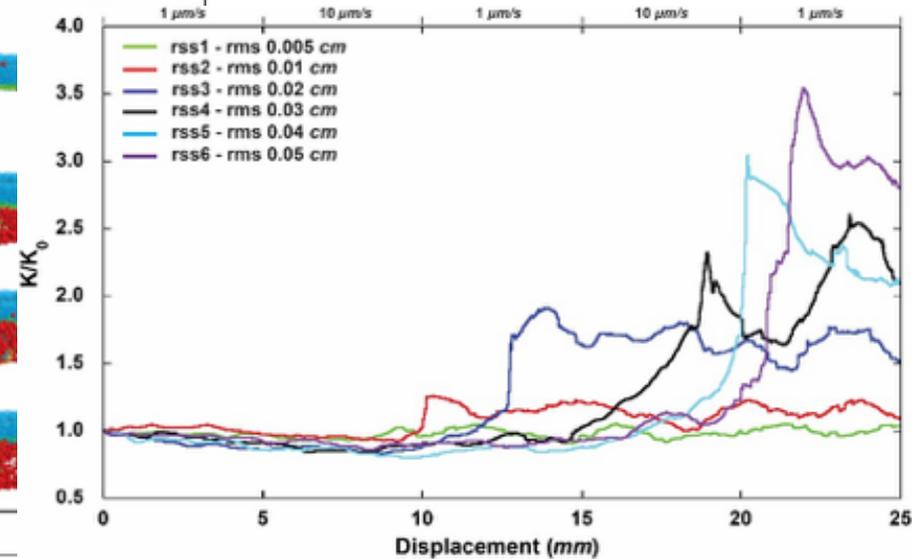


Permeability Evolution - Role of Wear Products

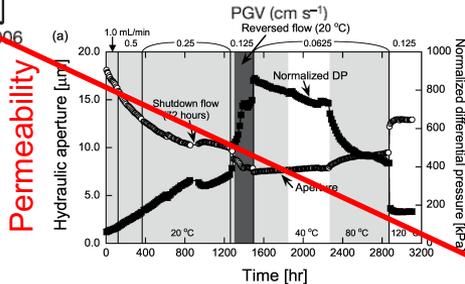
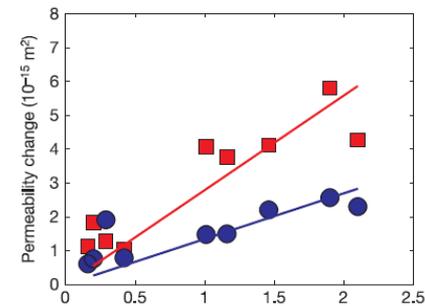
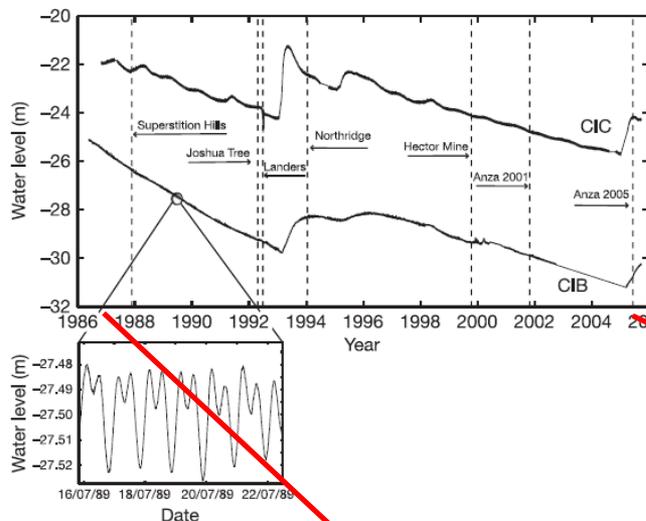
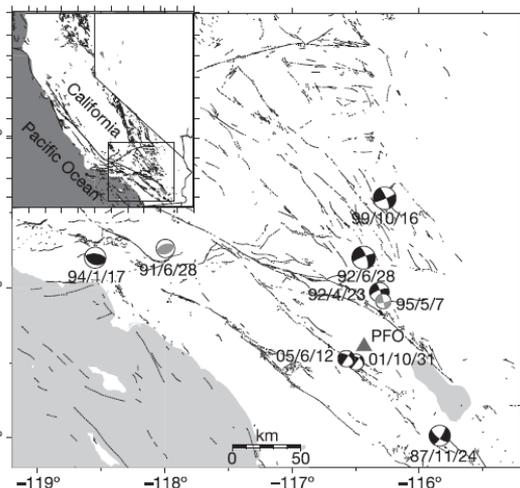
Profiles - Variable RMS and Wear Products



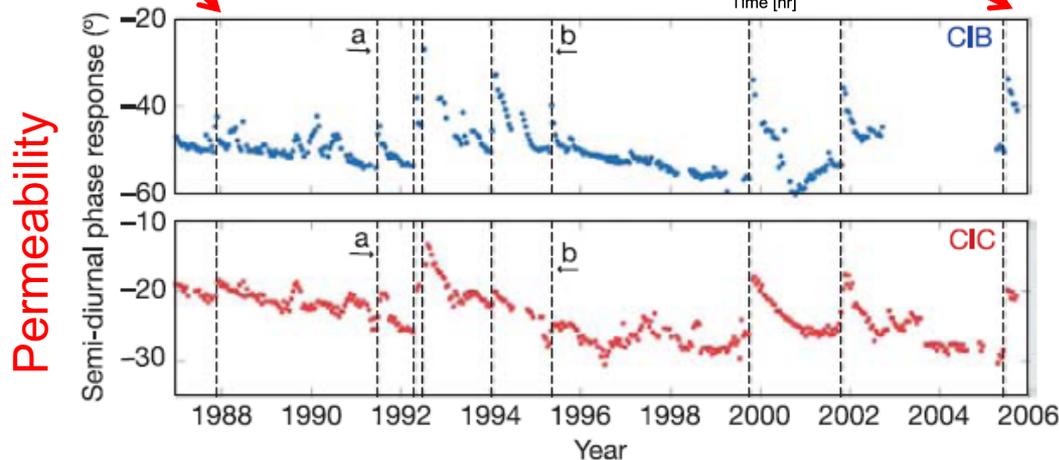
Permeability Evolution



Permeability Changes due to Dynamic Stressing



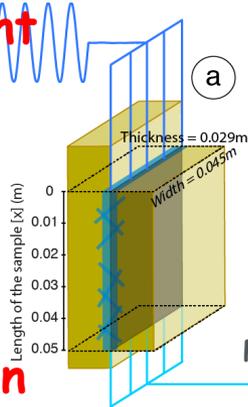
- Remote** earthquakes trigger dynamic changes in permeability
- Unusual record transits ~8y
- Sharp rise in permeability followed by slow "healing" to background
- Scales of observations:
 - Field scale
 - Laboratory scale
- Mechanistic understanding and control?



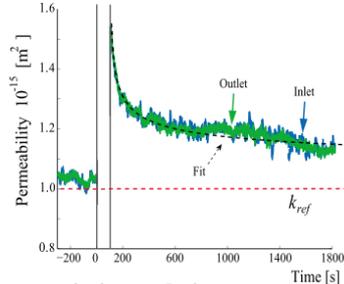
[Elkhoury et al., Nature, 2006]

Dynamic Stressing - Mechanisms

Experiment

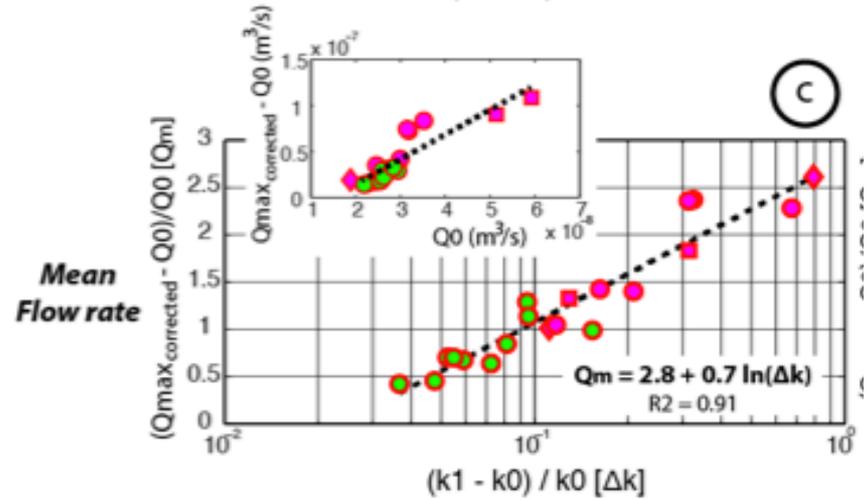


Observation



Permeability Enhancement via Dynamic Stressing

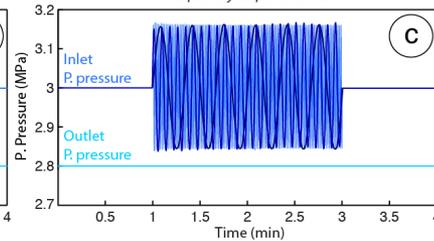
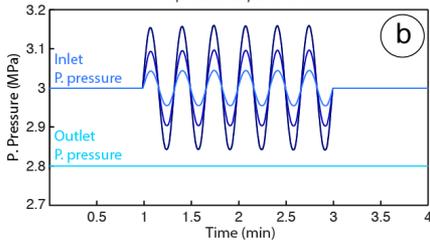
Correlations with Flow Rate



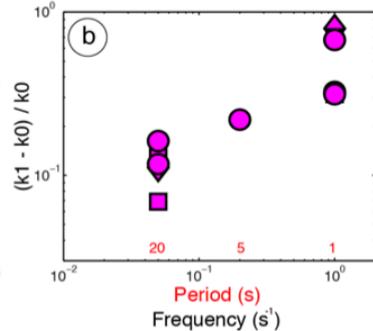
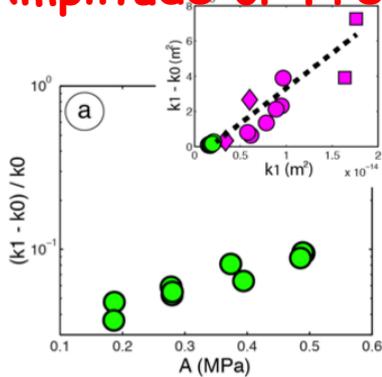
Excitation

Amplitude?
Amplitude experiments

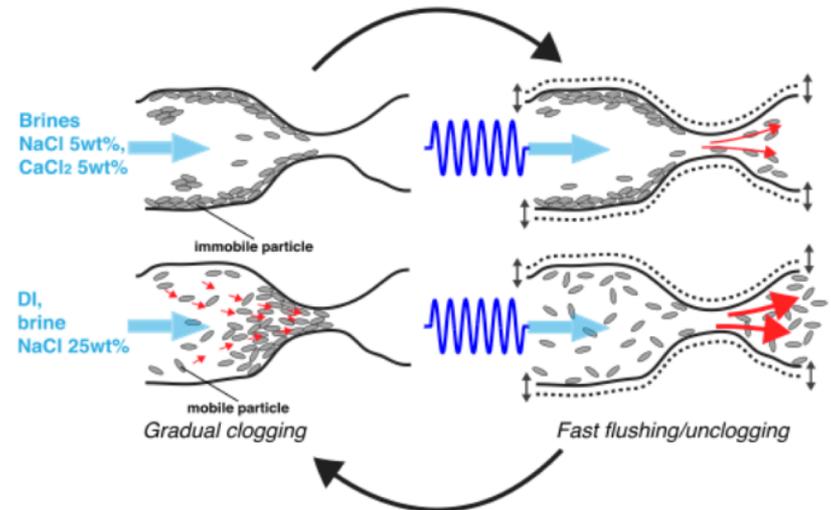
or
Frequency?
Frequency experiments



Amplitude or Frequency Dependency



Suggested Mechanism



[Candela et al., 2014a,b]

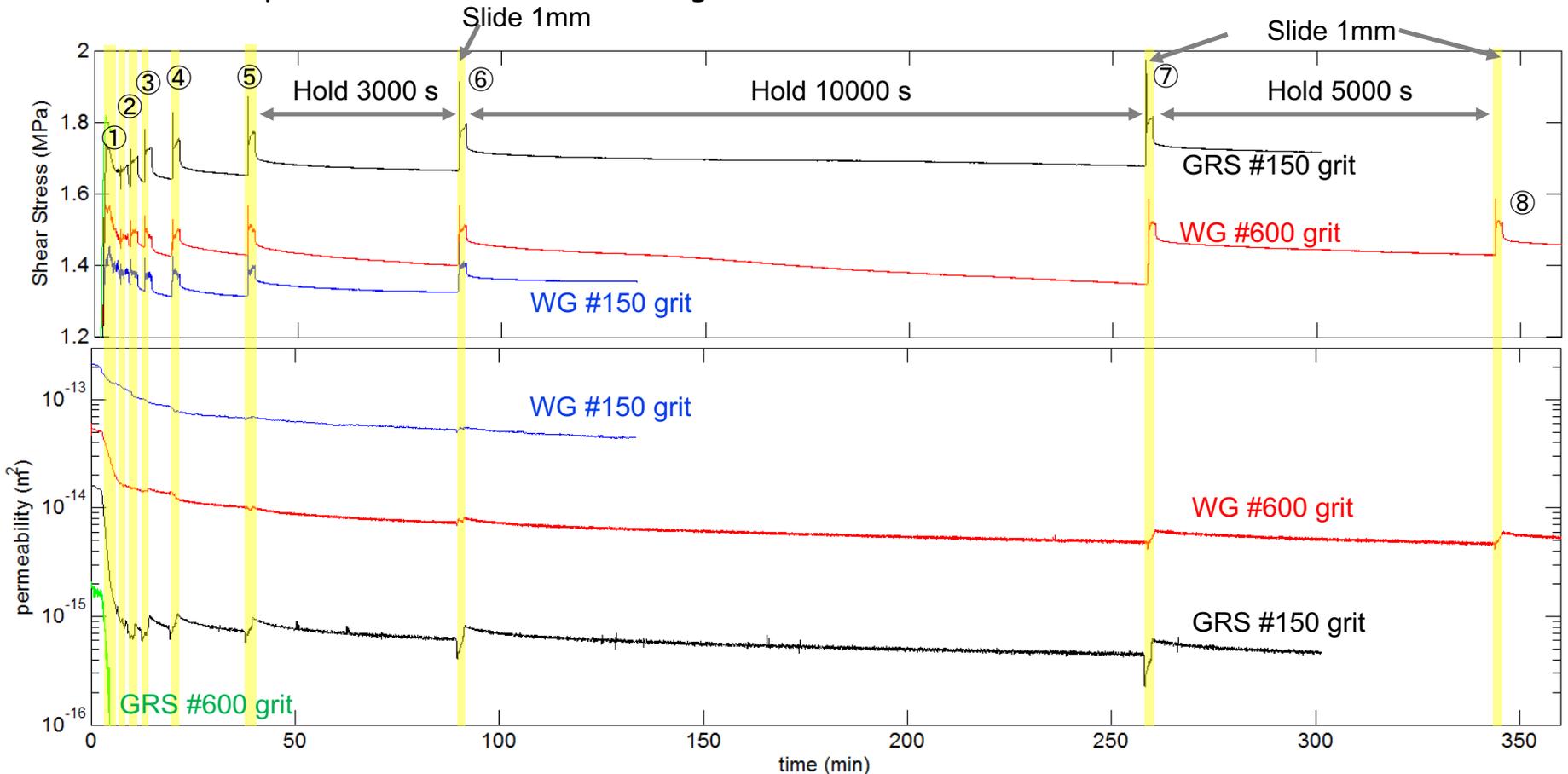
Healing - Necessary Component of the Seismic Cycle

Shear Stress and Permeability Evolution

- Increasing shear stress peak is observed with increasing hold time (Frictional Healing)
- Permeability declines overall with temporal response to shear events
- Permeability decline is fast at initial stage then become slower

Experimental Notes

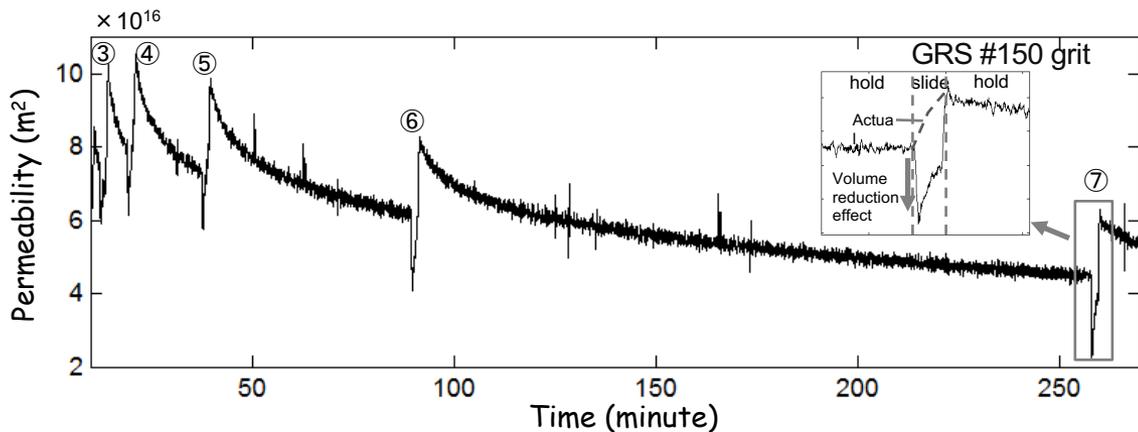
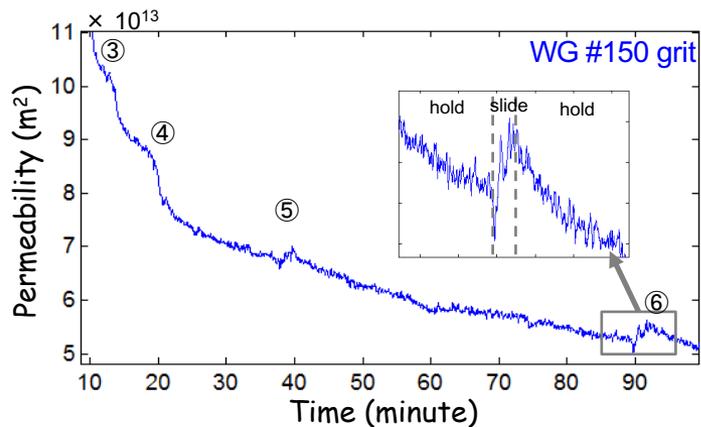
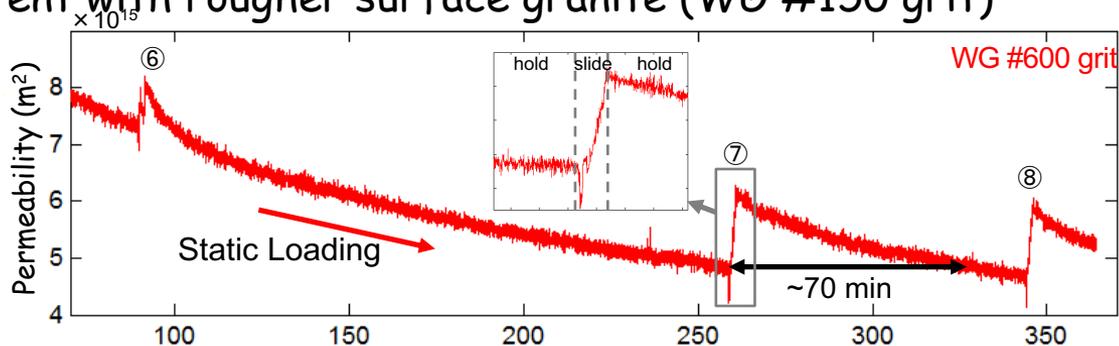
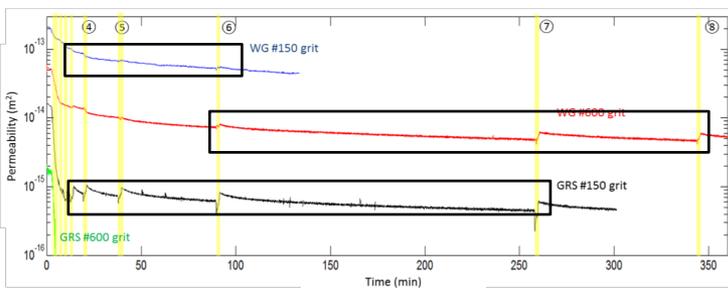
- Permeability of Green River shale #600 grit became unresolvable after initial shear
- Westerly granite #150 grit stopped at ~150 min due to limited pump capacity
- 8th shear applied to Westerly granite #600 grit after 5000 seconds



Shear Permeability Enhancement

Shear Induced Permeability Enhancement

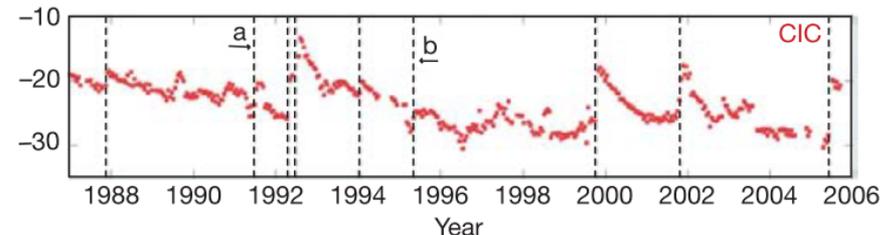
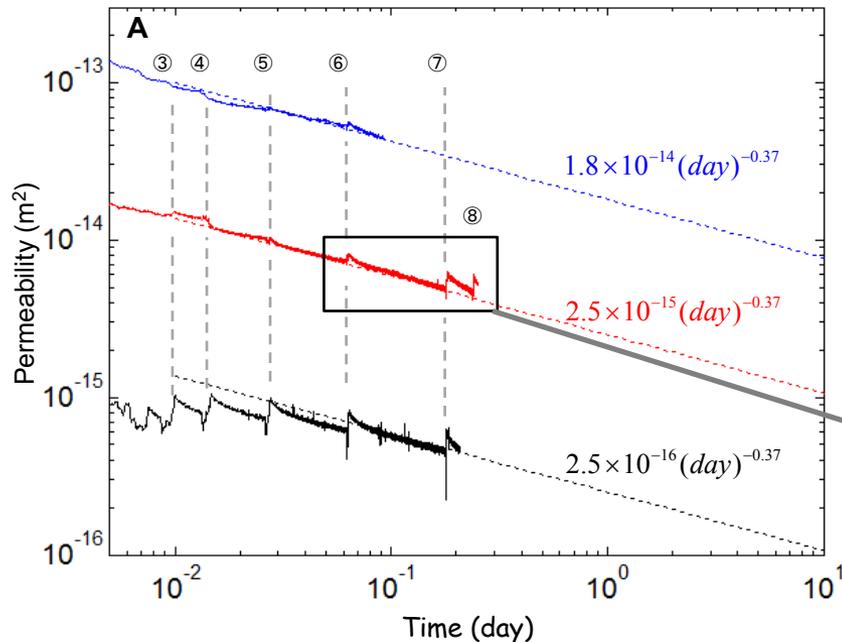
- Later stage shear slip + Incremented duration of prior slip → Significant permeability enhancement
- Permeability continuously decreases during hold (Pressure solution?)
- Prior slip permeability recovery took 70 minute after slip ⑦, WG #600 grit case
- Permeability increase appears to be linear to slip distance
- The enhancement is least apparent with rougher surface granite (WG #150 grit)



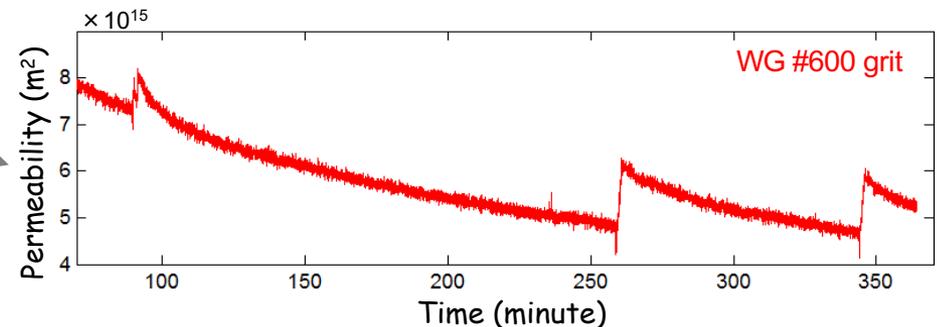
Permeability Healing (Sealing) Law

Pressure solution

- Permeability reduction due to pressure solution in all cases seems to follow power law decay $k = k_0 t^{-p}$ with power $p = -0.37$
- The enhancement can be significant after extremely long (natural scale) holds
- Can this be applied to natural hydraulic systems?



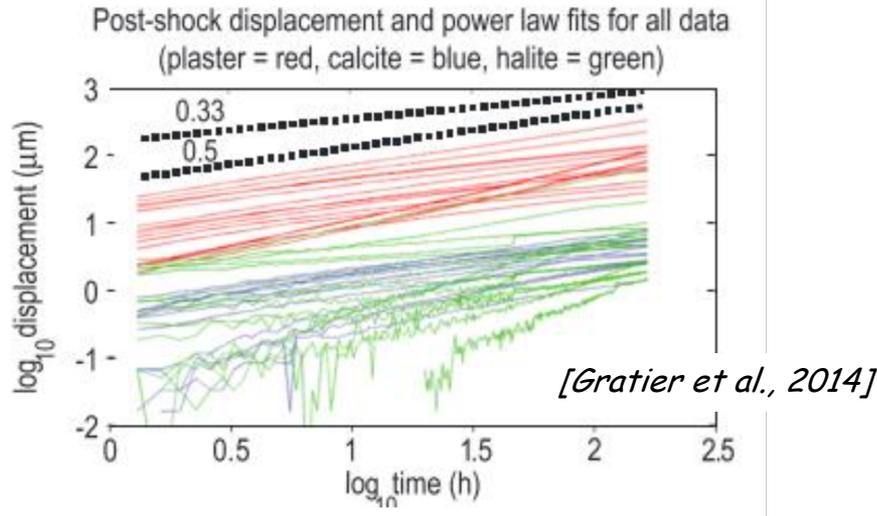
Permeability change and earthquake catalog ($M_L > 3$) in southern California [Elkhoury et. al., 2006]



Permeability Decay - Role of Pressure Solution

Power-law dependence

Rigid indenter, Pressure solution

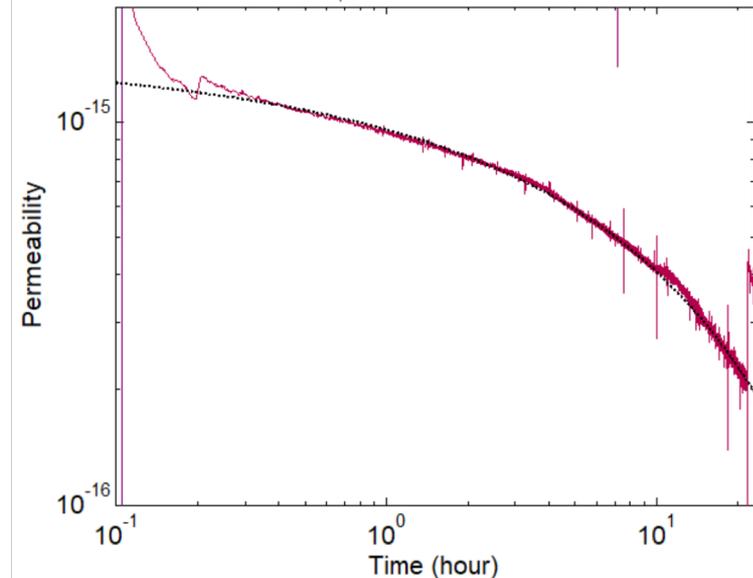
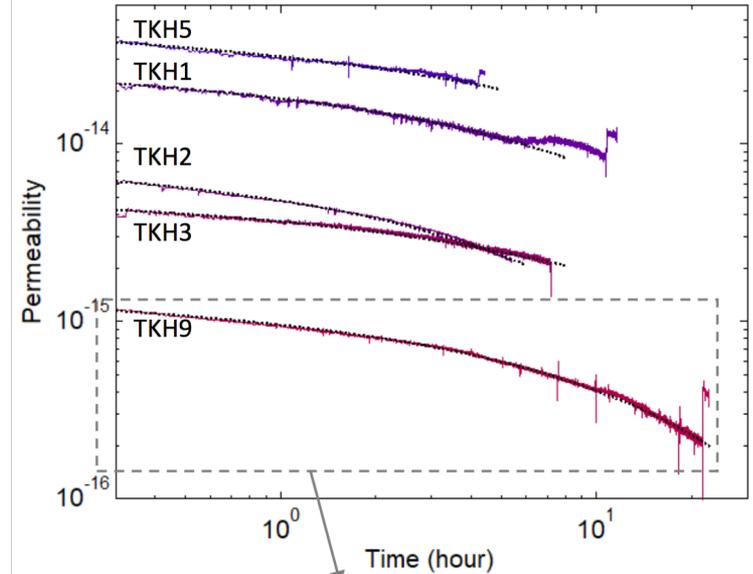


Indentation rate:

$$\Delta b = \alpha t^\beta$$

Permeability change:

$$k = k_0 \left[1 - \frac{\Delta b}{b_0}\right]^3 \rightarrow k = k_0 \left[1 - \frac{\alpha}{b_0} t^\beta\right]^3$$



Shear Permeability Enhancement

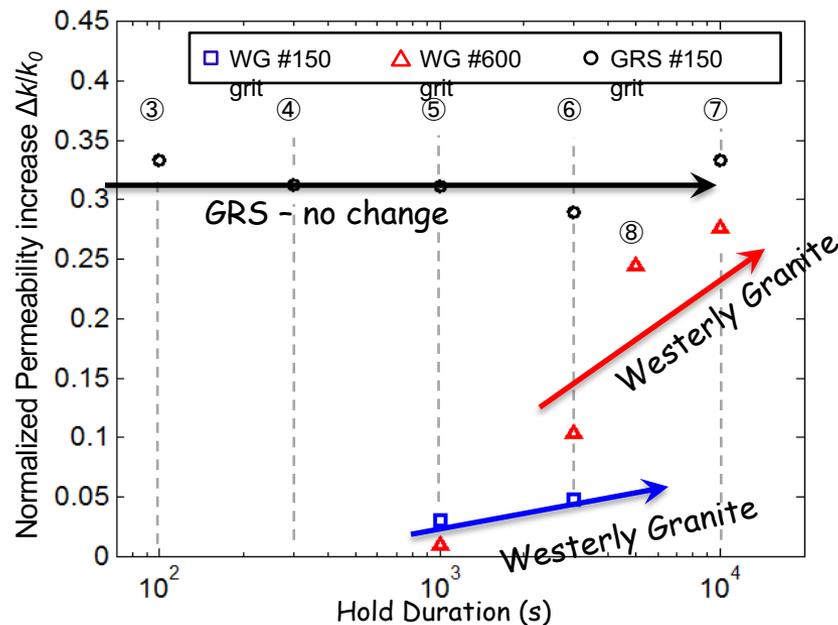
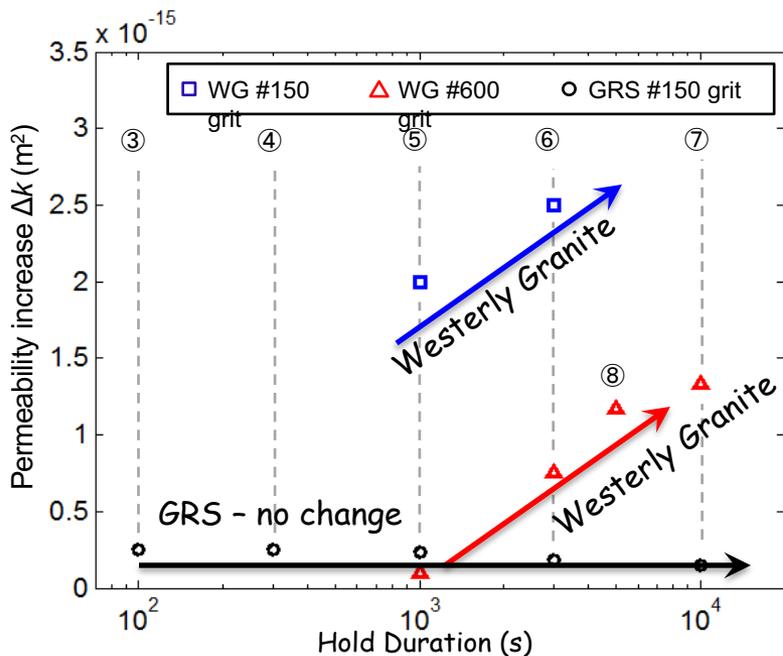
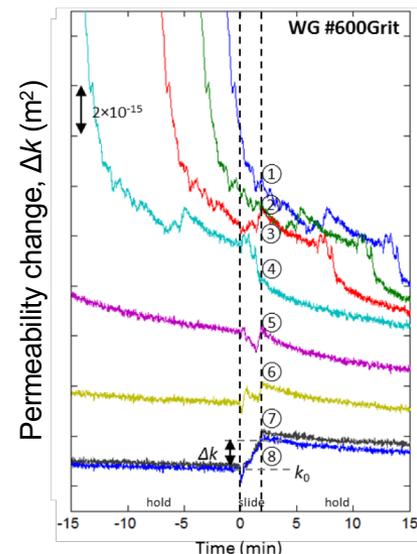
Magnitude of Permeability Enhancement

Absolute perm increase: rougher granite > smoother granite > shale

Normalized perm increase: shale > smoother granite > rougher granite

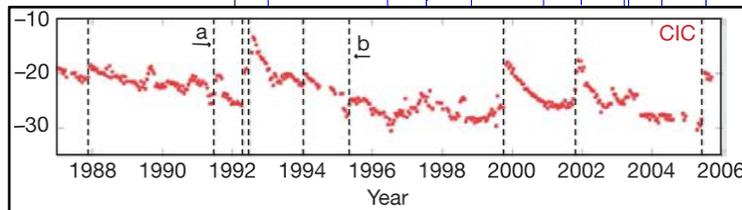
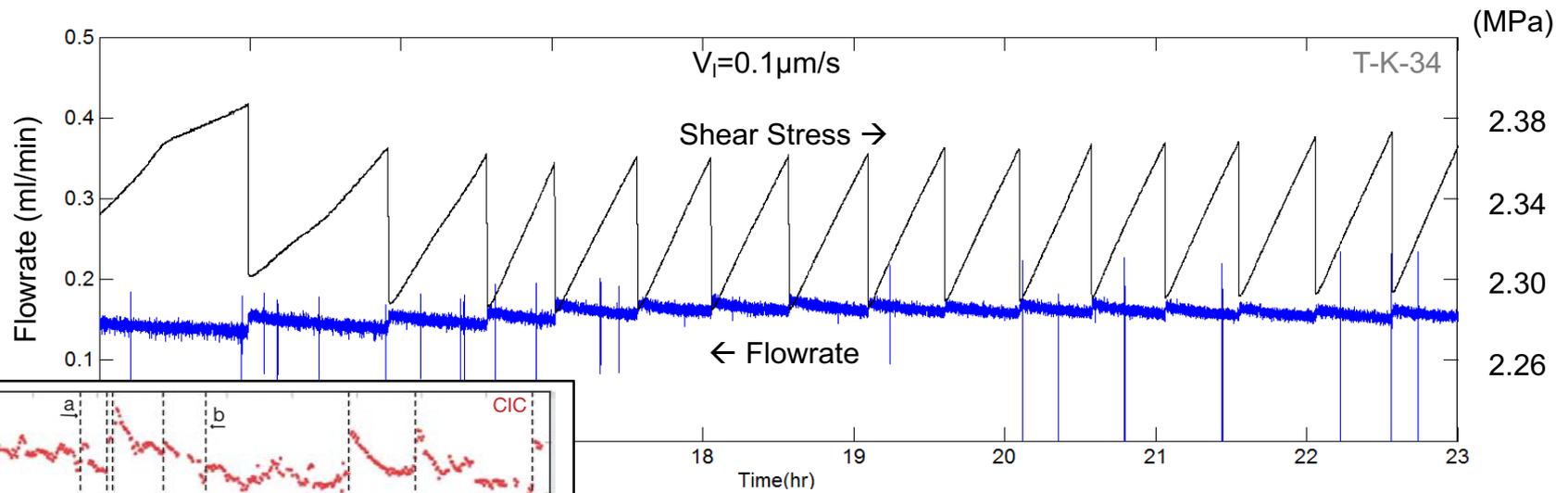
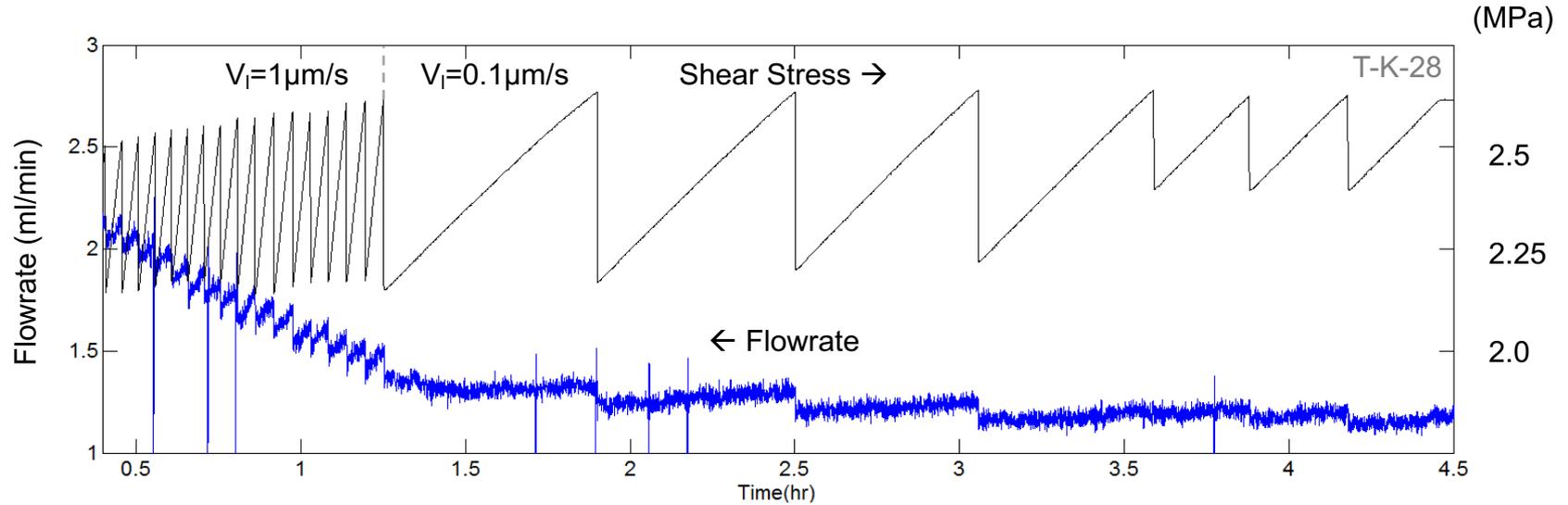
Shear permeability increase with duration of prior hold time for Westerly granites

Shear permeability slightly decreases with prior hold time for Green River shale



Stick-Slip Response

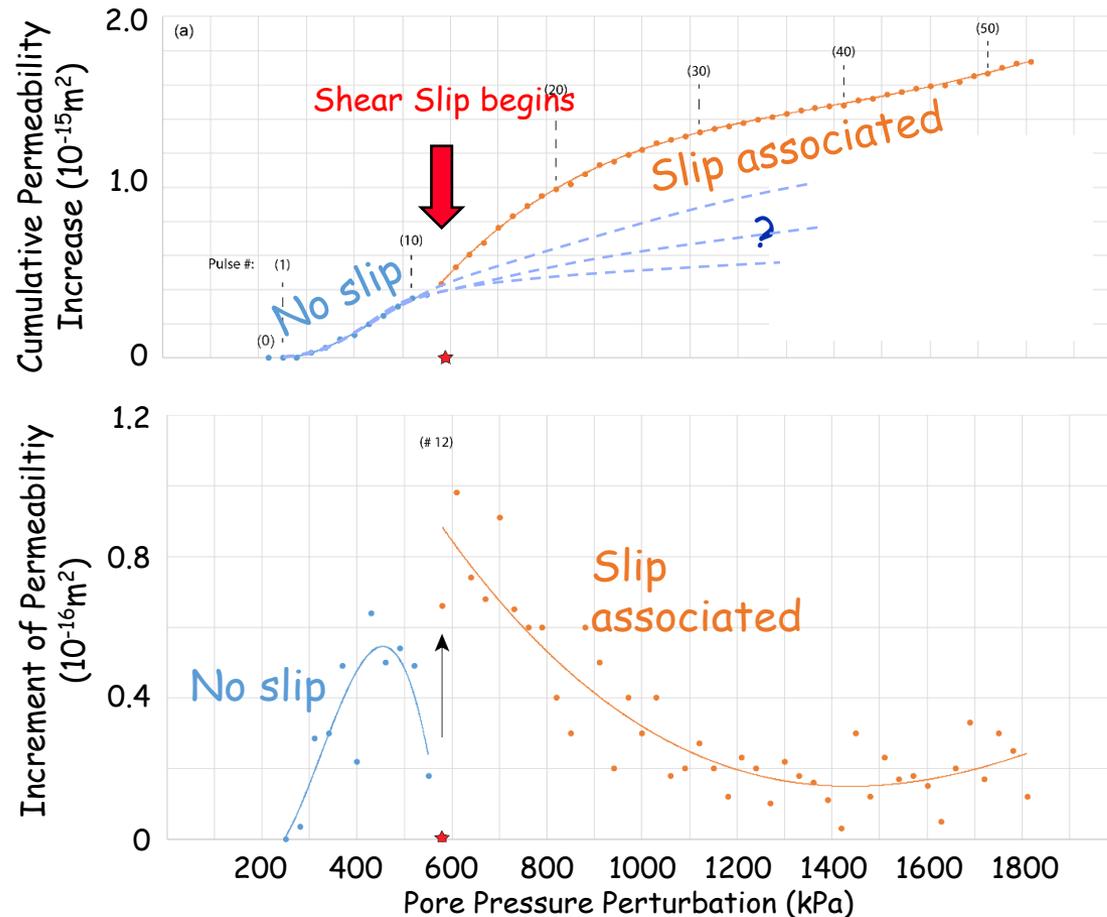
Response to Laboratory Earthquakes (Stick Slip)



Pore Pressure Perturbation

Effect of induced shear slip

- Slope of permeability increment curve changes at initiation of shear slip
- Permeability increment suddenly increases when shear slip initiates (stress threshold)



Seismicity-Permeability Coupling in the Breaching and Sealing of Reservoirs and Caprocks

Derek Elsworth (Penn State), Yi Fang (PSU), Chaoyi Wang (PSU), Takuya Ishibashi (AIST/PSU), Yves Guglielmi (LBNL/Aix-Marseille), Kyunjae Im (PSU), Yunzhong Jia (PSU/NTU), Brandon Schwartz (PSU), Ziyang Li (PSU), Elif Yildirim (PSU), Andre Niemeijer (UU), Thibault Candela (TNO), Ben Madara (PSU), Mengke An (Tongji), Fengshou Zhang (Tongji), Jacques Riviere (Grenoble/PSU), Parisa Shokouhi (PSU), Chris Marone (PSU)

Some Key Issues in Energy Supply

Needs

Constraints and Solutions

CO₂ Sequestration - Linking Induced Seismicity to Permeability Evolution

Controls on seismicity - the aseismic-seismic transition

Controls on maximum magnitude event

RSF - for permeability evolution

Controls on stability and permeability

Mineralogical & textural

Structural

Healing and sealing and the seismic cycle

Energy From Hot Rocks - EGS and SGRs

Anomalous seismicity - Newberry Demonstration Project

Permeability scaling - Newberry Demonstration Project

Summary

Basic Observations of Permeability Evolution and IS

Challenges

- Prospecting (characterization)
- Accessing (drilling)
- Creating reservoir
- Sustaining reservoir
- Environmental issues

Observation

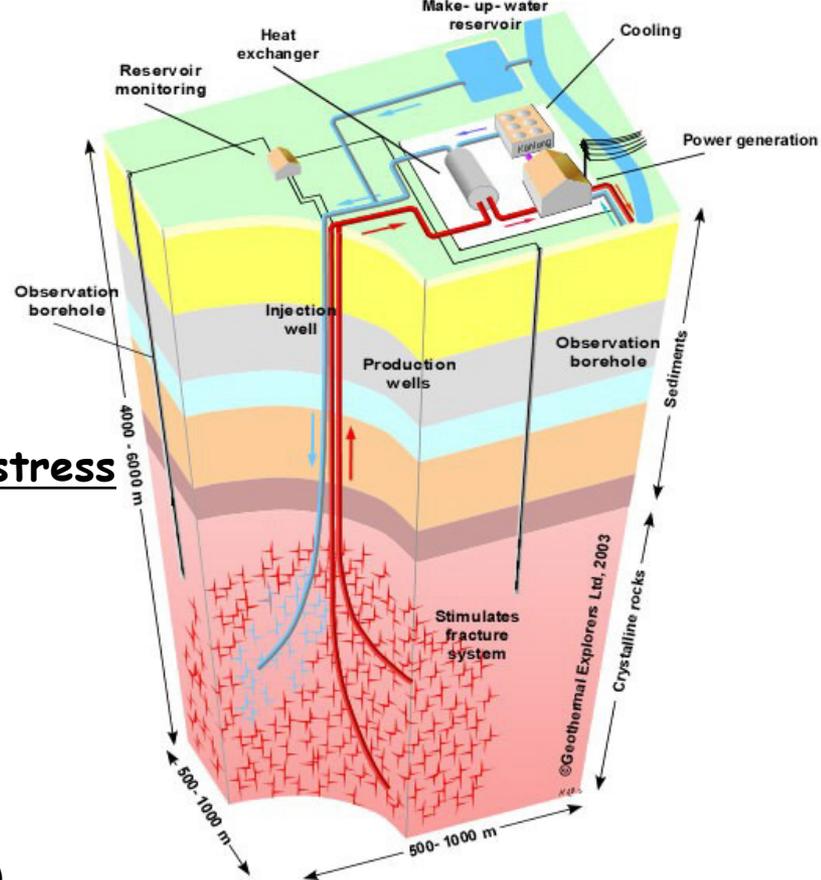
- Stress-sensitive reservoirs
- T H M C all influence via effective stress
- Effective stresses influence
 - Permeability
 - Reactive surface area
 - Induced seismicity

Understanding T H M C is key:

- Size of relative effects of THMC(B)
- Timing of effects
- Migration within reservoir
- Using them to engineer the reservoir

Resource

- Hydrothermal (US: 10^4 EJ)
- EGS (US: 10^7 EJ; 100 GW in 50y)



- Permeability
- Reactive surface area
- Induced seismicity

Anomalous Seismicity - The Missing Zone

Questions:

- What is the mechanism of this anomalous distribution of MEQs?
- What does the anomalous distribution of MEQs imply?

Wellbore Characteristics

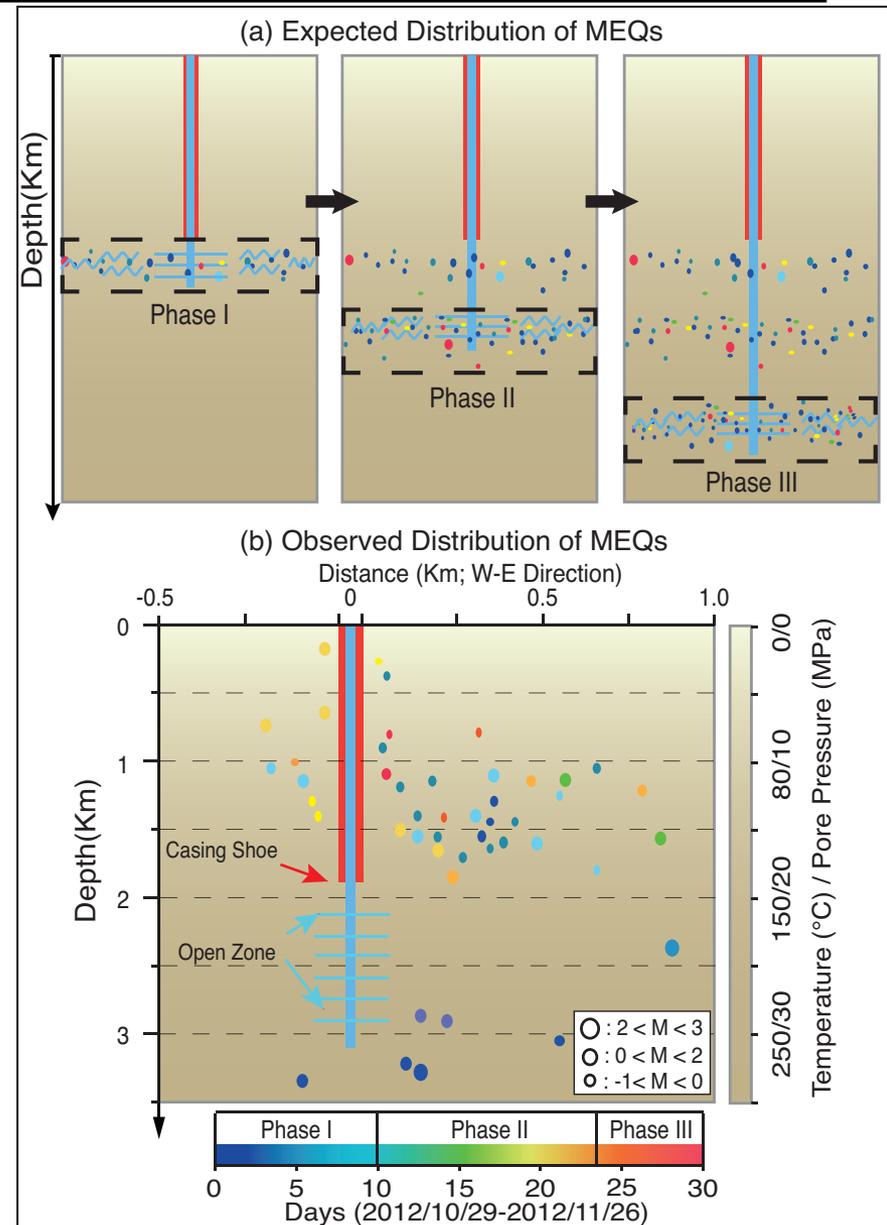
- 0-2000m: Casing shoe
- 2000m-3000m: open zone

Spatial Anomaly

- Bimodal depth distribution
- Below 1950 m, **only a few** MEQs occurred.
- Between 500m and 1800m, **90%** MEQs occurred adjacent to the cased part.

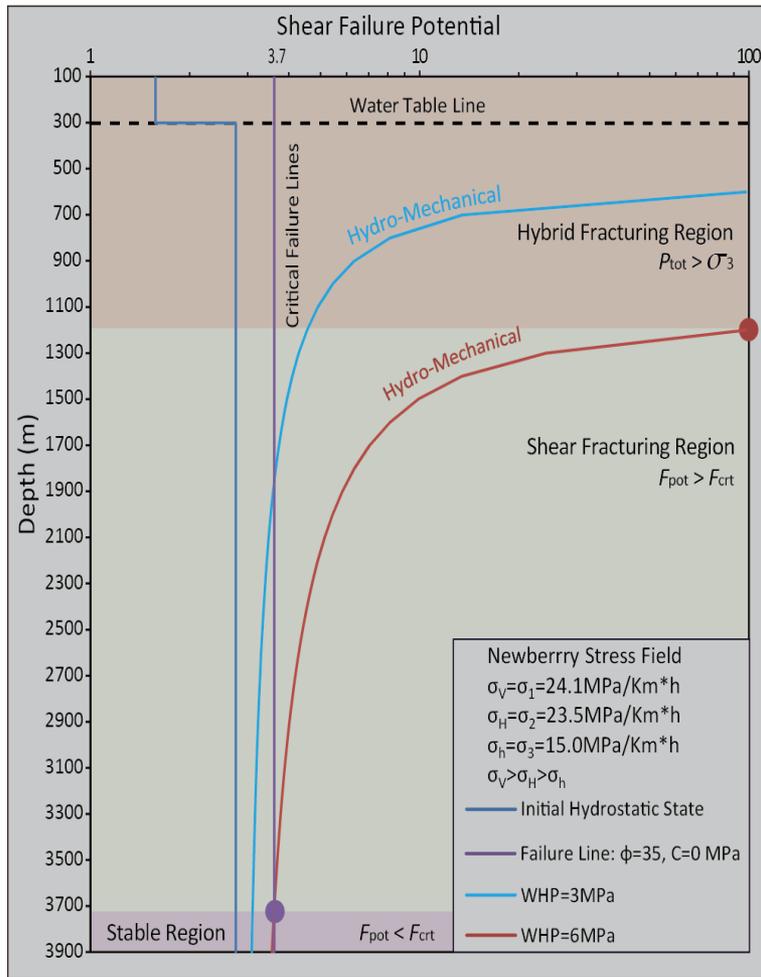
Temporal Anomaly

- Deep MEQs occurred within **4 days** and diminished after that time.
- Shallow MEQs occurred since the 4th day.



Constraints on Frictional Slip

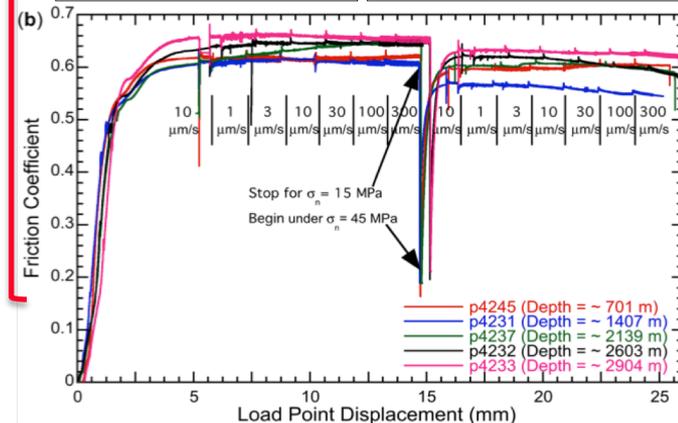
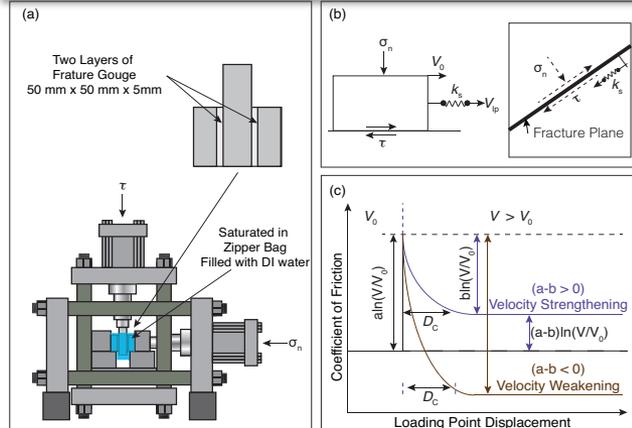
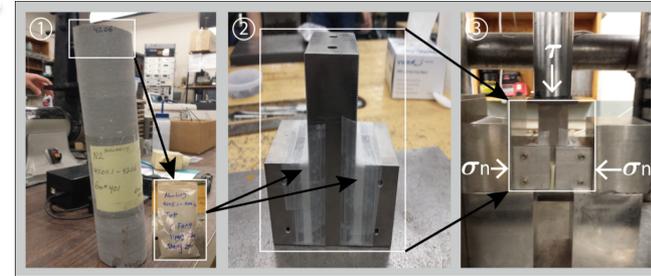
1. Shear Failure Analysis



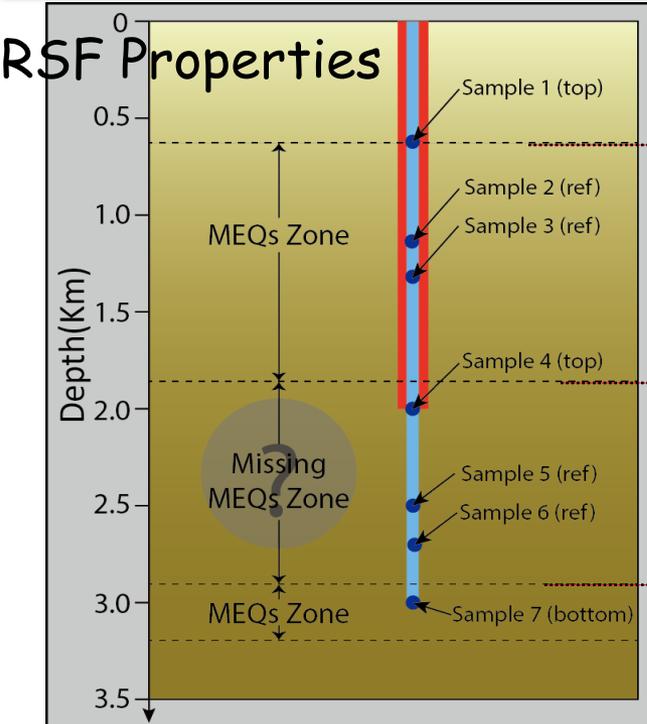
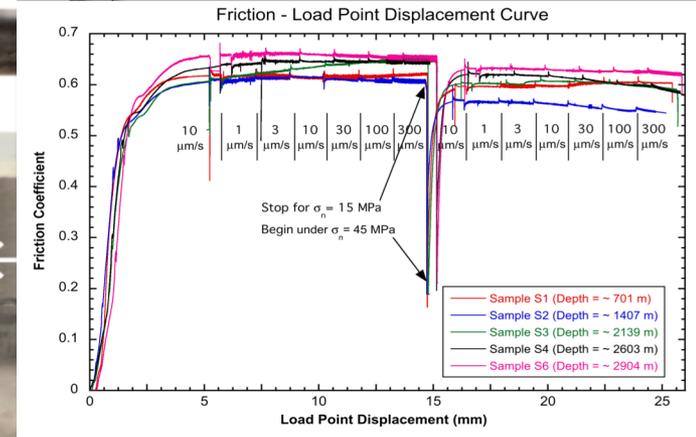
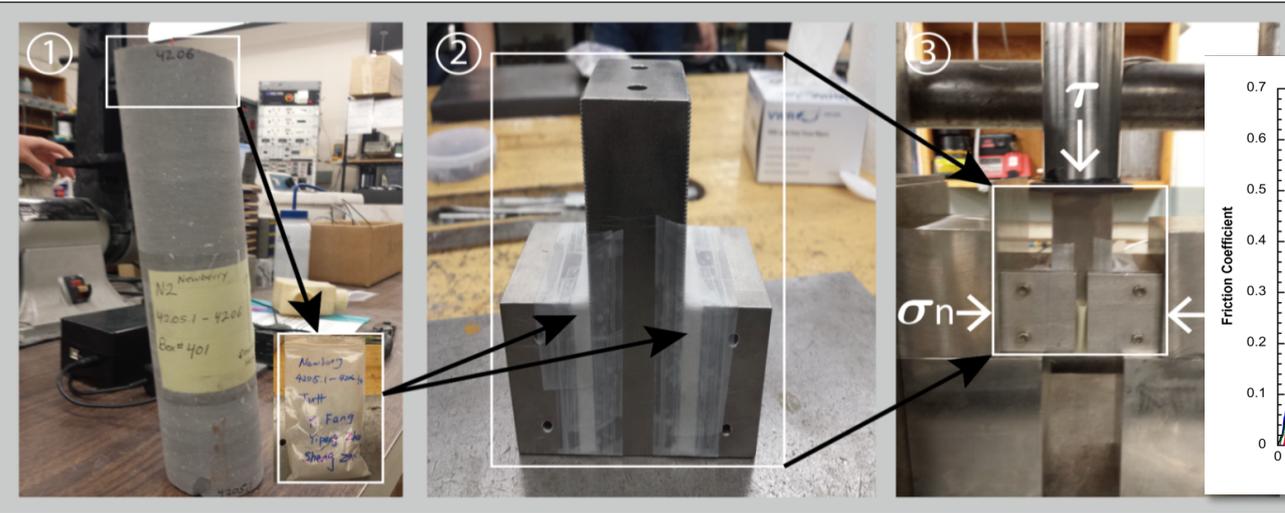
1. Shear Failure Analysis suggests that if seismicity occurs at great depth, it should occur continuously up the rock column, and not with a gap.

2. Frictional Experiments are performed to explore the frictional stability with depth and to explore the mechanisms of the unexplained seismic gap.

2. Friction Experiments

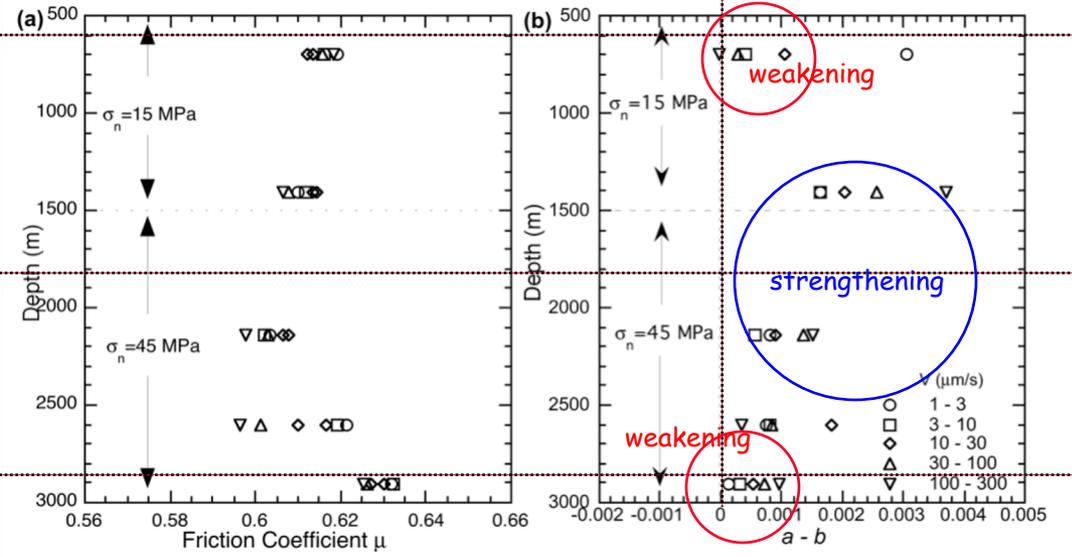


RSF Properties



Friction

(a-b) at 15-45 MPa

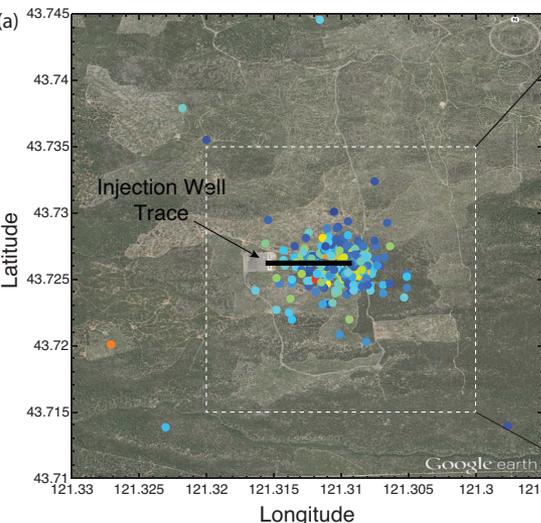
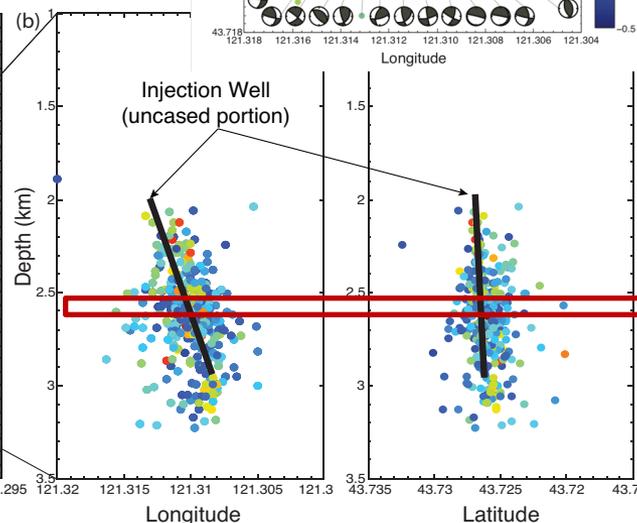
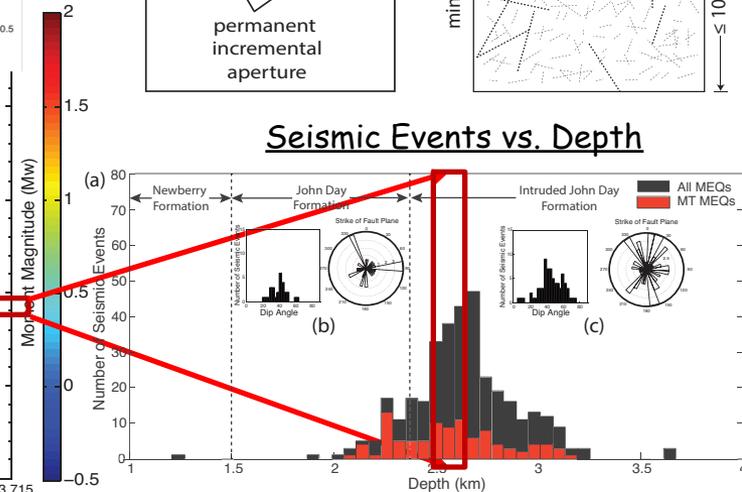
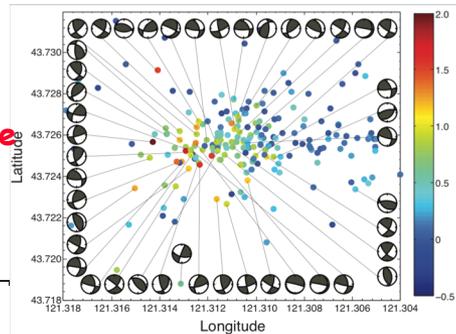
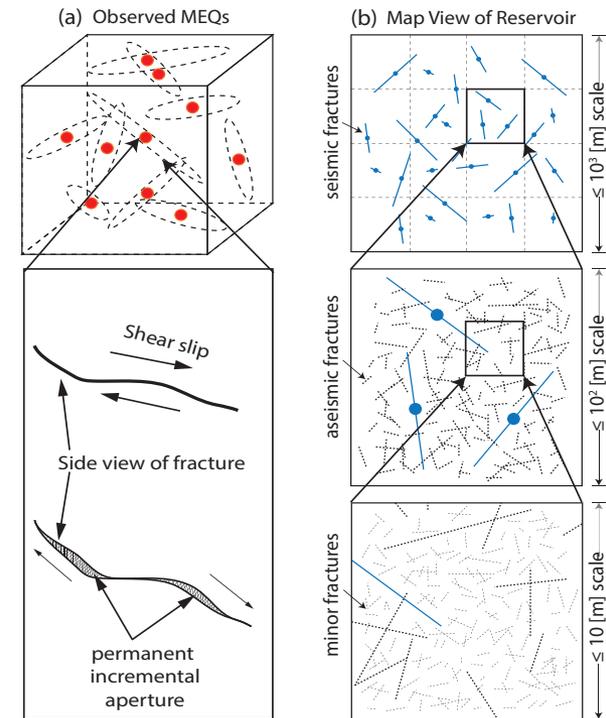


Linking MEQs to Permeability Evolution

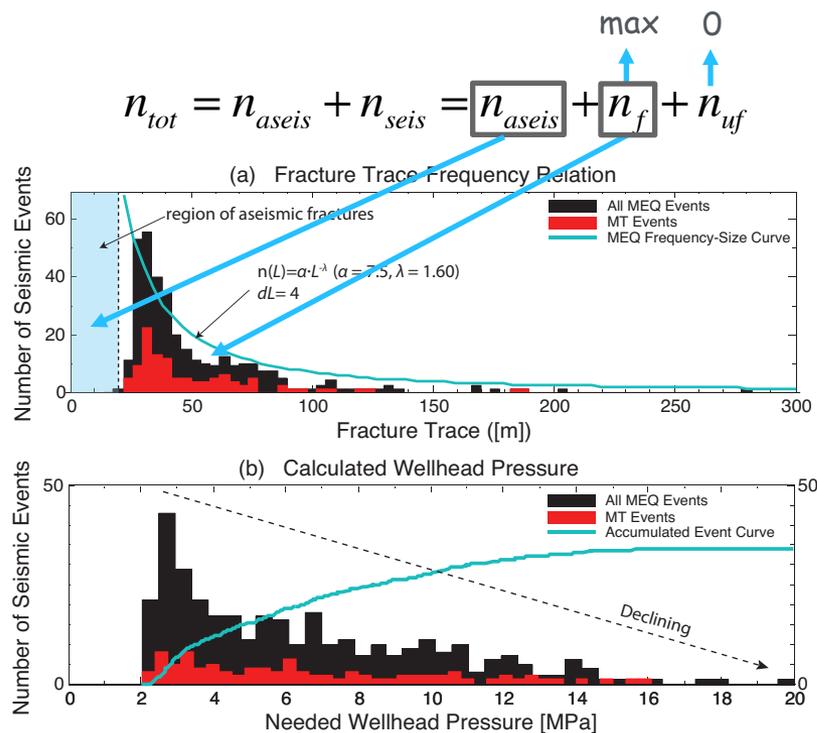
1. Seismicity induced by hydroshearing is controlled by the Mohr-Coulomb shear criterion.
2. The frictional coefficient evolves during seismic slip.
3. Two types of fractures:
 - Velocity-weakening/seismic fractures and,
 - Velocity-strengthening/aseismic fractures (fracture size smaller than the critical length).
4. Fracture interaction is ignored - consequently variations in the orientations of principal stresses are negligible

Workflow:

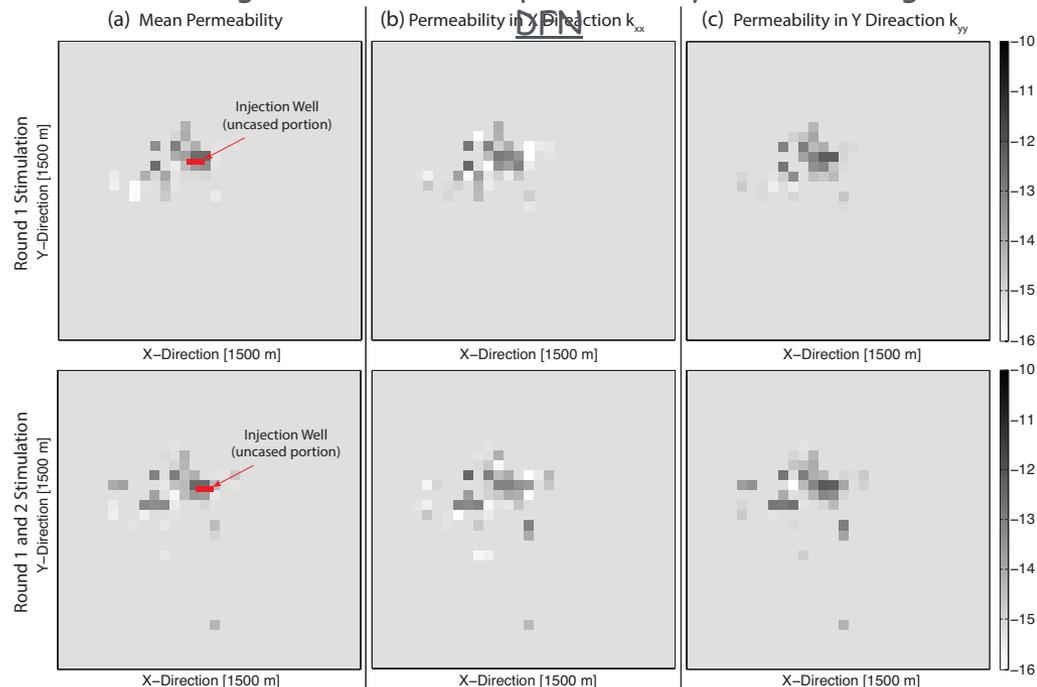
1. MT -> Orientation, mode of disp.
2. Magnitude, stress drop -> fracture size
3. Size -> roughness and dilation
4. Dilation/mode -> permeability evolution



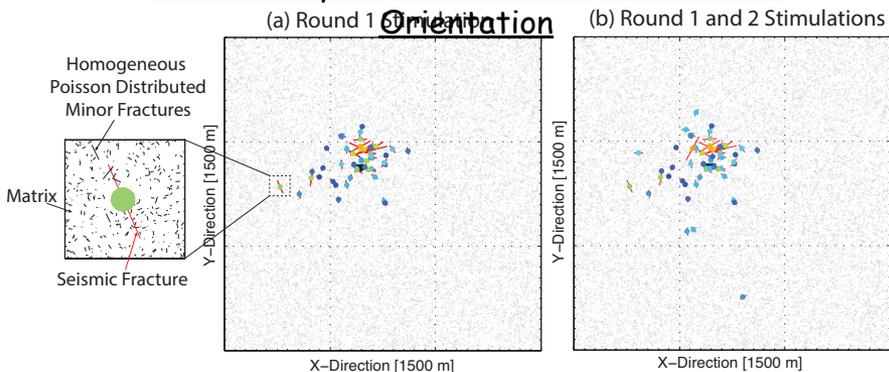
Seismicity-Permeability Validation



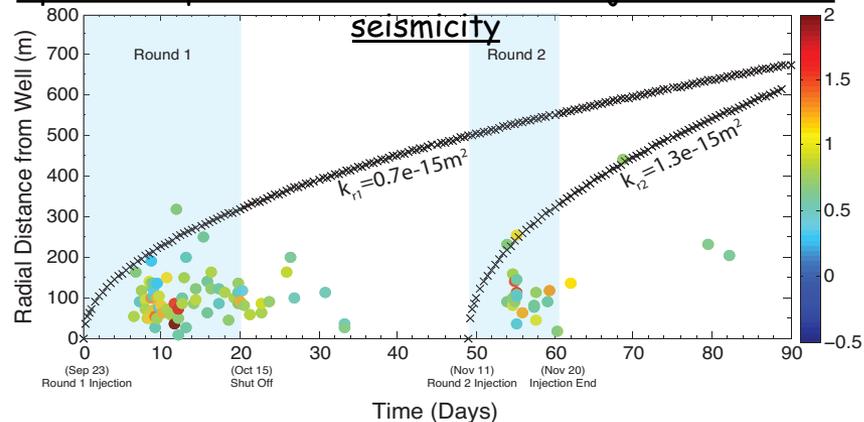
Cellular grid of stimulated permeability created using the



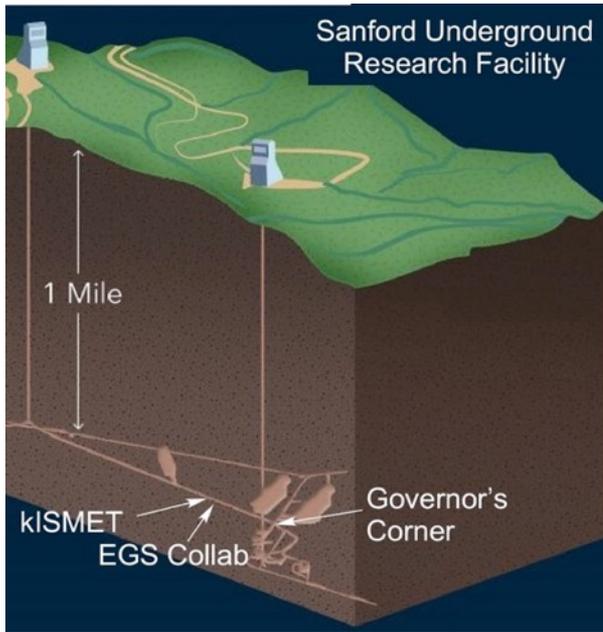
Statistically Inverted Fracture Trace and



Spatio-temporal distribution of fluid-injected-induced seismicity



DoE EGS Collab(oration) Project

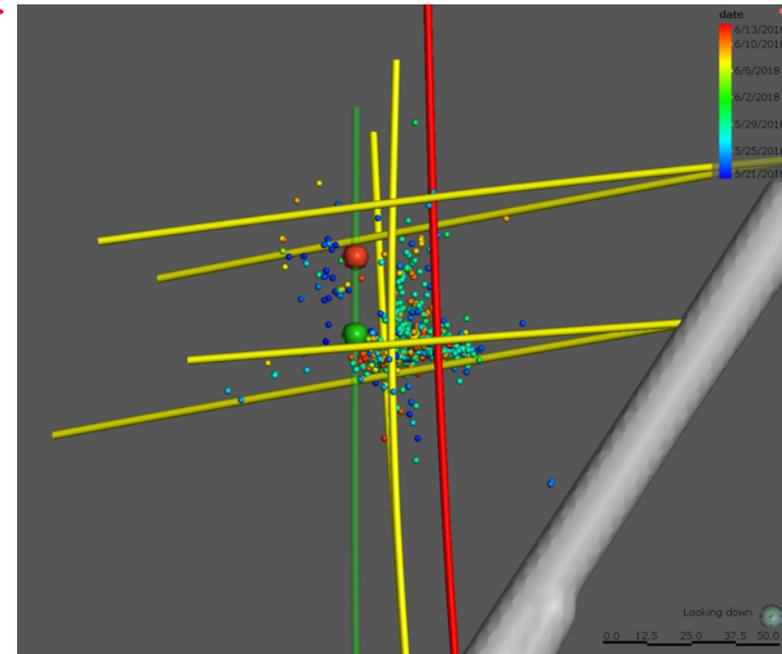
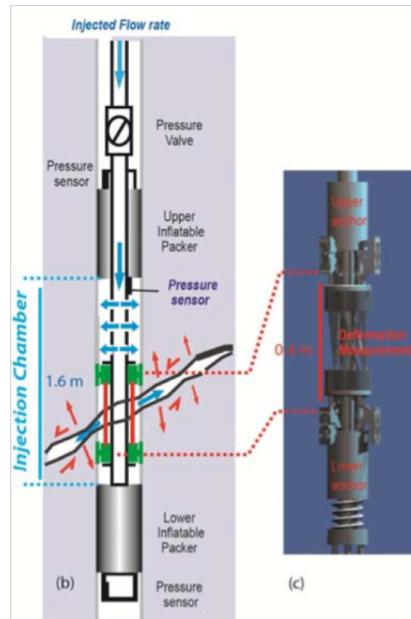
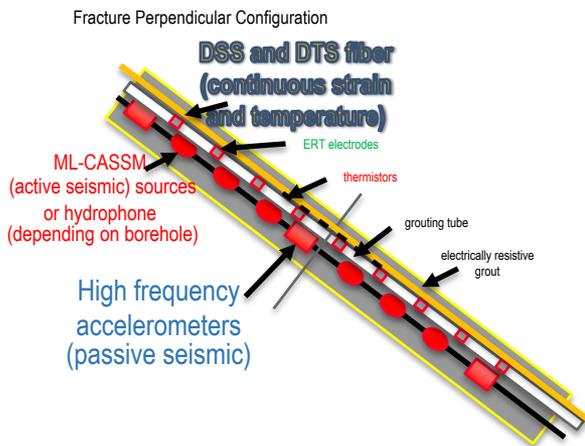


At Sanford Underground Research Facility (SURF-DUSEL) - 1500m

Experiment 1, intended to investigate hydraulic fracturing*, in situ

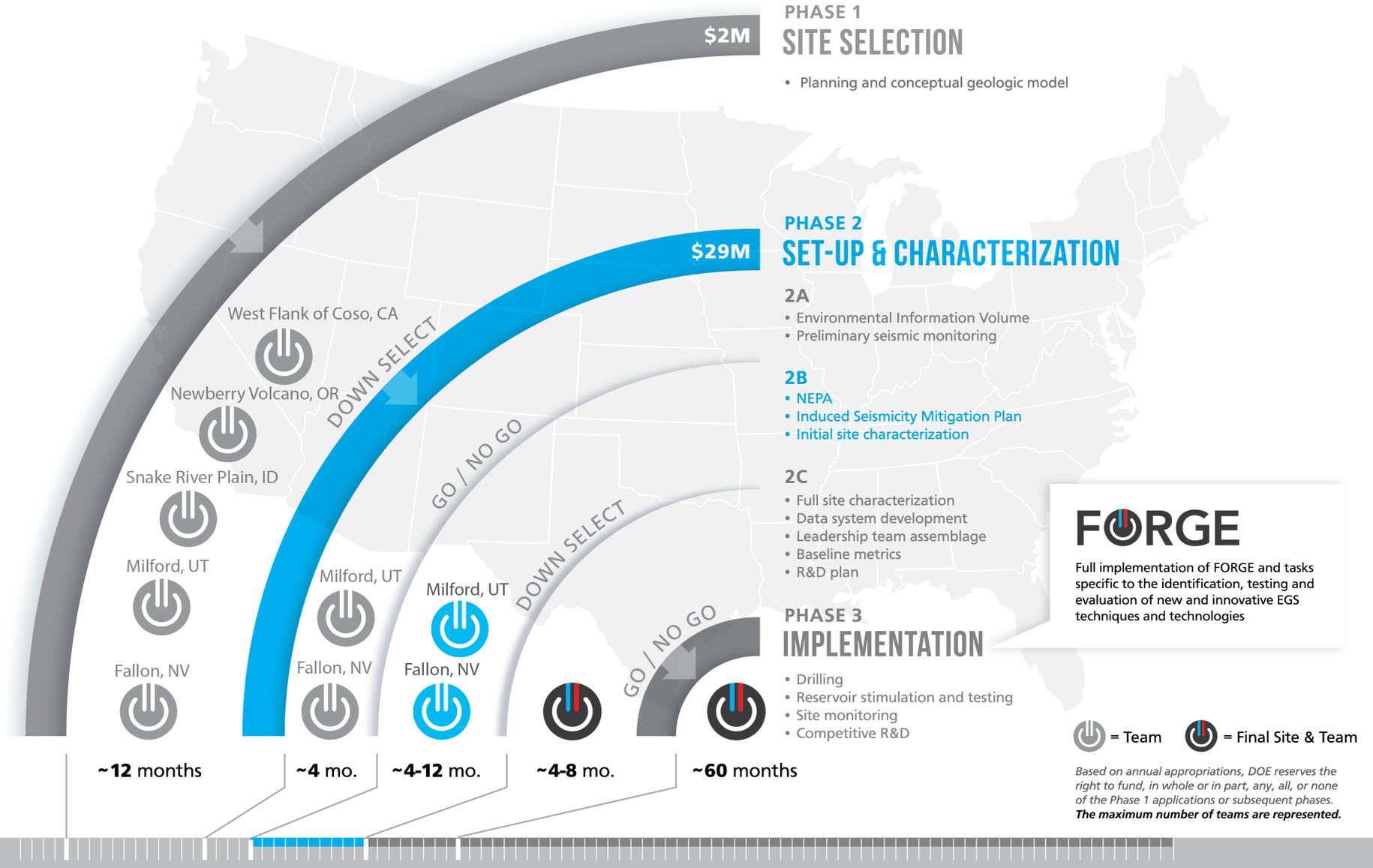
Experiment 2 designed to investigate shear stimulation*.

Experiment 3 will investigate changes in fracturing strategies - TBD.



Courtesy: Tim Kneafsey (LBNL), Tim Johnson (PNNL), Hunter Knox (SNL), Jonathan Ajo-Franklin (LBNL), Paul Cook (LBNL), Yves Guglielmi (LBNL), Martin Schoenball (LBNL), Hari Neupane (INL) & EGS Collab.

Frontier Observatory for Research in Geothermal Energy



Summary

Sub-Surface Science/Engineering is a Key Component to a Sustainable Future

Deep geothermal, unconventional resources and sequestration are examples
Access to, and the ability to create and control the "reservoir" is key

Complex Process Interactions Influence Reservoir Evolution

Permeability/Seismicity evolution is strongly influenced by these processes
These interactions can be complex and involve:

- Mineralogy

- Structure, texture and heterogeneity

- Evolving patch dimension

- Brittleness (a-b) and pore-pressure or effective stress level

- Role of Fault Core (FC) and Damage Zone (FDZ)

Interseismic Behavior

Necessary to reset permeability for brittle failure

Consistent with observations with far-field reactivation of faults/fractures

Prospects for Permeability-Seismicity Linkage

Observed seismicity is a certifiable predictor of permeability evolution

Possible despite potential for aseismic slip

- possibility that aseismic slip → creep → no dilation & wear products